



User's Guide

for

LibHuAirProp

**Library for the Calculation of Psychrometric,
Thermodynamic, and Transport Properties
for *Real* Humid Air, Steam, Water, and Ice**

I-P & SI Units

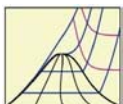
Version 10.0

FluidEXL for Excel

**Add-In for the comfortable use
of LibHuAirProp in Excel**

*Based on ASHRAE Research Projects
RP-1485 and RP-1767*

Prepared by



**THERMO
FLUID
PROPERTIES**

www.thermofluidprop.com

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LibHuAirProp Product Information

Do you need property values for moist air in I-P or SI units in your daily work?

► Use the property library LibHuAirProp ◀

Do you need these properties in Excel®, MATLAB®, Mathcad®, Mathcad Prime®, Engineering Equation Solver®, LabVIEW™, DYMOLA®, or SimulationX®?

► Use the add-ins FluidEXL, FluidLAB, FluidMAT, FluidPRIME, FluidEES, FluidVIEW, or FluidDYM ◀

What properties can be calculated using this software?

- thermodynamic properties psychrometric functions ◀
- transport properties backward functions ◀

What range of state is covered by this property library?

- unsaturated and saturated moist air ◀
- supersaturated moist air (liquid fog and ice fog) ◀
- temperatures from -143.15°C (-225.67°F) to 350°C (662°F) ◀
- pressures from 0.01 kPa (0.00145 psi) to 10,000 kPa (1450.4 psi) ◀

What are the references of LibHuAirProp?

Tables for moist air properties in the 2009, 2013, 2017, 2021, and 2025 ASHRAE Handbook of Fundamentals were calculated using LibHuAirProp

Psychrometrics

1.3

Table 2 Thermodynamic Properties of Moist Air at Standard Atmospheric Pressure, 101.325 kPa

Temp., °C <i>t</i>	Humidity Ratio <i>W_g</i> , kg _w /kg _{da}	Specific Volume, m ³ /kg _{da}			Specific Enthalpy, kJ/kg _{da}			Specific Entropy, kJ/(kg _{da} ·K)		Temp., °C <i>t</i>
		<i>v_{da}</i>	<i>v_{as}</i>	<i>v_g</i>	<i>h_{da}</i>	<i>h_{as}</i>	<i>h_g</i>	<i>s_{da}</i>	<i>s_g</i>	
-60	0.000067	0.6027	0.0000	0.6027	-60.341	0.016	-60.325	-0.2494	-0.2494	-60
-59	0.000076	0.6055	0.0000	0.6055	-59.335	0.018	-59.317	-0.2447	-0.2446	-59
-58	0.000087	0.6084	0.0000	0.6084	-58.329	0.021	-58.308	-0.2400	-0.2399	-58
-57	0.000100	0.6112	0.0000	0.6112	-57.323	0.024	-57.299	-0.2354	-0.2353	-57
-56	0.000114	0.6141	0.0000	0.6141	-56.317	0.027	-56.289	-0.2307	-0.2306	-56
-55	0.000129	0.6169	0.0000	0.6169	-55.311	0.031	-55.280	-0.2261	-0.2260	-55
-54	0.000147	0.6198	0.0000	0.6198	-54.305	0.035	-54.269	-0.2215	-0.2213	-54
-53	0.000167	0.6226	0.0000	0.6226	-53.299	0.040	-53.258	-0.2169	-0.2167	-53
-52	0.000190	0.6255	0.0000	0.6255	-52.293	0.046	-52.247	-0.2124	-0.2121	-52
-51	0.000215	0.6283	0.0000	0.6283	-51.287	0.052	-51.235	-0.2078	-0.2076	-51

Thermodynamic and psychrometric property algorithms from ASHRAE Research Project 1485

VOLUME 15, NUMBER 5

HVAC&R RESEARCH

SEPTEMBER 2009

FINAL REPORT ASHRAE RP-1485

Thermodynamic Properties of Real Moist Air,
Dry Air, Steam, Water, and Ice

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November 17, 2008 (Submitted to TC for review)

March 12, 2009 (Final with corrections)

January 18, 2017 (Last update)

(For the documentation of corrections and modifications see the Appendix)

Thermodynamic Properties of Real Moist Air, Dry Air, Steam, Water, and Ice (RP-1485)

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Received February 14, 2009; accepted May 6, 2009

This paper is based on findings resulting from ASHRAE Research Project RP-1485.

This research updates the modeling of moist air as a real gas mixture using the virial equation of state. It includes the Hyland and Wexler model (1983a, 1983b) and considers the Nelson-Sauer model (2002). All new National Institute of Standards and Technology reference equations and the latest International Association for the Properties of Water and Steam (IAPWS) standards, as well as the current values for the molar masses and gas constants, have been incorporated. The deviations of the proposed model to the Hyland-Wexler and Nelson-Sauer models are very low at ambient pressures but increase with increasing pressures and temperatures. The range of validity of the new model is in pressure from 0.01 kPa up to 10 MPa, in temperature from -143.15°C up to 350°C, and in humidity ratio from 0 kg_w/kg_{da} up to 10 kg_w/kg_{da}. This model was used to produce moist air and H₂O saturation property tables for the psychrometric chapter in the 2009 ASHRAE Handbook—Fundamentals (ASHRAE 2009). The paper summarizes ASHRAE Research Project 1485 (RP-1485).

Transport property algorithms of moist air from ASHRAE Research Project 1767

FINAL REPORT

ASHRAE RP-1767

Transport Properties of Real Moist Air, Dry Air, Steam, and Water

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December 31, 2018

Properties of dry air from the NIST Reference Equation of *Lemmon et al.* and properties of steam, water, and ice from the Industrial Formulation IAPWS-IF97, the Scientific Formulation IAPWS-95, and other current IAPWS formulations

Thermodynamic Properties of Air and Mixtures of Nitrogen, Argon, and Oxygen From 60 to 2000 K at Pressures to 2000 MPa

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Received June 25, 1999; revised manuscript received December 2, 1999

A thermodynamic property formulation for standard dry air based upon available experimental p - ρ - T , heat capacity, speed of sound, and vapor-liquid equilibrium data is presented. This formulation is valid for liquid, vapor, and supercritical air at temperatures from the solidification point on the bubble-point curve (59.75 K) to 2000 K at pressures up to 2000 MPa. In the absence of reliable experimental data for air above 873 K and 70 MPa, air properties were predicted from nitrogen data in this region. These values were included in the determination of the formulation to extend the range of validity. Experimental shock tube measurements on air give an indication of the extrapolation behavior of the equation of state up to temperatures and pressures of 5000 K and 98 GPa. The

0047-2689/2009/29(3)/331/55/\$37.00

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J. Phys. Chem. Ref. Data, Vol. 29, No. 3, 2000

The International Association for the Properties of Water and Steam

Lucerne, Switzerland
August 2007

Revised Release on the IAPWS Industrial Formulation 1997
for the Thermodynamic Properties of Water and Steam
(The revision only relates to the extension of region 5 to 50 MPa)

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The International Association for the Properties of Water and Steam

Doorwerth, The Netherlands
September 2009

Revised Release on the IAPWS Formulation 1995 for the Thermodynamic
Properties of Ordinary Water Substance for General and Scientific Use

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Property Library for *Real Humid Air*, Steam, Water, and Ice

ASHRAE-LibHuAirProp

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0 Package Contents

Add-Ins for 32- or 64-bit version of Microsoft Office®

The following ZIP file has been delivered for your computer running a 32- or 64-bit version of Microsoft Office®.

ZIP file "CD_FluidEXL_ASHRAE_LibHuAirProp.zip" for Excel®

The ZIP file contains the following files and folders:

- \Chm\

- \Files\

- \Office32\

- \Office64\

- FluidEXL_ASHRAE_LibHuAirProp_Users_Guide.pdf

- FluidEXL_Graphics.msi

Part I-P Units

1 Property Library ASHRAE-LibHuAirProp-IP

1.1 Function Overview

1.1.1 Function Overview for Real Moist Air

Functional Dependence	Function Name	Property or Function	Unit of the Result	Page
$a = f(p, t, W)$	a_ptW_HAP_IP	Thermal diffusivity	ft ² /s	3/2
$\alpha_p = f(p, t, W)$	alphap_ptW_HAP_IP	Relative pressure coefficient	1/°R	3/3
$\beta_p = f(p, t, W)$	betap_ptW_HAP_IP	Isothermal stress coefficient	lb/ft ³	3/4
$c = f(p, t, W)$	c_ptW_HAP_IP	Speed of sound	ft/s	3/5
$c_p = f(p, t, W)$	cp_ptW_HAP_IP	Specific isobaric heat capacity	Btu/(lb·°R)	3/6
$c_v = f(p, t, W)$	cv_ptW_HAP_IP	Specific isochoric heat capacity	Btu/(lb·°R)	3/7
$f = f(p, t)$	f_pt_HAP_IP	Enhancement factor (decimal ratio)	-	3/8
$h = f(p, t, W)$	h_ptW_HAP_IP	Air-specific enthalpy	Btu/lb _a	3/9
$\eta = f(p, t, W)$	Eta_ptW_HAP_IP	Dynamic viscosity	lb·s/ft ²	3/10
$\kappa = f(p, t, W)$	Kappa_ptW_HAP_IP	Isentropic exponent	-	3/11
$\lambda = f(p, t, W)$	Lambda_ptW_HAP_IP	Thermal conductivity	Btu/(h·ft·°R)	3/12
$\nu = f(p, t, W)$	Ny_ptW_HAP_IP	Kinematic viscosity	ft ² /s	3/13
$p = f(t, s, W)$	p_tsW_HAP_IP	Pressure of humid air	psi	3/14
$p = f(z_{\text{ele}})$	p_zele_HAP_IP	Pressure of humid air from elevation	psi	3/15
$p_{\text{Air}} = f(p, t, W)$	pAIR_ptW_HAP_IP	Partial pressure of dry air in moist air	psi	3/16
$p_{\text{H}_2\text{O}} = f(p, t, W)$	pH2O_ptW_HAP_IP	Partial pressure of water vapor in moist air	psi	3/17
$p_{\text{H}_2\text{O}_s} = f(p, t)$	pH2Os_pt_HAP_IP	Partial saturation pressure of water vapour in moist air	psi	3/18

Functional Dependence	Function Name	Property or Function	Unit of the Result	Page
$\phi = f(p, t, W)$	phi_ptW_HAP_IP	Relative humidity (decimal ratio)	-	3/19
$Pr = f(p, t, W)$	Pr_ptW_HAP_IP	PRANDTL number	-	3/20
$\psi_{\text{Air}} = f(W)$	PsiAir_W_HAP_IP	Mole fraction of dry air in moist air	mol _a /mol	3/21
$\psi_{\text{H}_2\text{O}} = f(W)$	PsiH2O_W_HAP_IP	Mole fraction of water vapor in moist air	mol _w /mol	3/22
$\rho = f(p, t, W)$	Rho_ptW_HAP_IP	Density	lb/ft ³	3/23
$s = f(p, t, W)$	s_ptW_HAP_IP	Air-specific entropy	Btu/(lb _a ·°R)	3/24
$t = f(p, h, \phi)$	t_phphi_HAP_IP	Backward function: temperature from total pressure, air-specific enthalpy and relative humidity	°F	3/25
$t = f(p, h, W)$	t_phW_HAP_IP	Backward function: temperature from total pressure, enthalpy and humidity ratio	°F	3/26
$t = f(p, s, W)$	t_psW_HAP_IP	Backward function: temperature from total pressure, entropy and humidity ratio	°F	3/27
$t = f(p, t_{\text{wb}}, W)$	t_ptwbW_HAP_IP	Backward function: temperature from total pressure, wet-bulb temperature and humidity ratio	°F	3/28
$t_d = f(p, W)$	td_pW_HAP_IP	Dew-point/frost-point temperature	°F	3/29
$t_s = f(p, p_{\text{H}_2\text{O}})$	ts_ppH2O_HAP_IP	Backward function: saturation temperature of water from total pressure and partial pressure of water vapor	°F	3/30
$t_{\text{wb}} = f(p, t, W)$	twb_ptW_HAP_IP	Wet-bulb/ice-bulb temperature	°F	3/31
$u = f(p, t, W)$	u_ptW_HAP_IP	Air-specific internal energy	Btu/lb _a	3/32
$v = f(p, t, W)$	v_ptW_HAP_IP	Air-specific volume	ft ³ /lb _a	3/33
$W = f(p, t, p_{\text{H}_2\text{O}})$	W_ptpH2O_HAP_IP	Humidity ratio from total pressure, temperature, and partial pressure of water vapor	lb _w /lb _a	3/34
$W = f(p, t, \phi)$	W_ptphi_HAP_IP	Humidity ratio from total pressure, temperature, and relative humidity	lb _w /lb _a	3/35
$W = f(p, t_d)$	W_ptd_HAP_IP	Humidity ratio from total pressure and dew-point temperature	lb _w /lb _a	3/36

Functional Dependence	Function Name	Property or Function	Unit of the Result	Page
$W = f(p, t, t_{wb})$	W_pttwb_HAP_IP	Humidity ratio from total pressure, (dry bulb) temperature, and wet-bulb temperature	lb _w /lb _a	3/37
$W_s = f(p, t)$	Ws_pt_HAP_IP	Saturation humidity ratio	lb _w /lb _a	3/38
$\xi_{Air} = f(W)$	XiAir_W_HAP_IP	Mass fraction of dry air in moist air	lb _a /lb	3/39
$\xi_{H2O} = f(W)$	XiH2O_W_HAP_IP	Mass fraction of water vapor in moist air	lb _w /lb	3/40
$Z = f(p, t, W)$	Z_ptW_HAP_IP	Compression factor (decimal ratio)	-	3/41

Range of Validity of Thermodynamic Properties

Property	Range of Validity					
Pressure:	0.00145	≤	p	≤	1450.4	psi
Temperature:	-225.67	≤	t	≤	662	°F
Humidity ratio:	0	≤	W	≤	10	lb _w /lb _a
Relative humidity:	0	≤	ϕ	≤	1	(decimal ratio)
Dew-point temperature:	-225.67	≤	t_d	≤	662	°F
Wet-bulb temperature:	-225.67	≤	t_{wb}	≤	662	°F

Units

Symbol	Quantity	Unit
p	Pressure	psi
t	Temperature	°F
W	Humidity ratio	lb _w /lb _a (lb water / lb dry air)
ϕ	Relative humidity	(decimal ratio)
t_d	Dew point temperature	°F
t_{wb}	Wet bulb temperature	°F

Range of Validity of Transport Properties

Property	Range of Validity					
Pressure:	0.00145	≤	p	≤	1450.4	psi
Temperature:	-99.67	≤	t	≤	662	°F
Humidity ratio:	0	≤	W	≤	10	lb _w /lb _a
Relative humidity:	0	≤	ϕ	≤	1	(decimal ratio)

Molar Masses

Component	Molar Mass	Reference
Dry Air	63.859 lb/kmol	[17]
Water	39.7168998 lb/kmol	[5], [6]

Reference States

Property	Dry Air	Steam, Water, and Ice
Pressure	14.6959 psi	$p_s(32.018^\circ\text{F}) = 0.088714$ psi
Temperature	32°F	32.018°F
Enthalpy	0 Btu/lb	0.00026301926 Btu/lb
Entropy	0 Btu/(lb·°R)	0 Btu/(lb·°R)

1.1.2 Function Overview for Steam and Water for Temperatures $t \geq 32^\circ\text{F}$

Functional Dependence	Function Name	Property or Function	Unit of the Result	Page
$h_{\text{liq}} = f(p, t)$	hliq_pt_97_IP	Specific enthalpy of liquid water	Btu/lb	3/43
$h_{\text{liq,s}} = f(t)$	hliqs_t_97_IP	Specific enthalpy of saturated liquid water	Btu/lb	3/44
$h_{\text{vap,s}} = f(t)$	hvaps_t_97_IP	Specific enthalpy of saturated water vapor	Btu/lb	3/45
$p_s = f(t)$	ps_t_97_IP	Saturation pressure of water	psi	3/46
$s_{\text{liq}} = f(p, t)$	sliq_pt_97_IP	Specific entropy of liquid water	Btu/(lb·°R)	3/47
$s_{\text{liq,s}} = f(t)$	sliqs_t_97_IP	Specific entropy of saturated liquid water	Btu/(lb·°R)	3/48
$s_{\text{vap,s}} = f(t)$	svaps_t_97_IP	Specific entropy of saturated water vapor	Btu/(lb·°R)	3/49
$t_s = f(p)$	ts_p_97_IP	Saturation temperature of water	°F	3/50
$v_{\text{liq}} = f(p, t)$	vliq_pt_97_IP	Specific volume of liquid water	ft ³ /lb	3/51
$v_{\text{liq,s}} = f(t)$	vliqs_t_97_IP	Specific volume of saturated liquid water	ft ³ /lb	3/52
$v_{\text{vap,s}} = f(t)$	vvaps_t_97_IP	Specific volume of saturated water vapor	ft ³ /lb	3/53

Range of Validity

Property	Range of Validity				
Pressure:	0.00145	\leq	p	\leq	1450.4 psi
Temperature:	32	\leq	t	\leq	662 °F

Reference State

Property	Water Vapor and Liquid Water
Pressure	$p_s(32.018^\circ\text{F}) = 0.088714$ psi
Temperature	32.018°F
Enthalpy	0.00026301926 Btu/lb
Entropy	0 Btu/(lb·°R)

Units

Symbol	Quantity	Unit
p	Pressure	psi
t	Temperature	°F

1.1.3 Function Overview for Steam and Ice for Temperatures $t \leq 32^\circ\text{F}$

Functional Dependence	Function Name	Property	Unit of the Result	Page
$h_{\text{ice,sub}} = f(t)$	hicesub_t_06_IP	Specific enthalpy of saturated ice	Btu/lb	3/55
$h_{\text{vap,sub}} = f(t)$	hvapsub_t_95_IP	Specific enthalpy of saturated water vapor	Btu/lb	3/56
$p_{\text{mel}} = f(t)$	pmel_t_08_IP	Melting pressure of ice	psi	3/57
$p_{\text{sub}} = f(t)$	psub_t_08_IP	Sublimation pressure of ice	psi	3/58
$s_{\text{ice,sub}} = f(t)$	sicesub_t_06_IP	Specific entropy of saturated ice	Btu/(lb·°R)	3/59
$s_{\text{vap,sub}} = f(t)$	svapsub_t_95_IP	Specific entropy of saturated water vapor	Btu/(lb·°R)	3/60
$t_{\text{mel}} = f(p)$	tmel_p_08_IP	Melting temperature of ice	°F	3/61
$t_{\text{sub}} = f(p)$	tsub_p_08_IP	Sublimation temperature of ice	°F	3/62
$v_{\text{ice,sub}} = f(t)$	vicesub_t_06_IP	Specific volume of saturated ice	ft ³ /lb	3/63
$v_{\text{vap,sub}} = f(t)$	vvapsub_t_95_IP	Specific volume of saturated water vapor	ft ³ /lb	3/64

Range of Validity

Property	Range of Validity				
Pressure:	$p_{\text{sub}}(-225.67^{\circ}\text{F}) = 1.7407\text{E-}12$	\leq	p	\leq	1450.4 psi
Temperature:	-225.67	\leq	t	\leq	32 °F

Units

Symbol	Quantity	Unit
p	Pressure	psi
t	Temperature	°F

Reference State

Property	Water Vapor and Ice
Pressure	$p_s(32.018^{\circ}\text{F}) = 0.088714$ psi
Temperature	32.018°F
Enthalpy	0.00026301926 Btu/lb
Entropy	0 Btu/(lb·°R)

1.2 Conversion of SI and I-P Units

Property	Conversion: SI Units → I-P Units	Conversion: I-P Units → SI Units	Units SI	Units I-P
Thermal diffusivity a	$\frac{a_{IP}}{\frac{ft^2}{s}} = \frac{a_{SI}}{\frac{m^2}{s}} \times 10.76391042$	$\frac{a_{SI}}{\frac{m^2}{s}} = \frac{a_{IP}}{\frac{ft^2}{s}} \times 0.0929304$	m ² /s	ft ² /s
Relative pressure coefficient α_p	$\frac{\alpha_{p,IP}}{\frac{1}{^\circ R}} = \frac{\alpha_{p,SI}}{\frac{1}{K}} \times \frac{9}{5}$	$\frac{\alpha_{p,SI}}{\frac{1}{K}} = \frac{\alpha_{p,IP}}{\frac{1}{^\circ R}} \times \frac{5}{9}$	1/K	1/°R
Isothermal stress coefficient β_p	$\frac{\beta_{p,IP}}{\frac{lb}{ft^3}} = \frac{\beta_{p,SI}}{\frac{kg}{m^3}} \times 0.062428$	$\frac{\beta_{p,SI}}{\frac{kg}{m^3}} = \frac{\beta_{p,IP}}{\frac{lb}{ft^3}} \times 16.018463$	kg/m ³	lb/ft ³
Speed of sound c	$\frac{c_{IP}}{\frac{ft}{s}} = \frac{c_{SI}}{\frac{m}{s}} \times 3.2808399$	$\frac{c_{SI}}{\frac{m}{s}} = \frac{c_{IP}}{\frac{ft}{s}} \times 0.3048$	m/s	ft/s
Specific isobaric heat capacity c_p	$\frac{c_{p,IP}}{\frac{Btu}{lb \cdot ^\circ R}} = \frac{c_{p,SI}}{\frac{kJ}{kg \cdot K}} \times 0.2388459$	$\frac{c_{p,SI}}{\frac{kJ}{kg \cdot K}} = \frac{c_{p,IP}}{\frac{Btu}{lb \cdot ^\circ R}} \times 4.1868$	kJ/(kg·K)	Btu/(lb·°R)
Specific isochoric heat capacity c_v	$\frac{c_{v,IP}}{\frac{Btu}{lb \cdot ^\circ R}} = \frac{c_{v,SI}}{\frac{kJ}{kg \cdot K}} \times 0.2388459$	$\frac{c_{v,SI}}{\frac{kJ}{kg \cdot K}} = \frac{c_{v,IP}}{\frac{Btu}{lb \cdot ^\circ R}} \times 4.1868$	kJ/(kg·K)	Btu/(lb·°R)
Dynamic viscosity η	$\frac{\eta_{IP}}{\frac{lb \cdot s}{ft^2}} = \frac{\eta_{SI}}{\frac{Pa \cdot s}}{\frac{Pa \cdot s}{s}} \times 0.02088543$	$\frac{\eta_{SI}}{\frac{Pa \cdot s}}{\frac{Pa \cdot s}{s}} = \frac{\eta_{IP}}{\frac{lb \cdot s}{ft^2}} \times 47.880259$	Pa·s	lb·s/ft ²
Enhancement factor f	$f_{IP} = f_{SI}$	$f_{SI} = f_{IP}$	-	-

Property	Conversion: SI Units → I-P Units	Conversion: I-P Units → SI Units	Units SI	Units I-P
Air-specific enthalpy (moist air) h	$\frac{h_{IP}}{\text{Btu/lb}_a} = \frac{h_{SI}}{\text{kJ/kg}_a} \times 0.4299226 + 7.68565365666$	$\frac{h_{SI}}{\text{kJ/kg}_a} = \left(\frac{h_{IP}}{\text{Btu/lb}_a} - 7.68565365666 \right) \times 2.326$	kJ/kg _a	Btu/lb _a
Specific enthalpy (water, water vapor, ice) h_w	$\frac{h_{IP}}{\text{Btu/lb}} = \frac{h_{SI}}{\text{kJ/kg}} \times 0.4299226$	$\frac{h_{SI}}{\text{kJ/kg}} = \frac{h_{IP}}{\text{Btu/lb}} \times 2.326$	kJ/kg	Btu/lb
Isentropic exponent κ	$\kappa_{IP} = \kappa_{SI}$	$\kappa_{SI} = \kappa_{IP}$	-	-
Thermal conductivity λ	$\frac{\lambda_{IP}}{\text{Btu/h ft } ^\circ\text{R}} = \frac{\lambda_{SI}}{\text{W/m K}} \times 0.57778932$	$\frac{\lambda_{SI}}{\text{W/m K}} = \frac{\lambda_{IP}}{\text{Btu/h ft } ^\circ\text{R}} \times 1.73073467$	W/(m·K)	Btu/(h·ft·°R)
Kinematic viscosity ν	$\frac{\nu_{IP}}{\text{ft}^2/\text{s}} = \frac{\nu_{SI}}{\text{m}^2/\text{s}} \times 10.763910417$	$\frac{\nu_{SI}}{\text{m}^2/\text{s}} = \frac{\nu_{IP}}{\text{ft}^2/\text{s}} \times 0.092903040$	m ² /s	ft ² /s
Pressure p	$\frac{p_{IP}}{\text{psi}} = \frac{p_{SI}}{\text{kPa}} \times 0.14503774$	$\frac{p_{SI}}{\text{kPa}} = \frac{p_{IP}}{\text{psi}} \times 6.894757$	kPa	psi
Relative humidity ϕ	$\phi_{IP} = \phi_{SI}$	$\phi_{SI} = \phi_{IP}$	-	-
Prandtl number Pr	$Pr_{IP} = Pr_{SI}$	$Pr_{SI} = Pr_{IP}$	-	-
Mole fraction ψ	$\psi_{IP} = \psi_{SI}$	$\psi_{SI} = \psi_{IP}$	mol/mol	mol/mol
Density ρ	$\frac{\rho_{IP}}{\text{lb/ft}^3} = \frac{\rho_{SI}}{\text{kg/m}^3} \times 0.062428$	$\frac{\rho_{SI}}{\text{kg/m}^3} = \frac{\rho_{IP}}{\text{lb/ft}^3} \times 16.018463$	kg/m ³	lb/ft ³
Air-specific entropy (moist air) s	$\frac{s_{IP}}{\text{Btu/lb}_a \text{ } ^\circ\text{R}} = \frac{s_{SI}}{\text{kJ/kg}_a \text{ K}} \times 0.2388459 + 0.01616365106$	$\frac{s_{SI}}{\text{kJ/kg}_a \text{ K}} = \left(\frac{s_{IP}}{\text{Btu/lb}_a \text{ } ^\circ\text{R}} - 0.01616365106 \right) \times 4.1868$	kJ/(kg _a ·K)	Btu/(lb _a ·°R)

Property	Conversion: SI Units → I-P Units	Conversion: I-P Units → SI Units	Units SI	Units I-P
Specific entropy (water, water vapor, ice) s_w	$\frac{s_{IP}}{\frac{\text{Btu}}{\text{lb}_a \cdot ^\circ\text{R}}} = \frac{s_{SI}}{\frac{\text{kJ}}{\text{kg}_a \cdot \text{K}}} \times 0.23884589$	$\frac{s_{SI}}{\frac{\text{kJ}}{\text{kg}_a \cdot \text{K}}} = \frac{s_{IP}}{\frac{\text{Btu}}{\text{lb}_a \cdot ^\circ\text{R}}} \times 4.1868$	kJ/(kg _a ·K)	Btu/(lb _a ·°R)
Temperature t	$\frac{t_{IP}}{^\circ\text{F}} = \frac{t_{SI}}{^\circ\text{C}} \times \frac{9}{5} + 32$	$\frac{t_{SI}}{^\circ\text{C}} = \left(\frac{t_{IP}}{^\circ\text{F}} - 32 \right) \times \frac{5}{9}$	°C	°F
Air-specific internal energy (moist air) u	$(u = h - pv)$ $\frac{u_{IP}}{\frac{\text{Btu}}{\text{lb}_a}} = \frac{h_{SI}}{\frac{\text{kJ}}{\text{kg}_a}} \times 0.4299226 + 7.68565365666$ $- \frac{p_{SI}}{\text{kPa}} \times 0.145037738 \cdot \frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}_a}} \times 16.018453$	$(u = h - pv)$ $\frac{u_{SI}}{\frac{\text{kJ}}{\text{kg}_a}} = \left(\frac{h_{IP}}{\frac{\text{Btu}}{\text{lb}_a}} - 7.68565365666 \right) \times 2.236$ $- \frac{p_{IP}}{\text{psi}} \times 6.894757293 \cdot \frac{v_{SI}}{\frac{\text{ft}^3}{\text{lb}_a}} \times 0.062428$	kJ/kg _a	Btu/lb _a
Air-specific volume (moist air) v	$\frac{v_{IP}}{\frac{\text{ft}^3}{\text{lb}_a}} = \frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}_a}} \times 16.018453$	$\frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}_a}} = \frac{v_{IP}}{\frac{\text{ft}^3}{\text{lb}_a}} \times 0.062428$	m ³ /kg _a	ft ³ /lb _a
Specific volume (water, water vapor, ice) v_w	$\frac{v_{IP}}{\frac{\text{ft}^3}{\text{lb}}} = \frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}}} \times 16.018453$	$\frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}}} = \frac{v_{IP}}{\frac{\text{ft}^3}{\text{lb}}} \times 0.062428$	m ³ /kg	ft ³ /lb
Humidity ratio W	$W_{IP} = W_{SI}$	$W_{SI} = W_{IP}$	kg _w /kg _a	lb _w /lb _a
Mass fraction ζ	$\zeta_{IP} = \zeta_{SI}$	$\zeta_{SI} = \zeta_{IP}$	kg _w /kg	lb _w /lb
Compression factor Z	$Z_{IP} = Z_{SI}$	$Z_{SI} = Z_{IP}$	-	-

1.3 Calculation Algorithms

1.3.1 Algorithms for Real Moist Air

The properties of moist air are calculated from the modified Hyland-Wexler model given in Herrmann, Kretschmar, and Gatley (HKG) [1], [2]. The modifications incorporate:

- the value for the universal molar gas constant from the CODATA standard by Mohr and Taylor [22]
- the value for the molar mass of dry air from Gatley et al. [17] and that of water from IAPWS-95 [5], [6]
- the calculation of the ideal-gas parts of the heat capacity, enthalpy, and entropy for dry air from the fundamental equation of Lemmon et al. [14]
- the calculation of the ideal-gas parts of the heat capacity, enthalpy, and entropy for water vapor from IAPWS-IF97 [7], [8], [9] for $t \geq 32^\circ\text{F}$ and from IAPWS-95 [5], [6] for $t \leq 32^\circ\text{F}$
- the calculation of the vapor-pressure enhancement factor from the equation given by the models of Hyland and Wexler [21]
- the calculation of the second and third molar virial coefficients B_{aa} and C_{aaa} for dry air from the fundamental equation of Lemmon et al. [14] according to Feistel et al. [24]
- the calculation of the second and third molar virial coefficients B_{ww} and C_{www} for water and steam from IAPWS-95 [5], [6] according to Feistel et al. [24]
- the calculation of the air-water second molar cross-virial coefficient B_{aw} from Harvey and Huang [15]
- the calculation of the air-water third molar cross-virial coefficients C_{aaw} and C_{aww} from Nelson and Sauer [12], [13]
- the calculation of the saturation pressure of water from IAPWS-IF97 [7], [8], [9] for $t \geq 32^\circ\text{F}$ and of the sublimation pressure of water from IAPWS-08 [11] for $t \leq 32^\circ\text{F}$
- the calculation of the isothermal compressibility of saturated liquid water from IAPWS-IF97 [7], [8], [9] for $t \geq 32^\circ\text{F}$ and that of ice from IAPWS-06 [10] for $t \leq 32^\circ\text{F}$ in the determination of the vapor-pressure enhancement factor
- the calculation of Henry's constant from the IAPWS Guideline 2004 [16] in the determination of the enhancement factor. The mole fractions for the three main components of dry air were taken from Lemmon et al. [14]. Argon was not considered in the calculation of Henry's constant in the former research projects, but it is now the third component of dry air.

The transport properties of moist air are calculated from the model given in Herrmann et al. [3], [4].

1.3.2 Algorithms for Steam and Water for Temperatures $t \geq 32^\circ\text{F}$

The p - T diagram in Fig. 1 shows the formulations used for water and water vapor. The temperature range above 32°F is covered by IAPWS-IF97 [7], [8], [9]:

- The saturation line is calculated from the IAPWS-IF97 saturation pressure equation $p_s^{97}(t)$ and saturation temperature equation $t_s^{97}(p)$.
- The properties in the liquid region including saturated-liquid line are calculated from the fundamental equation of the IAPWS-IF97 region 1.
- The properties in the vapor region including saturated-vapor line are calculated from the fundamental equation of the IAPWS-IF97 region 2.

1.3.3 Algorithms for Steam and Ice for Temperatures $t \leq 32^\circ\text{F}$

- The sublimation curve is covered by the IAPWS-08 sublimation pressure equation $p_{\text{subl}}^{08}(t)$ [11] (see Fig. 1).
- The properties of ice including saturated ice are determined by the fundamental equation of the IAPWS-06 [10].
- The properties of vapor including saturated vapor are calculated from the fundamental equation of IAPWS-95 [5], [6].

1.3.4 Overview of the Applied Formulations for Steam, Water, and Ice

The following p - T diagram shows the used IAPWS Formulations and the ranges where they are applied.

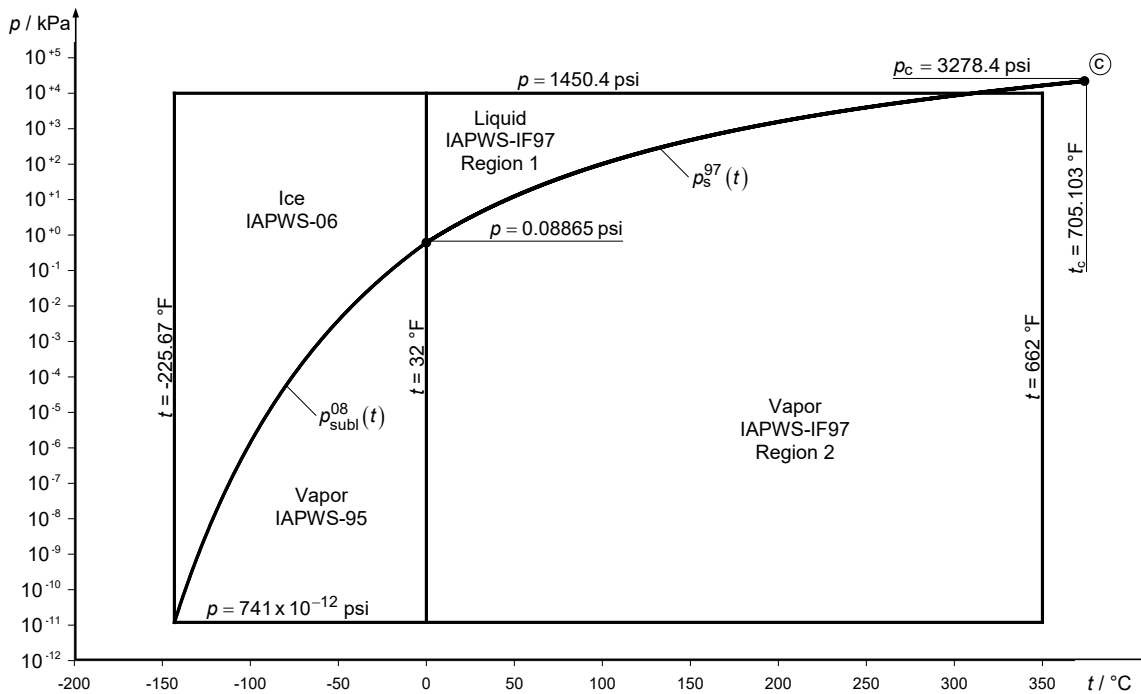


Figure 1: p - T diagram with used IAPWS formulations for steam, water, and ice.

2 Add-In FluidEXL^{Graphics} for Excel[®] for ASHRAE-LibHuAirProp-IP

2.1 Installing FluidEXL^{Graphics}

The FluidEXL^{Graphics} Add-In has been developed to calculate thermophysical properties in Excel[®] more conveniently. Within Excel[®], it enables the direct call of functions relating to real moist air, steam, water, and ice from the ASHRAE-LibHuAirProp-IP property library.

2.1.1 Installing FluidEXL^{Graphics} including LibHuAirProp

In this section, the installation of FluidEXL^{Graphics} and both, LibHuAirProp-IP and LibHuAirProp-SI, is described.

The installation routine for **32-bit** and **64-bit** versions of **MS Excel[®]** is similar. The following instructions are valid for both versions.

After you have downloaded and extracted the zip-file

"CD_FluidEXL_ASHRAE_LibHuAirProp.zip"

you will see the folder

\CD_FluidEXL_ASHRAE_LibHuAirProp\

in your Windows Explorer, Norton Commander, or any other similar program you may be using.

Now, open this folder by double-clicking on it.

Within this folder you will see the following files and folders:

\Chm\

\Files\

\Office32\

\Office64\

FluidEXL_ASHRAE_LibHuAirProp_Users_Guide.pdf

FluidEXL_Graphics.msi

In order to install FluidEXL^{Graphics} including the ASHRAE-LibHuAirProp-IP and ASHRAE-LibHuAirProp-SI property libraries, please run the msi file

FluidEXL_Graphics.msi

which will install ASHRAE LibHuAirProp. During the installation processes the following files and folders

\FLUFT\

\Formulation97\

FluidEXL_Graphics.xlam

FluidEXL_XLL64.xll (64-bit version) **or** FluidEXL_XLL32.xll (32-bit version)

LC.dll

LibHuAirProp_IP.chm

LibHuAirProp_IP.dll

LibHuAirProp_SI.chm

LibHuAirProp_SI.dll

will be copied into the folder

C:\Users\[your name]\AppData\Roaming\FluidEXL_Graphics\
where [your name] is your user name in the Windows system.

The installation of FluidEXLGraphics has been completed.

2.1.2 The FluidEXL *Graphics* Help System

As mentioned earlier, FluidEXL *Graphics* also provides detailed online help functions.

Information on individual property functions may be accessed via the following steps:

- Click "Calculate" in the FluidEXL *Graphics* menu bar.
- Click on the "ASHRAE-LibHuAirProp-IP" library under "Or select a category:" in the "Insert Function" window which will appear.
- Click the "Help on this function" button in the lower left-hand edge of the "Insert Function" window. The help window of the "ASHRAE-LibHuAirProp-IP" library will appear (Figure 2.1.1).

LibHuAirProp_IP

Ausblenden Zurück Vorwärts Startseite Drucken Optionen

Inhalt | Suchen | Favoriten |

$h = f(p,t,W)$

Air-Specific Enthalpy $h = f(p,t,W)$

Function Name:
h_ptW_HAP_IP

Fortran Program:
REAL*8 FUNCTION H_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p	-	Total pressure p in psi
t	-	Temperature t in °F
W	-	Humidity ratio W in lb_w/lb_a

Result:
h_ptW_HAP_IP - Air-specific enthalpy in Btu/lb_a

Range of Validity:

Temperature t :	from -225.67°F to 662°F
Total pressure p :	from 0.00145 psi to 1450.4 psi
Humidity ratio W :	$0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:
- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:
h_ptW_HAP_IP = -1000

References:

$h(p,t,W)$	Herrmann et al. [1], [2]
$h_w(p,t)$	IAPWS-IF97 [7], [8] and IAPWS-06 [11]
$h_a(t)$	Lemmon et al. [14]

Figure 2.1.1: Help Window

If the LibHuAirProp_IP.chm function help cannot be found, you will be redirected to a Microsoft® help website by your standard browser. In this case, the LibHuAirProp_IP.chm file has to be copied into the folder of FluidEXL *Graphics*, in the standard case

C:\Users\[your name]\AppData\Roaming\FluidEXL_Graphics\
where [your name] is your user name in the Windows system (see Sec. 2.1.1).

2.2 Licensing the LibHuAirProp Property Library

The licensing procedure must be carried out when Excel[®] starts up and a FluidEXL *Graphics* prompt message appears. In this case, you will see the "License Information" window for LibHuAirProp (see figure below).

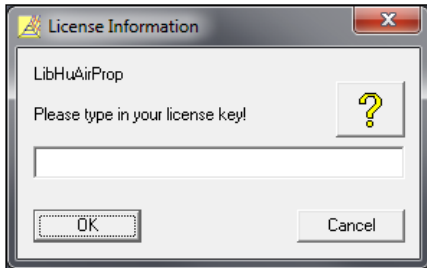


Figure 2.2.1: "License Information" window

Here you are asked to type in the license key which you have obtained from ASHRAE. If you do not have this, or have any questions, you will find contact information on the "Content" page of this User's Guide or by clicking the yellow question mark in the "License Information" window. Then the following window will appear:

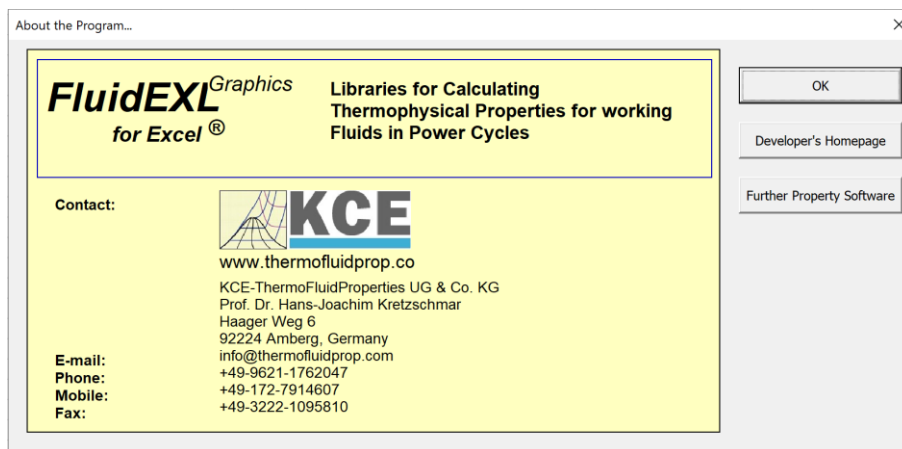


Figure 2.2.2: "About the Program..." window

If you do not enter a valid license it is still possible to start Excel[®] by clicking "Cancel" twice. In this case, the LibHuAirProp property library will display the result "-11111111" for every calculation you ask it to make.

The "License Information" window will appear every time you start Excel[®] unless you uninstall FluidEXL *Graphics* according to the description in section 2.4 of this User's Guide.

Should you not wish to license the LibHuAirProp property library, you have to delete the files

LibHuAirProp_IP.dll	LibHuAirProp_SI.dll
LibHuAirProp_IP.chm	LibHuAirProp_SI.chm

in the installation folder of FluidEXL *Graphics*, in the standard case

C:\Users\[your name]\AppData\Roaming\FluidEXL_Graphics\,

where [your name] is your user name in the Windows system (see Sec. 2.1.1), using an appropriate program such as Explorer[®] or Norton Commander[®].

2.3 Example: Calculation of $h = f(p, t, W)$

We will now calculate, step by step, the air-specific enthalpy h of real moist air as a function of total pressure p , temperature t and humidity ratio W , using FluidEXL *Graphics*. The following description relates to MS Excel® 2019. The use of FluidEXL *Graphics* here is analogous to the description for using it with earlier or later Excel® versions.

Please carry out the following steps:

- Start Excel®
- Enter the value for p in psi into a cell
(Range of validity: $p = 0.00145 \dots 1450.4$ psi)
⇒ e.g.: Enter the value 14.6959 into cell A2
- Enter the value for t in °F into a cell
(Range of validity: $t = -226.67 \dots 662$ °F)
⇒ e.g.: Enter the value 68 into cell B2
- Enter the value for W in lb_w/lb_a (*lb water per lb dry air*) into a cell
(Range of validity: $W = 0 \dots 10$ lb_w/lb_a)
⇒ e.g.: Enter the value 0.01 into cell C2
- Click the cell in which the air-specific enthalpy h in Btu/lb_a is to be displayed
⇒ e.g.: Click cell D2
- Click "Calculate" in the FluidEXL *Graphics* menu bar
The "Insert Function" window appears (see Figure 2.3.1)

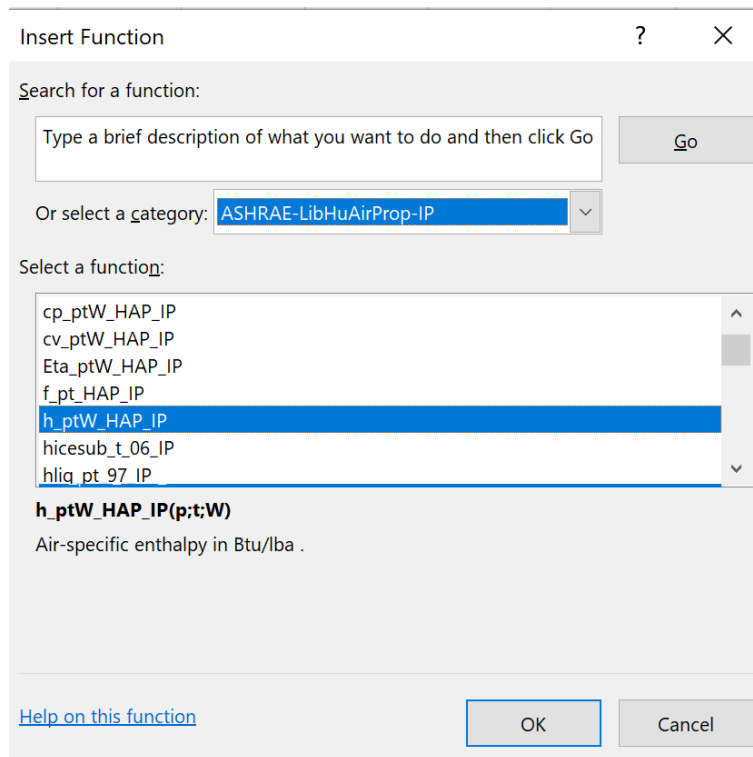


Figure 2.3.1: Choosing the library and function name

- Click on the "ASHRAE-LibHuAirProp-IP" library under "Or select a category:" in the upper part of the window
- Choose the function "h_ptW_HAP_IP" under "Select a function:" directly below that
- Click the "OK" button. The "Function Arguments" menu for the function "h_ptW_HAP_IP" in Figure 2.3.2 will now appear.

The screenshot shows an Excel spreadsheet with the following data:

	A	B	C	D	E
1	p in psi	t in °F	W in lb _w /lb _a	h in Btu/lb _a	
2	14.6959	68	0.010	=h_ptW_HAP_IP(A2;B2;C2)	

The 'Function Arguments' dialog box for the function h_ptW_HAP_IP is open, showing the following arguments and their values:

- P: A2 = 14.6959
- T: B2 = 68
- W: C2 = 0.010

The result of the function is 27.24124326. The dialog also includes a 'Help on this function' link and 'OK' and 'Cancel' buttons.

Figure 2.3.2: Input menu for the function

- The cursor is now situated on the line next to "P" You can now enter the value for the mixture pressure p either by clicking the cell with the value for p , by entering the name of the cell, or by entering the value for p directly into the line next to "P".
⇒ e.g.: [Click on cell A2](#)
- Situate the cursor on the line next to "T" and enter the value for t either by clicking the cell with the value for t , by entering the name of the cell, or by entering the value for t directly into the line next to "T".

⇒ e.g.: Type B2 into the line next to "T"

- Situate the cursor on the line next to "W" and enter the value for the humidity ratio W either by clicking the cell with the value for W , by entering the name of the cell, or by entering the value for W directly into the line next to "W".

⇒ e.g.: Click on cell C2

- It is possible to get detailed information on the "h_ptW_HAP_IP" property function.
- Click the blue "Help on this function" link in the lower left-hand edge of the "Function Arguments" window.

You may be informed that the "LibHuAirProp_IP.chm" function help cannot be found. In this case, confirm the question whether you want to look for it yourself with "Yes." Select the "LibHuAirProp_IP.chm" file in the installation menu of FluidEXL *Graphics* in the window which is opened, the standard being

C:\Users\[your name]\AppData\Roaming\FluidEXL_Graphics\,

where [your name] is your user name in the Windows system (see Sec. 2.1.1), and click "Yes" in order to complete the search.

- Now you should see the help page of the "h_ptW_HAP_IP" property function (see Figure 2.3.3).

h = f(p,t,W)

Air-Specific Enthalpy $h = f(p,t,W)$

Function Name:
h_ptW_HAP_IP

Fortran Program:
REAL*8 FUNCTION H_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p	-	Total pressure p in psi
t	-	Temperature t in °F
W	-	Humidity ratio W in lb _w /lb _a

Result:
h_ptW_HAP_IP - Air-specific enthalpy in Btu/lb_a

Range of Validity:

Temperature t :	from -225.67°F to 662°F
Total pressure p :	from 0.00145 psi to 1450.4 psi
Humidity ratio W :	$0 \leq W \leq 10$ lb _w /lb _a

Comments:
- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:
h_ptW_HAP_IP = -1000

References:

$h(p, t, W)$	Herrmann et al. [1], [2]
$h_w(p, t)$	IAPWS-IF97 [7], [8] and IAPWS-06 [11]
$h_a(t)$	Lemmon et al. [14]

Figure 2.3.3: Help page for the "h_ptW_HAP_IP" function

- Click the "OK" button

The result for h in Btu/lb_a appears in the cell selected above.

⇒ The cell D2 now contains the value 27.2412.

The calculation of $h = f(p, t, W)$ has thus been completed.

You can now arbitrarily change the values for p , t or W in the appropriate cells. The specific enthalpy h is recalculated and updated every time you change the data. This shows that the Excel® data flow and the DLL calculations are working together successfully.

Note:

If the calculation result is -1000, this indicates that the values entered are located outside the range of validity of real moist air. More detailed information on each function and its range of validity is available in Chapter 3.

For further property functions calculable in FluidEXL *Graphics* see the function table in Chapter 1.

2.4 Removing FluidEXL *Graphics* including LibHuAirProp

Should you wish to remove only the LibHuAirProp-IP library, delete the files
LibHuAirProp_IP.dll and LibHuAirProp_IP.chm

in the directory selected for the installation of FluidEXL *Graphics*, the standard being

C:\Users\[your name]\AppData\Roaming\FluidEXL_Graphics\,

where [your name] is your user name in the Windows system (see Sec. 2.1.1), by using an appropriate program such as Windows Explorer®, or Norton Commander®.

Should you wish to remove only the LibHuAirProp-SI library, delete the files

LibHuAirProp_SI.dll and LibHuAirProp_SI.chm

in the directory selected for the installation of FluidEXL *Graphics*, the standard being

C:\Users\[your name]\AppData\Roaming\FluidEXL_Graphics\,

where [your name] is your user name in the Windows system (see Sec. 2.1.1), by using an appropriate program such as Windows Explorer®, or Norton Commander®.

Should you wish to remove FluidEXL *Graphics* from your computer, delete all the files and folders you have copied during the installation process:

\FLUFT\ and \Formulation97\

FluidEXL_Graphics.xlam

FluidEXL_XLL64.xll (64-bit version) or FluidEXL_XLL32.xll (32-bit version)

LC.dll, LibHuAirProp_IP.chm, LibHuAirProp_IP.dll, LibHuAirProp_SI.chm,

LibHuAirProp_SI.dll

in the directory selected for the installation of FluidEXL *Graphics*, the standard being

C:\Users\[your name]\AppData\Roaming\FluidEXL_Graphics\,

where [your name] is your user name in the Windows system (see Sec. 2.1.1), by using an appropriate program such as Windows Explorer®, or Norton Commander®.

Now FluidEXL *Graphics* has been completely removed from your computer.

3 Property Functions of ASHRAE-LibHuAirProp-IP

3.1 Functions for Real Moist Air

Thermal Diffusivity $a = f(p, t, W)$ **Function Name:**

a_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION A_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:a_ptW_HAP_IP - Thermal diffusivity of humid air in ft²/s**Range of Validity:**

Temperature t : from -99.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Thermal diffusivity $a = \frac{\lambda}{\rho \cdot c_p}$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

a_ptW_HAP_IP = -1000

References:

$\lambda(p, t, W)$ Herrmann et al. [3], [4]
 $\rho(p, t, W)$ Herrmann et al. [1], [2]
 $c_p(p, t, W)$ Herrmann et al. [1], [2]

Relative Pressure Coefficient $\alpha_p = f(p, t, W)$
Function Name:

alphap_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION ALPHAP_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

alphap_ptW_HAP_IP - Relative pressure coefficient of humid air in 1/°R

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Relative pressure coefficient $\alpha_p = \frac{1}{p} \left(\frac{\partial p}{\partial T} \right)_v$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

alphap_ptW_HAP_IP = -1000

References:

$\alpha_p(p, t, W)$ Herrmann et al. [1], [2]

Isothermal Stress Coefficient $\beta_p = f(p, t, W)$
Function Name:

betap_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION BETAP_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:betap_ptW_HAP_IP - Isothermal stress coefficient of humid air in lb/ft³**Range of Validity:**

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Isothermal stress coefficient $\beta_p = -\frac{1}{p} \left(\frac{\partial p}{\partial v} \right)_T$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

betap_ptW_HAP_IP = -1000

References: $\beta_p(p, t, W)$ Herrmann et al. [1], [2]

Speed of Sound $c = f(p, t, W)$
Function Name:

c_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION C_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

c_ptW_HAP_IP - Speed of sound of humid air in ft/s

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- Speed of sound $c = v \sqrt{-\left(\frac{\partial p}{\partial v}\right)_s}$

- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

c_ptW_HAP_IP = -1000

References:

$c(p, t, W)$ Herrmann et al. [1], [2]

Isobaric Heat Capacity $c_p = f(p, t, W)$
Function Name:

cp_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION CP_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

cp_ptW_HAP_IP - Isobaric heat capacity of humid air in Btu/(lb °R)

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Isobaric heat capacity $c_p = \left(\frac{\partial h}{\partial T} \right)_p$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

cp_ptW_HAP_IP = -1000

References:
 $c_p(p, t, W)$ Herrmann et al. [1], [2]

Isochoric Heat Capacity $c_v = f(p, t, W)$
Function Name:

cv_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION CV_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

cv_ptW_HAP_IP - Isochoric heat capacity of humid air in Btu/(lb °R)

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Isochoric heat capacity $c_v = \left(\frac{\partial u}{\partial T} \right)_v$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

cv_ptW_HAP_IP = -1000

References:

$c_v(p, t, W)$ Herrmann et al. [3], [4]

Enhancement Factor $f = f(p,t)$ **Function Name:**

f_pt_HAP_IP

Fortran Program:

REAL*8 FUNCTION F_PT_HUAIRPROP(P,T), REAL*8 P,T

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F

Result:

f_pt_HAP_IP - Enhancement factor of water (decimal ratio)

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi

Comments:

- Enhancement factor $f = \frac{\rho_{H_2O,s}}{\rho_s(t)}$

with $\rho_s(t)$ for $t \geq 32^\circ\text{F}$ - Steam pressure of water

for $t < 32^\circ\text{F}$ - Sublimation pressure of water

- Describes the enhancement of the saturation pressure of water in the air atmosphere under elevated pressure

- Derived iteratively from the isothermal compressibility of liquid water, from Henry's constant [15], [16] and from the virial coefficients of air, water, and the air-water mixture

Result for Wrong Input Values:

f_pt_HAP_IP = -1000

References:

$f(p,t)$ Herrmann et al. [1], [2]

Air-Specific Enthalpy $h = f(p, t, W)$
Function Name:

h_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION H_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

h_ptW_HAP_IP - Air-specific enthalpy in Btu/lb_a

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

h_ptW_HAP_IP = -1000

References:

$h(p, t, W)$ Herrmann et al. [1], [2]
 $h_w(p, t)$ IAPWS-IF97 [7], [8] and IAPWS-06 [11]
 $h_a(t)$ Lemmon et al. [14]

Dynamic Viscosity $\eta = f(p, t, W)$

Function Name:

Eta_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION ETA_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:Eta_ptW_HAP_IP - Dynamic viscosity of humid air in (lb s/ft²)**Range of Validity:**

Temperature t : from -99.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- A new very accurate algorithm is implemented between 32°F and 662°F
- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

Eta_ptW_HAP_IP = -1000

References:

$\eta(p, t, W)$ Herrmann et al. [3], [4]
 $\eta_w(p, t)$ IAPWS-IF97 [7], [8] and IAPWS-06 [19]
 $\eta_a(t)$ Lemmon et al. [18]

Isentropic Exponent $\kappa = f(p, t, W)$

Function Name:

Kappa_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION KAPPA_PTW_HUAIRPROP(P,T, W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

Kappa_ptW_HAP_IP - Isentropic exponent

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- Isentropic exponent $\kappa = -\frac{v}{p} \left(\frac{\partial p}{\partial v} \right)_s$
- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets homogeneously mixed) is applied for $t \geq 32^\circ\text{F}$. For temperatures below (ice fog) the value of the saturated state is applied.

Result for Wrong Input Values:

Kappa_ptW_HAP_IP = -1000

References: $v(p, t, W)$ Herrmann et al. [1], [2]

Thermal Conductivity $\lambda = f(p, t, W)$ **Function Name:**

Lambda_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION LAMBDA_PTW_HUAIRPROP(P,T, W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

Lambda_ptW_HAP_IP - Thermal conductivity in Btu/(h ft °R)

Range of Validity:

Temperature t : from -99.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10$ lb_w/lb_a

Comments:

- A new very accurate algorithm is implemented between 32°F and 662°F
- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

Lambda_ptW_HAP_IP = -1000

References:

$\lambda(p, t, W)$ Herrmann et al. [3], [4]
 $\lambda_w(p, t)$ IAPWS-IF97 [7], [8] and IAPWS-08 [20]
 $\lambda_a(t)$ Lemmon et al. [18]

Kinematic Viscosity $\nu = f(p, t, W)$
Function Name:

Ny_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION NY_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:Ny_ptW_HAP_IP - Kinematic viscosity in ft²/s**Range of Validity:**

Temperature t : from -99.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Kinematic Viscosity $\nu = \frac{\eta}{\rho}$

Result for Wrong Input Values:

Ny_ptW_HAP_IP = -1000

References:

$\eta(p, t, W)$ Herrmann et al. [3], [4]
 $\rho(p, t, W)$ Herrmann et al. [1], [2]

Backward Function: Pressure $p = f(t,s,W)$ **Function Name:**

p_tsW_HAP_IP

Fortran Program:

REAL*8 FUNCTION P_TSW_HUAIRPROP(T,S,W), REAL*8 T,S,W

Input Values:

t - Temperature t in °F
 s - Air-specific entropy s in Btu/(lb_a °R)
 W - Humidity ratio W in lb_w/lb_a

Result:

p_tsW_HAP_IP - Total pressure of humid air in psi

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Air-specific entropy s : from -6.32 Btu/(lb_a °R) to 9.32877 Btu/(lb_a °R)
 Humidity ratio W : $0 \leq W \leq 10$ lb_w/lb_a

Comments:- Iteration of total pressure p from $s = f(p,t,W)$ **Result for Wrong Input Values:**

p_tsW_HAP_IP = -1000

References: $s(p,t,W)$ Herrmann et al. [1], [2]

Pressure $p = f(z_{\text{ele}})$ **Function Name:**

p_zele_HAP_IP

Fortran Program:

REAL*8 FUNCTION P_ZELE_HUAIRPROP(ZELE), REAL*8 ZELE

Input Values:z_{ele} - Elevation z_{ele} in ft**Result:**

p_zele_HAP_IP - Pressure of humid air in psi

Range of Validity:Elevation z_{ele} from -16,404 ft to 36,089 ft**Comments:**

- Pressure of humid air from elevation

$$- p(z_{\text{ele}}) = 14.696 \text{ psi} \cdot \left(1 - 6.8754 \cdot 10^{-6} \cdot \frac{z_{\text{ele}}}{\text{ft}} \right)^{5.256}$$

Result for Wrong Input Values:

p_zele_HAP_IP = -1000

References:p(z_{ele}) ASHRAE [23]

Partial Pressure of Air $p_{\text{Air}} = f(p, t, W)$
Function Name:

pAir_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION PAIR_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

pAir_ptW_HAP_IP - Partial pressure of (dry) air in humid air in psi

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- Partial pressure of (dry) air in humid air $p_{\text{Air}} = 1 - p_{\text{H}_2\text{O}}$
- Partial pressure of water vapor at saturation is calculated in case of supersaturated humid air ($W > W_s(p, t)$)
- The temperature value is used to calculate the saturation state

Result for Wrong Input Values:

pAir_ptW_HAP_IP = -1000

References: $p_{\text{H}_2\text{O}}(p, W)$ Herrmann et al. [1], [2]

Partial Pressure of Water Vapor $p_{\text{H}_2\text{O}} = f(p, t, W)$
Function Name:

pH2O_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION PH2O_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

pH2O_ptW_HAP_IP - Partial pressure of water vapor in humid air in psi

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- Partial pressure of water vapor in humid air $p_{\text{H}_2\text{O}} = \frac{W \cdot p}{\left(\frac{R_a}{R_w} + W\right)}$
- Partial pressure of water vapor at saturation is calculated in case of supersaturated humid air ($W > W_s(p, t)$)
- The temperature value is used to calculate the saturation state

Result for Wrong Input Values:

pH2O_ptW_HAP_IP = -1000

References:
 $p_{\text{H}_2\text{O}}(p, W)$ Herrmann et al. [1], [2]

Partial Sat. Pressure of Water Vapor in Humid Air $p_{\text{H}_2\text{O},s} = f(p, t)$
Function Name:

pH2Os_pt_HAP_IP

Fortran Program:

REAL*8 FUNCTION PH2OS_PT_HUAIRPROP(P,T), REAL*8 P,T

Input Values: p - Total pressure p in psi t - Temperature t in °F**Result:**

pH2Os_pt_HAP_IP - Partial saturation pressure of water vapor in humid air in psi

Range of Validity:Temperature t : from -225.67°F to 662°FTotal pressure p : from 0.00145 psi to 1450.4 psi**Comments:**- Partial pressure of water vapor at saturation $p_{\text{H}_2\text{O},s} = f \cdot p_s(t)$ with $p_s(t)$ for $t \geq 32^\circ\text{F}$ - Steam pressure of waterfor $t < 32^\circ\text{F}$ - Sublimation pressure of water**Result for Wrong Input Values:**

pH2Os_pt_HAP_IP = -1000

References: $f(p, t)$ Herrmann et al. [1], [2] $p_s(t)$ for $t \geq 32^\circ\text{F}$ IAPWS-IF97 [7], [8]for $t < 32^\circ\text{F}$ IAPWS-08 [11]

Relative Humidity $\phi = f(p, t, W)$
Function Name:

phi_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION PHI_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

phi_ptW_HAP_IP - Relative humidity (decimal ratio)

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10$ lb_w/lb_a

Comments:

- Relative humidity $\phi = \frac{p_{H2O}}{p_{H2O,s}}$
- This equation is valid for $p_{H2O} \leq p_{H2O,s}$ and for $0 \leq \phi \leq 1$

Result for Wrong Input Values:

phi_ptW_HAP_IP = -1000

References:

$\phi(p, t, W)$ Herrmann et al. [1], [2]

Prandtl Number $Pr = f(p, t, W)$ **Function Name:**

Pr_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION PR_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

Pr_ptW_HAP_IP - Prandtl number

Range of Validity:

Temperature t : from -99.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- Prandtl number $Pr = \frac{\eta \cdot c_p}{\lambda}$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

Pr_ptW_HAP_IP = -1000

References:

$\eta(p, t, W)$ Herrmann et al. [3], [4]
 $c_p(p, t, W)$ Herrmann et al. [3], [4]
 $\lambda(p, t, W)$ Lemmon et al. [20]

Mole Fraction of Air $\psi_{\text{Air}} = f(W)$
Function Name:

PsiAir_W_HAP_IP

Fortran Program:

REAL*8 FUNCTION PSIAIR_W_HUAIRPROP(W), REAL*8 W

Input Values: W - Humidity ratio W in lb_w/lb_a **Result:**PsiAir_W_HAP_IP - Mole fraction of (dry) air in humid air in mol_a/mol **Range of Validity:**Humidity ratio W : $0 \leq W \leq 10 \text{lb}_w/\text{lb}_a$ **Comments:**

- Mole fraction of air $\psi_{\text{Air}} = 1 - \psi_{\text{H}_2\text{O}} = 1 - \left(\frac{W}{\frac{R_a}{R_{\text{H}_2\text{O}}} + W} \right)$

Result for Wrong Input Values:

PsiAir_W_HAP_IP = -1000

References: $\psi_{\text{Air}}(W)$ Herrmann et al. [1], [2]

Mole Fraction of Water $\psi_{H_2O} = f(W)$
Function Name:

PsiH2O_W_HAP_IP

Fortran Program:

REAL*8 FUNCTION PSIH2O_W_HUAIRPROP(W), REAL*8 W

Input Values: W - Humidity ratio W in lb_w/lb_a **Result:**

PsiH2O_W_HAP_IP - Mole fraction of water in humid air in molw/mol

Range of Validity:Humidity ratio W : $0 \leq W \leq 10 lb_w/lb_a$ **Comments:**

- Mole fraction of water $\psi_{H_2O} = \frac{W}{\frac{R_a}{R_{H_2O}} + W}$

Result for Wrong Input Values:

PsiH2O_W_HAP_IP = -1000

References: $\psi_{H_2O}(W)$ Herrmann et al. [1], [2]

Density $\rho = f(p, t, W)$ **Function Name:**

Rho_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION RHO_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:Rho_ptW_HAP_IP - Density of humid air in lb/ft³**Range of Validity:**

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- Density of humid air obtained from air-specific volume: $\rho = \frac{1+W}{v}$

Result for Wrong Input Values:

Rho_ptW_HAP_IP = -1000

References: $\rho(p, t, W)$ Herrmann et al. [1], [2]

Air-Specific Entropy $s = f(p, t, W)$ **Function Name:**

s_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION S_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:s_ptW_HAP_IP - Air-specific entropy in Btu/(lb_a · °R)**Range of Validity:**

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

s_ptW_HAP_IP = -1000

References: $s(p, t, W)$ Herrmann et al. [1], [2]

Backward Function: Temperature $t = f(p, h, \varphi)$
Function Name:

t_phphi_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION T_PHPHI_HUAIRPROP(P,H,PHI), REAL*8 P,H,PHI
```

Input Values:

- p - Total pressure p in psi
- h - Air-specific enthalpy h in Btu/lb_a
- φ - Relative humidity φ (decimal ratio)

Result:

t_phphi_HAP_IP - Temperature from pressure, enthalpy, and relative humidity in °F

Range of Validity:

- Total pressure p : from 0.00145 psi to 1450.4 psi
- Air-specific enthalpy h : from -2469.22 Btu/lb_a to 12772.088 Btu/lb_a
- Relative humidity φ : $0 \leq \varphi \leq 1$

Comments:

- Iteration of temperature t from $h = f(p, t, W)$ using $W = f(p, t, \varphi)$

Result for Wrong Input Values:

t_phphi_HAP_IP = -1000

References: $h(p, t, W)$ Herrmann et al. [1], [2]

Backward Function: Temperature $t = f(p, h, W)$ **Function Name:**

t_phW_HAP_IP

Fortran Program:

REAL*8 FUNCTION T_PHW_HUAIRPROP(P,H,W), REAL*8 P,H,W

Input Values:

p - Total pressure p in psi
 h - Air-specific enthalpy h in Btu/lb_a
 W - Humidity ratio W in lb_w/lb_a

Result:

t_phW_HAP_IP - Temperature from pressure, enthalpy, and humidity ratio in °F

Range of Validity:

Total pressure p : from 0.00145 psi to 1450.4 psi
 Air-specific enthalpy h : from -2469.22 Btu/lb_a to 12772.088 Btu/lb_a
 Humidity ratio W : $0 \leq W \leq 10$ lb_w/lb_a

Comments:- Iteration of temperature t from $h = f(p, t, W)$ **Result for Wrong Input Values:**

t_phW_HAP_IP = -1000

References: $h(p, t, W)$ Herrmann et al. [1], [2]

Backward Function: Temperature $t = f(p,s,W)$
Function Name:

t_psW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION T_PSW_HUAIRPROP(P,S,W), REAL*8 P,S,W
```

Input Values:

p - Total pressure p in psi
 s - Air-specific entropy in Btu/(lb_a · °R)
 W - Humidity ratio W in lb_w/lb_a

Result:

t_psW_HAP_IP - Temperature from pressure, entropy, and humidity ratio in °F

Range of Validity:

Total pressure p : from 0.00145 psi to 1450.4 psi
 Air-specific entropy s : from -6.32 Btu/(lb_a °R) to 9.32877 Btu/(lb_a °R)
 Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- Iteration of temperature t from $s = f(p,t,W)$

Result for Wrong Input Values:

t_psW_HAP_IP = -1000

References:

$s(p,t,W)$ Herrmann et al. [1], [2]

Backward Function: Temperature $t = f(p, t_{wb}, W)$
Function Name:

t_ptwbW_HAP_IP

Fortran Program:

REAL*8 FUNCTION T_PTWBW_HUAIRPROP(P,TWB,W), REAL*8 P,TWB,W

Input Values:

p - Total pressure p in psi
 t_{wb} - Wet-bulb temperature in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

t_ptwbW_HAP_IP - Temperature from pressure, wet bulb temperature and humidity ratio in °F

Range of Validity:

Total pressure p : from 0.00145 psi to 1450.4 psi
Wet bulb temperature t_{wb} : from -225.67°F to 662°F
Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

- Iteration of temperature t from $t_{wb} = f(p, t, W)$

Result for Wrong Input Values:

t_ptwbW_HAP_IP = -1000

References:

$t_{wb}(p, t, W)$ Herrmann et al. [1], [2]

Dew-Point/Frost-Point Temperature $t_d = f(p, W)$
Function Name:

td_pW_HAP_IP

Fortran Program:

REAL*8 FUNCTION TD_PW_HUAIRPROP(P,W), REAL*8 P,W

Input Values:

p - Total pressure p in psi
 W - Humidity ratio W in lb_w/lb_a

Result:

td_pW_HAP_IP - Dew-point/frost-point temperature in °F

Range of Validity:

Total pressure p : from 0.00145 psi to 1450.4 psi
Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$

Comments:

Dew-point temperature $t_d = t_s(\rho_{\text{H}_2\text{O}})$ for $t \geq 32^\circ\text{F}$ (saturation temperature of water in humid air)

$t_d = t_{\text{sub}}(\rho_{\text{H}_2\text{O}})$ for $t \leq 32^\circ\text{F}$ (sublimation temperature of water in humid air)

Result for Wrong Input Values:

td_pW_HAP_IP = -1000

References:

$t_s(\rho_{\text{H}_2\text{O}})$ for $t_d \geq 32^\circ\text{F}$ IAPWS-IF97 [7], [8]
 $t_{\text{sub}}(\rho_{\text{H}_2\text{O}})$ for $t_d \leq 32^\circ\text{F}$ IAPWS-08 [11]
 $\rho_{\text{H}_2\text{O}}$ Herrmann et. al. [1], [2]

Saturation Temperature $t_s = f(p, p_{H_2O})$

Function Name:

ts_ppH2O_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION TS_PPH2O_HUAIRPROP(P,PH2O), REAL*8 P,PH2O
```

Input Values:

p - Total pressure p in psi
 p_{H_2O} - Partial saturation pressure of water p_{H_2O} in psi

Result:

ts_ppH2O_HAP_IP - Saturation temperature of water in humid air in °F

Range of Validity:

Total pressure p : from 0.00145 psi to 1450.4 psi
Partial pressure p_{H_2O} : from 0.00145 psi to 1450.4 psi

Comments:

- Iteration of saturation temperature t_s from $p_{H_2O,s} = f(p, t)$

Result for Wrong Input Values:

ts_ppH2O_HAP_IP = -1000

References:

$p_{H_2O,s}$ Herrmann et. al. [1], [2]

Wet-Bulb/Ice-Bulb Temperature $t_{wb} = f(p, t, W)$
Function Name:

twb_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION TWB_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

twb_ptW_HAP_IP - Wet-bulb/ice-bulb temperature in °F

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10 \text{lb}_w/\text{lb}_a$

Comments:

- Iteration of wet-bulb temperature t_{wb} from $h^{\text{unsaturated}}(p, t, W) = h^{\text{fog}}(p, t_{wb}, W)$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

twb_ptW_HAP_IP = -1000

References: $t_{wb}(p, t, W)$ Herrmann et al. [1], [2]

Air-Specific Internal Energy $u = f(p, t, W)$ **Function Name:**

u_ptW_HAP_IP

Fortran Program:

REAL*8 FUNCTION U_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:u_ptW_HAP_IP - Air-specific internal energy in Btu/lb_a**Range of Validity:**

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10$ lb_w/lb_a

Comments:- Internal energy $u = h - pv$ **Result for Wrong Input Values:**

u_ptW_HAP_IP = -1000

References: $u(p, t, W)$ Herrmann et al. [1], [2]

Air-Specific Volume $v = f(p, t, W)$
Function Name:

v_ptW_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION V_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

v_ptW_HAP_IP - Air-specific volume in ft³/lb_a

Range of Validity:

Temperature t : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi
 Humidity ratio W : $0 \leq W \leq 10$ lb_w/lb_a

Comments:

- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

v_ptW_HAP_IP = -1000

References:

$v(p, t, W)$ Herrmann et al. [1], [2]

Humidity Ratio from Partial Pressure of Water Vapor $W = f(p, t, p_{H_2O})$

Function Name:

W_ptpH2O_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION W_PTPH2O_HUAIRPROP(P,T,PH2O), REAL*8 P,T,PH2O
```

Input Values:

- p - Total pressure p in psi
- t - Temperature t in °F
- p_{H_2O} - Partial pressure of water p_{H_2O} in psi

Result:

W_ptpH2O_HAP_IP - Humidity ratio from pressure, temperature and partial pressure of water vapor in lb_w/lb_a

Range of Validity:

- Total pressure p : from 0.00145 psi to 1450.4 psi
- Temperature t : from -225.67°F to 662°F
- Partial pressure p_{H_2O} : from 0.00145 psi to 1450.4 psi

Comments:

- Iteration of humidity ratio W from $p_{H_2O} = f(p, t, W)$
- Result for supersaturated humid air is W_s

Result for Wrong Input Values:

W_ptpH2O_HAP_IP = -1000

References:

$p_{H_2O}(p, t, W)$ Herrmann et al. [1], [2]

Humidity Ratio from Relative Humidity $W = f(p, t, \varphi)$

Function Name:

W_ptphi_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION W_PTPHI_HUAIRPROP(P,T,PHI), REAL*8 P,T,PHI
```

Input Values:

- p - Total pressure p in psi
- t - Temperature t in °F
- φ - Relative humidity (decimal ratio)

Result:

W_ptphi_HAP_IP - Humidity ratio from pressure, temperature and relative humidity in lb_w/lb_a

Range of Validity:

- Temperature t : from -225.67°F to 662°F
- Total pressure p : from 0.00145 psi to 1450.4 psi
- Relative humidity φ : $0 \leq \varphi \leq 1$

Comments:

- Iteration of humidity ratio W from $\varphi = f(p, t, W)$

Result for Wrong Input Values:

W_ptphi_HAP_IP = -1000

References:

- $\varphi(p, t, W)$ Herrmann et al. [1], [2]

Humidity Ratio from Dew-Point Temperature $W = f(p, t_d)$

Function Name:

$W_ptd_HAP_IP$

Fortran Program:

REAL*8 FUNCTION $W_PTD_HUAIRPROP(P,TD)$, REAL*8 P,TD

Input Values:

p - Total pressure p in psi
 t_d - Dew-point temperature t_d in °F

Result:

$W_ptd_HAP_IP$ - Humidity ratio from pressure and dew-point temperature
 in lb_w/lb_a

Range of Validity:

Dew point temperature t_d : from -225.67°F to 662°F
 Total pressure p : from 0.00145 psi to 1450.4 psi

Comments:

- Iteration of humidity ratio W from $t_d = f(p, W)$

Result for Wrong Input Values:

$W_ptd_HAP_IP = -1000$

References:

$t_d(p, W)$ Herrmann et al. [1], [2]

Humidity Ratio from Wet-Bulb Temperature $W = f(p, t, t_{wb})$

Function Name:

W_pttwb_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION W_PTTWB_HUAIRPROP(P,T,TWB), REAL*8 P,T,TWB
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 t_{wb} - Wet-bulb temperature in °F

Result:

W_pttwb_HAP_IP - Humidity ratio from pressure, temperature and wet-bulb temperature in lb_w/lb_a

Range of Validity:

Total pressure p : from 0.00145 psi to 1450.4 psi
 Temperature t : from -225.67°F to 662°F
 Wet-bulb temperature t_{wb} : from -225.67°F to 662°F

Comments:

- Iteration of humidity ratio W from $t_{wb} = f(p, t, W)$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

W_pttwb_HAP_IP = -1000

References:

$t_{wb}(p, t, W)$ Herrmann et al. [1], [2]

Saturation Humidity Ratio $W_s = f(p, t)$

Function Name:

Ws_pt_HAP_IP

Fortran Program:

REAL*8 FUNCTION WS_PT_HUAIRPROP(P,T), REAL*8 P,T

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F

Result:Ws_pt_HAP_IP - Saturation humidity ratio in lb_w/lb_a**Range of Validity:**

Total pressure p : from 0.00145 psi to 1450.4 psi
 Temperature t : from -225.67°F to 662°F

Comments:

- Calculation of saturation humidity ratio W_s from $W_s = \frac{M_{H_2O}}{M_a} \frac{p_{H_2O,s}}{(p - p_{H_2O,s})}$

Result for Wrong Input Values:

Ws_pt_HAP_IP = -1000

References:

$p_{H_2O,s}$ Herrmann et al. [1], [2]

Mass Fraction of Air $\xi_{\text{Air}} = f(W)$
Function Name:

XiAir_W_HAP_IP

Fortran Program:

```
REAL*8 FUNCTION XIAIR_W_HUAIRPROP(W), REAL*8 W
```

Input Values:

W - Humidity ratio W in lb_w/lb_a

Result:

XiAir_W_HAP_IP - Mass fraction of (dry) air in humid air in lb_a/lb

Range of Validity:

Humidity ratio W : $0 \leq W \leq 10 \text{lb}_w/\text{lb}_a$

Comments:

- Mass fraction of (dry) air $\xi_{\text{Air}} = 1 - \xi_{\text{H}_2\text{O}} = 1 - \frac{W}{1+W}$

Result for Wrong Input Values:

XiAir_W_HAP_IP = -1000

References:

$\xi_{\text{Air}}(W)$ Herrmann et al. [1], [2]

Mass Fraction of Water Vapor in Humid Air $\zeta_{\text{H}_2\text{O}} = f(W)$
Function Name:

XiH2O_W_HAP_IP

Fortran Program:

REAL*8 FUNCTION XIH2O_W_HUAIRPROP(W), REAL*8 W

Input Values: W - Humidity ratio W in lb_w/lb_a **Result:**XiH2O_W_HAP_IP - Mass fraction of water vapor in humid air in lb_w/lb **Range of Validity:**Humidity ratio W : $0 \leq W \leq 10 \text{ lb}_w/\text{lb}_a$ **Comments:**- Mass fraction of water $\zeta_{\text{H}_2\text{O}} = \frac{W}{1+W}$ **Result for Wrong Input Values:**

XiH2O_W_HAP_IP = -1000

References: $\zeta_{\text{H}_2\text{O}}(W)$ Herrmann et al. [1], [2]

Compression Factor $Z = f(p, t, W)$

Function Name:

`Z_ptW_HAP_IP`

Fortran Program:

```
REAL*8 FUNCTION Z_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in psi
 t - Temperature t in °F
 W - Humidity ratio W in lb_w/lb_a

Result:

`Z_ptW_HAP_IP` - Compression factor (decimal ratio)

Range of Validity:

Total pressure p : from 0.00145 psi to 1450.4 psi
 Temperature t : from -225.67°F to 662°F
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Compression factor $Z = 1 + \frac{B_m}{\bar{v}} + \frac{C_m}{\bar{v}^2}$

$$\text{with } \bar{v} = \frac{M}{\rho} = \frac{M v}{1+W}$$

and M is the molar mass of humid air

- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

`Z_ptW_HAP_IP = -1000`

References:

$B_m(t, W), C_m(t, W)$ Herrmann et al. [1], [2]

$\rho(p, t, W), v(p, t, W)$ Herrmann et al. [1], [2]

3.2 Functions for Steam and Water for Temperatures $t \geq 32^\circ\text{F}$

Specific Enthalpy of Liquid Water $h_{\text{liq}} = f(p, t)$
Function Name:

hliq_pt_97_IP

Fortran Program:

```
REAL*8 FUNCTION HLIQ_PT_97(P,T), REAL*8 P,T
```

Input Values:

p - Pressure p in psi
 t - Temperature t in °F

Result:

hliq_pt_97_IP - Specific enthalpy of liquid water in Btu/lb

Range of Validity:

Pressure p : from $p_s(32^\circ\text{F}) = 0.08865$ psi to 1450.4 psi
 Temperature t : from 32°F to 662°F

Comments:

- Specific enthalpy of liquid water $h_{\text{liq}} = h^{97}(p, t)$ (Region 1)

Result for Wrong Input Values:

hliq_pt_97_IP = -1000

References:

$h^{97}(p, t)$ IAPWS-IF97 [7], [8]

Specific Enthalpy of Saturated Liquid Water $h_{\text{liq,s}} = f(t)$
Function Name:

hliqs_t_97_IP

Fortran Program:

REAL*8 FUNCTION HLIQS_T_97(T), REAL*8 T

Input Values: t - Temperature t in °F**Result:**

hliqs_t_97_IP - Specific enthalpy of saturated liquid water in Btu/lb

Range of Validity:Temperature t : from 32°F to 662°F**Comments:**- Specific enthalpy of liquid water $h_{\text{liq,s}} = h^{97}(p_s, t)$ (Region 1)with $p_s = p_s^{97}(t)$ **Result for Wrong Input Values:**

hliqs_t_97_IP = -1000

References: $h^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Specific Enthalpy of Saturated Water Vapor $h_{\text{vap},s} = f(t)$

Function Name:

hvaps_t_97_IP

Fortran Program:

```
REAL*8 FUNCTION HVAPS_T_97(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

hvaps_t_97_IP - Specific enthalpy of saturated water vapor in Btu/lb

Range of Validity:

Temperature t : from 32°F to 662°F

Comments:

- Specific enthalpy of saturated water vapor $h_{\text{vap},s} = h^{97}(p_s, t)$ (Region 2)

with $p_s = p_s^{97}(t)$

Result for Wrong Input Values:

hvaps_t_97_IP = -1000

References:

$h^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Saturation Pressure of Water $p_s = f(t)$

Function Name:

ps_t_97_IP

Fortran Program:

```
REAL*8 FUNCTION PS_T_97(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

ps_t_97_IP - Saturation pressure of water in psi

Range of Validity:

Temperature t : from 32°F to 662°F

Comments:

- Saturation pressure of water $p_s = p_s^{97}(t)$ (Region 4)

Result for Wrong Input Values:

ps_t_97_IP -1000

References:

$p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Specific Entropy of Liquid Water $s_{\text{liq}} = f(p, t)$

Function Name:

sliq_pt_97_IP

Fortran Program:

REAL*8 FUNCTION SLIQ_PT_97(P,T), REAL*8 P,T

Input Values:

p - Pressure p in psi
 t - Temperature t in °F

Result:

sliq_pt_97_IP - Specific entropy of liquid water in Btu/(lb °R)

Range of Validity:

Pressure p : from $p_s(32^\circ\text{F}) = 0.08865$ psi to 1450.4 psi
 Temperature t : from 32°F to 662°F

Comments:- Specific entropy of liquid water $s_{\text{liq}} = s^{97}(p, t)$ (Region 1)**Result for Wrong Input Values:**

sliq_pt_97_IP = -1000

References: $s^{97}(p, t)$ IAPWS-IF97 [7], [8]

Specific Entropy of Saturated Liquid Water $s_{\text{liq},s} = f(t)$
Function Name:

sliqs_t_97_IP

Fortran Program:

REAL*8 FUNCTION SLIQS_T_97(T), REAL*8 T

Input Values: t - Temperature t in °F**Result:**

sliqs_t_97_IP - Specific entropy of saturated liquid water in Btu/(lb °R)

Range of Validity:Temperature t : from 32°F to 662°F**Comments:**- Specific entropy of liquid water $s_{\text{liq},s} = s^{97}(p_s, t)$ (Region 1)with $p_s = p_s^{97}(t)$ **Result for Wrong Input Values:**

sliqs_t_97_IP = -1000

References: $s^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Specific Entropy of Saturated Water Vapor $s_{\text{vap},s} = f(t)$

Function Name:

svaps_t_97_IP

Fortran Program:

```
REAL*8 FUNCTION SVAPS_T_97(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

svaps_t_97_IP - Specific entropy of saturated water vapor in Btu/(lb °R)

Range of Validity:

Temperature t : from 32°F to 662°F

Comments:

- Specific entropy of saturated water vapor $s_{\text{vap},s} = s^{97}(p_s, t)$ (Region 2)

with $p_s = p_s^{97}(t)$

Result for Wrong Input Values:

svaps_t_97_IP = -1000

References:

$s^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Saturation Temperature of Water $t_s = f(p)$

Function Name:

ts_p_97_IP

Fortran Program:

```
REAL*8 FUNCTION TS_P_97(P), REAL*8 P
```

Input Values:

p - Pressure p in psi

Result:

ts_p_97_IP - Saturation temperature of water in °F

Range of Validity:

Pressure p : from 0.08865 psi to 1450.4 psi

Comments:

- Saturation temperature of water $t_s = t_s^{97}(p)$ (Region 4)

Result for Wrong Input Values:

ts_p_97_IP = -1000

References:

$t_s^{97}(p)$ IAPWS-IF97 [7], [8]

Specific Volume of Liquid Water $v_{\text{liq}} = f(p, t)$

Function Name:

vliq_pt_97_IP

Fortran Program:

```
REAL*8 FUNCTION VLIQ_PT_97(P,T), REAL*8 P,T
```

Input Values:

p - Pressure p in psi
 t - Temperature t in °F

Result:

vliq_pt_97_IP - Specific volume of liquid water in ft³/lb

Range of Validity:

Pressure p : from $p_s(32^\circ\text{F}) = 0.08865$ psi to 1450.4 psi
 Temperature t : from 32°F to 662°F

Comments:

- Specific volume of liquid water $v_{\text{liq}} = v^{97}(p, t)$ (Region 1)

Result for Wrong Input Values:

vliq_pt_97_IP = -1000

References:

$v^{97}(p, t)$ IAPWS-IF97 [7], [8]

Specific Volume of Saturated Liquid Water $v_{\text{liq,s}} = f(t)$
Function Name:

vliqs_t_97_IP

Fortran Program:

REAL*8 FUNCTION VLIQS_T_97(T), REAL*8 T

Input Values: t - Temperature t in °F**Result:**vliqs_t_97_IP - Specific volume of saturated liquid water in ft³/lb**Range of Validity:**Temperature t : from 32°F to 662°F**Comments:**- Specific volume of liquid water $v_{\text{liq,s}} = v^{97}(\rho_s, t)$ (Region 1)with $\rho_s = \rho_s^{97}(t)$ **Result for Wrong Input Values:**

vliqs_t_97_IP = -1000

References: $v^{97}(\rho, t), \rho_s^{97}(t)$ IAPWS-IF97 [7], [8]

Specific Volume of Saturated Water Vapor $v_{\text{vap},s} = f(t)$
Function Name:

vvaps_t_97_IP

Fortran Program:

```
REAL*8 FUNCTION  VVAPS_T_97(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

vvaps_t_97_IP - Specific volume of saturated water vapor in ft³/lb

Range of Validity:

Temperature t : from 32°F to 662°F

Comments:

- Specific volume of saturated water vapor $v_{\text{vap},s} = v^{97}(p_s, t)$ (Region 2)

with $p_s = p_s^{97}(t)$

Result for Wrong Input Values:

vvaps_t_97_IP = -1000

References:

$v^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

3.3 Functions for Steam and Ice for Temperatures $t \leq 32^\circ\text{F}$

Specific Enthalpy of Saturated Ice $h_{\text{ice,sub}} = f(t)$
Function Name:

hicesub_t_06_IP

Fortran Program:

```
REAL*8 FUNCTION HICESUB_T_06(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

hicesub_t_06_IP - Specific enthalpy of saturated ice in Btu/lb

Range of Validity:

Temperature t : from -225.67°F to 32°F

Comments:

- Specific enthalpy of saturated ice $h_{\text{ice,sub}} = h^{06}(\rho_{\text{sub}}, t)$

with $\rho_{\text{sub}} = \rho_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

hicesub_t_06_IP = -1000

References:

$h^{06}(\rho, t)$ IAPWS-06 [10]

$\rho_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Specific Enthalpy of Saturated Water Vapor $h_{\text{vap,sub}} = f(t)$
Function Name:

hvapsub_t_95_IP

Fortran Program:

```
REAL*8 FUNCTION HVAPSUB_T_95(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

hvapsub_t_95_IP - Specific enthalpy of saturated water vapor in Btu/lb

Range of Validity:

Temperature t : from -225.67°F to 32°F

Comments:

- Specific enthalpy of saturated water vapor $h_{\text{vap,sub}} = h^{95}(p_{\text{sub}}, t)$

with $p_{\text{sub}} = p_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

hvapsub_t_95_IP = -1000

References:

$h^{95}(p, t)$ IAPWS-95 [5], [6]

$p_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Melting Pressure of Ice $p_{\text{mel}} = f(t)$

Function Name:

pmel_t_08_IP

Fortran Program:

```
REAL*8 FUNCTION PMEL_T_08 (T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

pmel_t_08_IP - Melting pressure of ice in psi

Range of Validity:

Temperature t : from -7.573°F to 32°F

Result for Wrong Input Values:

pmel_t_08_IP = -1000

References:

$p_{\text{mel}}^{08}(t)$ IAPWS-08 [11]

Sublimation Pressure of Ice $p_{\text{sub}} = f(t)$

Function Name:

psub_t_08_IP

Fortran Program:

```
REAL*8 FUNCTION PSUB_T_08 (T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

psub_t_08_IP - Sublimation pressure of ice in psi

Range of Validity:

Temperature t : from -225.67°F to 32°F

Result for Wrong Input Values:

psub_t_08_IP = -1000

References:

$p_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Specific Entropy of Saturated Ice $s_{\text{ice,sub}} = f(t)$

Function Name:

sicesub_t_06_IP

Fortran Program:

```
REAL*8 FUNCTION SICESUB_T_06(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

sicesub_t_06_IP - Specific entropy of saturated ice in Btu/(lb °R)

Range of Validity:

Temperature t : from -225.67°F to 32°F

Comments:

- Specific entropy of saturated ice $s_{\text{ice,sub}} = s^{06}(p_{\text{sub}}, t)$
with $p_{\text{sub}} = p_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

sicesub_t_06_IP = -1000

References:

$s^{06}(p, t)$ IAPWS-06 [10]

$p_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Specific Entropy of Saturated Water Vapor $s_{\text{vap,sub}} = f(t)$
Function Name:

svapsub_t_95_IP

Fortran Program:

REAL*8 FUNCTION SVAPSUB_T_95(T), REAL*8 T

Input Values: t - Temperature t in °F**Result:**

svapsub_t_95_IP - Specific entropy of saturated water vapor in Btu/(lb °R)

Range of Validity:Temperature t : from -225.67°F to 32°F**Comments:**- Specific entropy of saturated water vapor $s_{\text{vap,sub}} = s^{95}(p_{\text{sub}}, t)$ with $p_{\text{sub}} = p_{\text{sub}}^{08}(t)$ **Result for Wrong Input Values:**

svapsub_t_95_IP = -1000

References: $s^{95}(p, t)$ IAPWS-95 [7], [8] $p_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Melting Temperature of Ice $t_{\text{mel}} = f(p)$

Function Name:

tmel_p_08_IP

Fortran Program:

```
REAL*8 FUNCTION TMEL_P_08(P), REAL*8 P
```

Input Values:

p - Pressure p in psi

Result:

tmel_p_08_IP - Melting temperature of ice in °F

Range of Validity:

Pressure p : from p_s (32°F) = 0.08865 psi to 1450.4 psi

Result for Wrong Input Values:

tmel_p_08_IP = -1000

References:

$t_{\text{mel}}^{08}(p)$ IAPWS-08 [11]

Sublimation Temperature of Ice $t_{\text{sub}} = f(p)$

Function Name:

tsub_p_08_IP

Fortran Program:

```
REAL*8 FUNCTION TSUB_P_08(P), REAL*8 P
```

Input Values:

p - Pressure p in psi

Result:

tsub_p_08_IP - Sublimation temperature of ice in °F

Range of Validity:

Pressure p : from $p_{\text{subl}}(-225.67^\circ\text{F}) = 1.7407 \times 10^{-12}$ psi to $p_{\text{subl}}(32^\circ\text{F}) = 0.08865$ psi

Result for Wrong Input Values:

tsub_p_08_IP = -1000

References:

$t_{\text{sub}}^{08}(p)$ IAPWS-08 [11]

Specific Volume of Saturated Ice $v_{\text{ice,sub}} = f(t)$
Function Name:

vicesub_t_06_IP

Fortran Program:

```
REAL*8 FUNCTION VICESUB_T_06(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

vicesub_t_06_IP - Specific volume of saturated ice in ft³/lb

Range of Validity:

Temperature t : from -225.67°F to 32°F

Comments:

- Specific volume of saturated ice $v_{\text{ice,sub}} = v^{06}(\rho_{\text{sub}}, t)$

with $\rho_{\text{sub}} = \rho_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

vicesub_t_06_IP = -1000

References:

$v^{06}(\rho, t)$ IAPWS-06 [10]

$\rho_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Specific Volume of Saturated Water Vapor $v_{\text{vap,sub}} = f(t)$
Function Name:

vvapsub_t_95_IP

Fortran Program:

```
REAL*8 FUNCTION  VVAPSUB_T_95(T), REAL*8 T
```

Input Values:

t - Temperature t in °F

Result:

vvapsub_t_95_IP - Specific volume of saturated water vapor in ft³/lb

Range of Validity:

Temperature t : from -225.67°F to 32°F

Comments:

- Specific volume of saturated water vapor $v_{\text{vap,sub}} = v^{95}(\rho_{\text{sub}}, t)$

with $\rho_{\text{sub}} = \rho_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

vvapsub_t_95_IP = -1000

References:

$v^{95}(\rho, t)$ IAPWS-95 [7], [8]

$\rho_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

4. Property Libraries for Calculating Heat Cycles, Boilers, Turbines and Refrigerators

Water and Steam

Library LibIF97

- Industrial Formulation IAPWS-IF97 (Revision 2007)
- Supplementary Standards IAPWS-IF97-S01, -S03rev, -S04, and -S05
- IAPWS Revised Advisory Note No. 3 on Thermodynamic Derivatives (2008)

Library LibIF97_META

- Industrial Formulation IAPWS-IF97 (Revision 2007) for metastable steam

Humid Combustion Gas Mixtures

Library LibHuGas

- Model: Ideal mixture of the real fluids:
 CO₂ - Span, Wagner H₂O - IAPWS-95
 O₂ - Schmidt, Wagner N₂ - Span et al.
 Ar - Tegeler et al.
 and of the ideal gases:
 SO₂, CO, Ne
 (Scientific Formulation of Bückner et al.)
 Consideration of:
- Dissociation from VDI 4670
 - Poynting effect

Humid Air

Library LibHuAir

- Model: Ideal mixture of the real fluids:
- Dry air from Lemmon et al.
 - Steam, water and ice from IAPWS-IF97 and IAPWS-06
- Consideration of:
- Condensation and freezing of steam
 - Dissociation from VDI 4670
 - Poynting effect from ASHRAE RP-1485

Extremely Fast Property Calculations

- Spline-Based Table
 Look-up Method (SBTL)
Library LibSBTL_IF97
Library LibSBTL_95
Library LibSBTL_HuAir
 For steam, water, humid air, carbon dioxide and other fluids and mixtures according IAPWS Guideline 2015 for Computational Fluid Dynamics (CFD), real-time and non-stationary simulations

Carbon Dioxide Including Dry Ice

Library LibCO2

Formulation of Span and Wagner (1996)

Seawater

Library LibSeaWa

IAPWS Industrial Formulation 2013

Ice

Library LibICE

Ice from IAPWS-06, Melting and sublimation pressures from IAPWS-08, Water from IAPWS-IF97, Steam from IAPWS-95 and -IF97

Ideal Gas Mixtures

Library LibIdGasMix

Model: Ideal mixture of the ideal gases:

Ar	NO	He	Propylene
Ne	H ₂ O	F ₂	Propane
N ₂	SO ₂	NH ₃	Iso-Butane
O ₂	H ₂	Methane	n-Butane
CO	H ₂ S	Ethane	Benzene
CO ₂	OH	Ethylene	Methanol
Air			

Consideration of:

- Dissociation from the VDI Guideline 4670

Library LibIDGAS

Model: Ideal gas mixture from VDI Guideline 4670

Consideration of:

- Dissociation from the VDI Guideline 4670

Humid Air

Library ASHRAE LibHuAirProp

Model: Virial equation from ASHRAE Report RP-1485 for real mixture of the real fluids:
 - Dry air
 - Steam

Consideration of:

- Enhancement of the partial saturation pressure of water vapor at elevated total pressures
www.ashrae.org/bookstore

Dry Air Including Liquid Air

Library LibRealAir

Formulation of Lemmon et al. (2000)

Refrigerants

Ammonia

Library LibNH3

Formulation of Tillner-Roth et al. (1993)

R134a

Library LibR134a

Formulation of Tillner-Roth and Baehr (1994)

Iso-Butane

Library LibButane_Iso

Formulation of Bückner and Wagner (2006)

n-Butane

Library LibButane_n

Formulation of Bückner and Wagner (2006)

Mixtures for Absorption Processes

Ammonia/Water Mixtures

Library LibAmWa

IAPWS Guideline 2001 of Tillner-Roth and Friend (1998)

Helmholtz energy equation for the mixing term (also useable for calculating the Kalina Cycle)

Water/Lithium Bromide Mixtures

Library LibWaLi

Formulation of Kim and Infante Ferreira (2004)

Gibbs energy equation for the mixing term

Liquid Coolants

Liquid Secondary Refrigerants

Library LibSecRef

Liquid solutions of water with

C ₂ H ₆ O ₂	Ethylene glycol
C ₃ H ₈ O ₂	Propylene glycol
C ₂ H ₅ OH	Ethanol
CH ₃ OH	Methanol
C ₃ H ₈ O ₃	Glycerol
K ₂ CO ₃	Potassium carbonate
CaCl ₂	Calcium chloride
MgCl ₂	Magnesium chloride
NaCl	Sodium chloride
C ₂ H ₃ KO ₂	Potassium acetate
CHKO ₂	Potassium formate
LiCl	Lithium chloride
NH ₃	Ammonia

Formulation of the International Institute of Refrigeration (IIR 2010)

Ethanol**Library LibC2H5OH**

Formulation of
Schroeder et al. (2014)

Methanol**Library LibCH3OH**

Formulation of
de Reuck and Craven (1993)

Propane**Library LibPropane**

Formulation of
Lemmon et al. (2009)

Siloxanes as ORC Working Fluids

Octamethylcyclotetrasiloxane $C_8H_{24}O_4Si_4$ **Library LibD4**

Decamethylcyclopentasiloxane $C_{10}H_{30}O_5Si_5$ **Library LibD5**

Tetradecamethylhexasiloxane $C_{14}H_{42}O_6Si_6$ **Library LibMD4M**

Hexamethyldisiloxane $C_6H_{18}OSi_2$ **Library LibMM**

Formulation of Colonna et al. (2006)

Dodecamethylcyclohexasiloxane $C_{12}H_{36}O_6Si_6$ **Library LibD6**

Decamethyltetrasiloxane $C_{10}H_{30}O_3Si_4$ **Library LibMD2M**

Dodecamethylpentasiloxane $C_{12}H_{36}O_4Si_5$ **Library LibMD3M**

Octamethyltrisiloxane $C_8H_{24}O_2Si_3$ **Library LibMDM**

Formulation of Colonna et al. (2008)

Nitrogen and Oxygen**Libraries
LibN2 and LibO2**

Formulations of Span et al. (2000)
and Schmidt and Wagner (1985)

Hydrogen**Library LibH2**

Formulation of
Leachman et al. (2009)

Helium**Library LibHe**

Formulation of
Arp et al. (1998)

Hydrocarbons

Decane $C_{10}H_{22}$ **Library LibC10H22**

Isopentane C_5H_{12} **Library LibC5H12_Iso**

Neopentane C_5H_{12} **Library LibC5H12_Neo**

Isohexane C_6H_{14} **Library LibC6H14**

Toluene C_7H_8 **Library LibC7H8**

Formulation of Lemmon and Span (2006)

Further Fluids

Carbon monoxide **CO** **Library LibCO**

Carbonyl sulfide **COS** **Library LibCOS**

Hydrogen sulfide **H₂S** **Library LibH2S**

Nitrous oxide **N₂O** **Library LibN2O**

Sulfur dioxide **SO₂** **Library LibSO2**

Acetone C_3H_6O **Library LibC3H6O**

Formulation of Lemmon and Span (2006)

**For more information please contact:**

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Fax: +49-3222-1095810

The following thermodynamic and transport properties can be calculated^a:**Thermodynamic Properties**

- Vapor pressure p_s
- Saturation temperature T_s
- Density ρ
- Specific volume v
- Enthalpy h
- Internal energy u
- Entropy s
- Exergy e
- Isobaric heat capacity c_p
- Isochoric heat capacity c_v
- Isentropic exponent κ
- Speed of sound w
- Surface tension σ

Transport Properties

- Dynamic viscosity η
- Kinematic viscosity ν
- Thermal conductivity λ
- Prandtl number Pr
- Thermal diffusivity a

Backward Functions

- $T, v, s(p, h)$
- $T, v, h(p, s)$
- $p, T, v(h, s)$
- $p, T(v, h)$
- $p, T(v, u)$

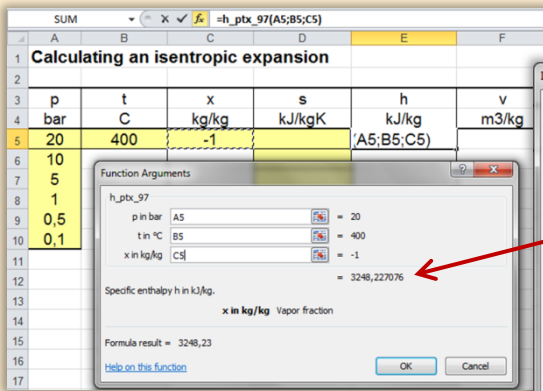
Thermodynamic Derivatives

- Partial derivatives used in process modeling can be calculated.

^a Not all of these property functions are available in all property libraries.

Property Software for Calculating Heat Cycles, Boilers, Turbines and Refrigerators

Add-In FluidEXL^{Graphics} for Excel[®]



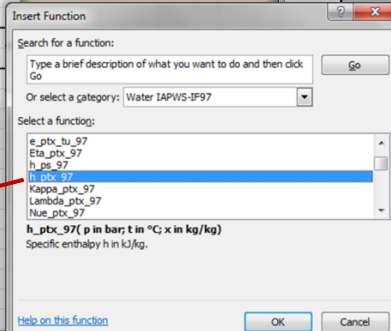
Calculating an isentropic expansion

p	t	x	s	h	v
bar	C	kg/kg	kJ/kgK	kJ/kg	m ³ /kg
20	400	-1		A5;B5;C5	
10					
5					
1					
0,5					
0,1					

Function Arguments dialog for h_ptx_97:

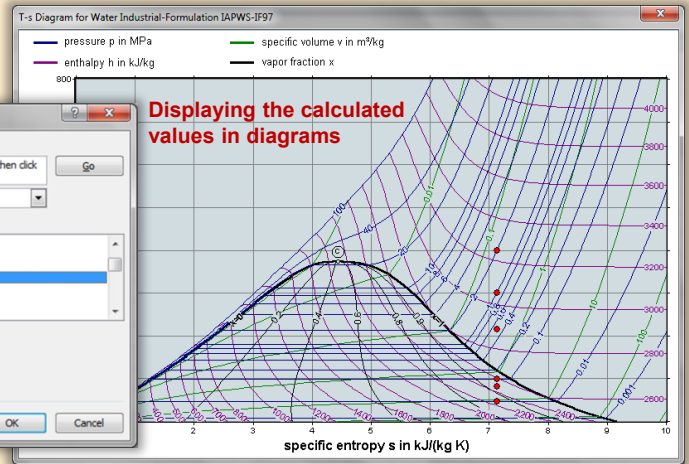
- p in bar: A5 = 20
- t in C: B5 = 400
- x in kg/kg: C5 = -1
- Specific enthalpy h in kJ/kg: = 3248,227076
- Formula result: = 3248,23

Choosing a property library and a function



Insert Function dialog box showing the selection of the h_ptx_97 function from the Water IAPWS-IF97 library.

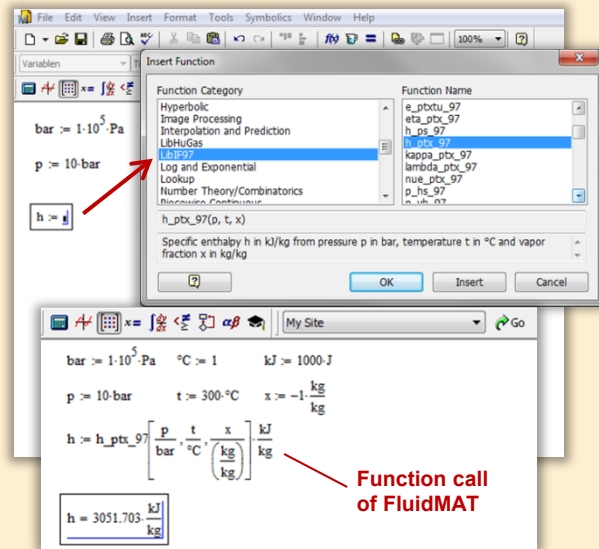
Displaying the calculated values in diagrams



Menu for the input of given property values

Add-On FluidMAT for Mathcad[®]
Add-On FluidPRIME for Mathcad Prime[®]

The property libraries can be used in Mathcad[®] and Mathcad Prime[®].

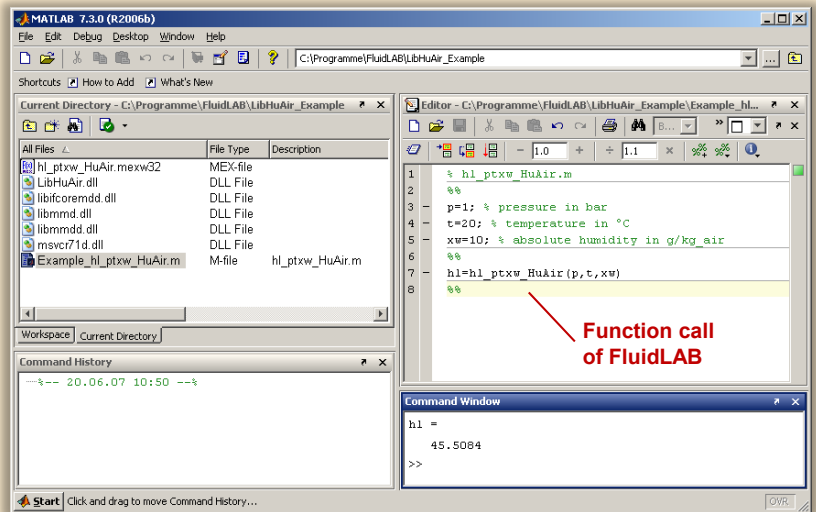


Mathcad interface showing the selection of the h_ptx_97 function and its application in a calculation. The function call is: $h = h_{ptx_97} \left[\frac{p}{\text{bar}}, \frac{t}{\text{C}}, \frac{x}{\left(\frac{\text{kg}}{\text{kg}}\right)} \right] \frac{\text{kJ}}{\text{kg}}$. The result is $h = 3051.703 \frac{\text{kJ}}{\text{kg}}$.

Function call of FluidMAT

Add-On FluidLAB for MATLAB[®] and SIMULINK[®]

Using the Add-In FluidLAB the property functions can be called in MATLAB[®] and SIMULINK[®].

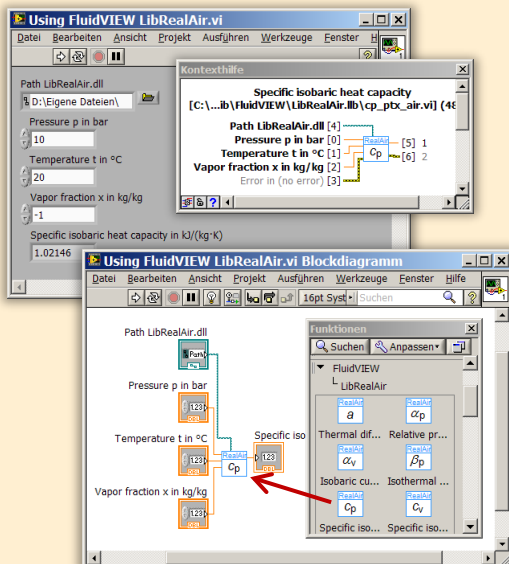


MATLAB 7.3.0 (R2006b) interface showing the FluidLAB function call in a script: `h1 = hl_ptxw_HuAir(p,t,xw)`. The Command Window shows the result: `h1 = 45.5084`.

Function call of FluidLAB

Add-On FluidVIEW for LabVIEW[™]

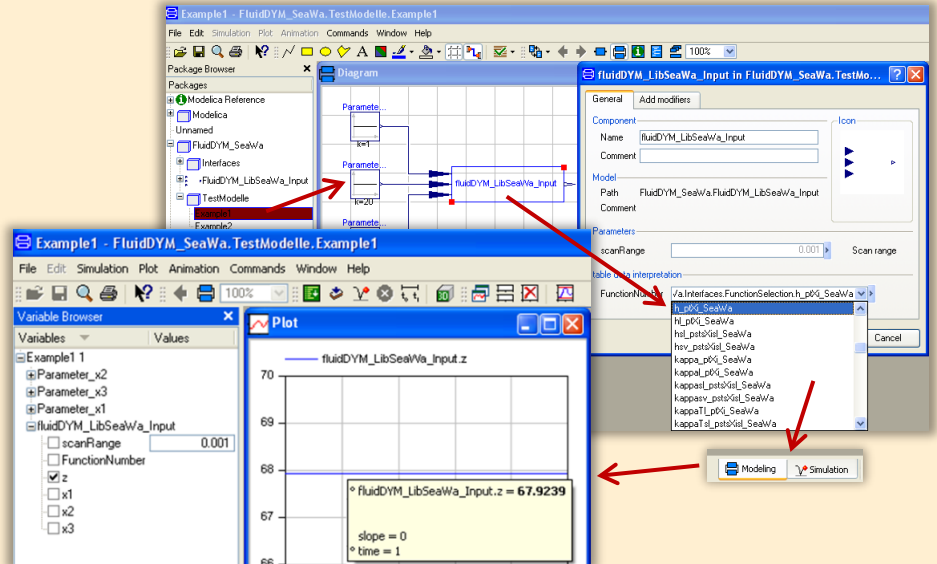
The property functions can be calculated in LabVIEW[™].



LabVIEW interface showing the FluidVIEW function block. Inputs include Pressure p in bar (10), Temperature t in C (20), and Vapor fraction x in kg/kg (-1). The output is Specific isobaric heat capacity in kJ/(kg K) (1.02146).

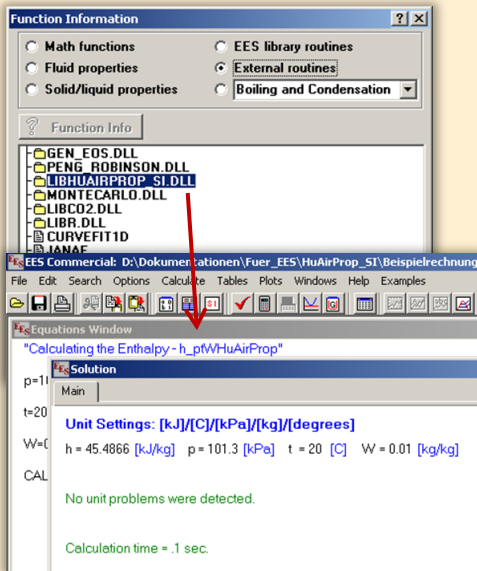
Add-On FluidDYM for DYMOLA[®] (Modelica) and SimulationX[®]

The property functions can be called in DYMOLA[®] and SimulationX[®].



SimulationX interface showing the FluidDYM function block. The output plot shows the value of fluidDYM_LibSeaWa_Input.z as 67.9239.

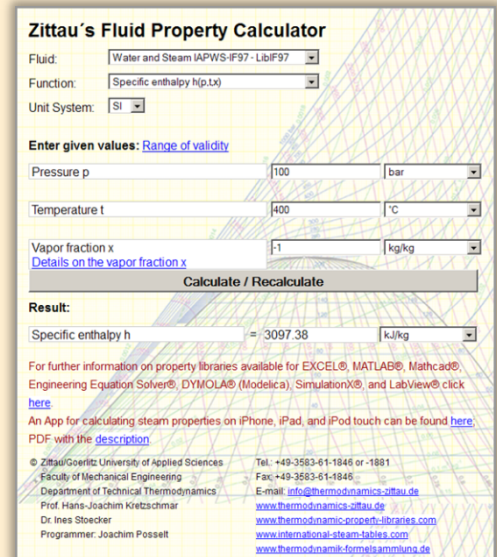
Add-On FluidEES for Engineering Equation Solver®



App International Steam Tables for iPhone, iPad, iPod touch, Android Smartphones and Tablets



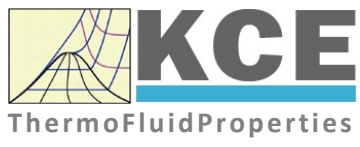
Online Property Calculator at www.thermofluidprop.com



Property Software for Pocket Calculators

<p>FluidCasio</p> <p>fx 9750 G II CFX 9850 fx-GG20 CFX 9860 G Graph 85 ALGEBRA FX 2.0</p>				<p>FluidHP</p> <p>HP 48 HP 49</p>		<p>FluidTI</p> <p>TI Nspire CX CAS TI 83 TI Nspire CAS TI 84 TI 89 TI Voyage 200</p>	
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For more information please contact:



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The following thermodynamic and transport properties^a can be calculated in Excel®, MATLAB®, Mathcad®, Engineering Equation Solver® (EES), DYMOLA® (Modelica), SimulationX® and LabVIEW™:

- | | | | |
|--|---|---|---|
| <p>Thermodynamic Properties</p> <ul style="list-style-type: none"> • Vapor pressure p_s • Saturation temperature T_s • Density ρ • Specific volume v • Enthalpy h • Internal energy u • Entropy s • Exergy e • Isobaric heat capacity c_p • Isochoric heat capacity c_v • Isentropic exponent κ • Speed of sound w • Surface tension σ | <p>Transport Properties</p> <ul style="list-style-type: none"> • Dynamic viscosity η • Kinematic viscosity ν • Thermal conductivity λ • Prandtl number Pr • Thermal diffusivity a | <p>Backward Functions</p> <ul style="list-style-type: none"> • $T, v, s(p, h)$ • $T, v, h(p, s)$ • $p, T, v(h, s)$ • $p, T(v, h)$ • $p, T(v, u)$ | <p>Thermodynamic Derivatives</p> <ul style="list-style-type: none"> • Partial derivatives used in process modeling can be calculated. |
|--|---|---|---|

^a Not all of these property functions are available in all property libraries.

5 References

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6 Satisfied Customers

Period from 2018 to 2022

The following companies and institutions use the property libraries:

- FluidEXL *Graphics* for Excel® incl. VBA
- FluidLAB for MATLAB® and Simulink
- FluidMAT for Mathcad®
- FluidPRIME for Mathcad Prime®
- FluidEES for Engineering Equation Solver® EES
- FluidDYM for Dymola® (Modelica) and SimulationX®
- FluidVIEW for LabVIEW™
- FluidPYT for Python
- FluidJAVA for Java
- DLLs for Windows Applications
- Shared Objects for Linux
- Shared Objects for macOS.

2022

ASTG, Graz, Austria	12/2022
Wandschneider + Gutjahr, Hamburg	
RWE Supply & Trading, Essen	11/2022
Stadtwerke Rosenheim	
CEA, Saclay, France	10/2022
RWE Supply & Trading, Essen	
SEEC Saudi Energy Efficiency Center, Riyadh, Saudi Arabia	
MAN, Copenhagen, Denmark	
Hermeler & Partner Consulting Engineers, Sassenberg	09/2022
Envi Con, Nürnberg	
Drill Cool Systems, Bakersfield CA, USA	
RWE Supply & Trading, Essen	
Maerz Ofenbau, Zürich, Switzerland	
Saale Energie, Schkopau	
ERGO, Dresden	
Mainova, Frankfurt/Main	
Bundeswehr, Koblenz	08/2022
RWE Supply & Trading, Essen	
Grenzbach Corporation, Newnan GE, USA	
AGRANA, Gmuend, Austria	07/2022
MIBRAG, Zeitz	
Hochschule Niederrhein, Krefeld	
ULT, Löbau	06/2022
LEAG, Cottbus	

VPC Group, Vetschau	
Wärme, Hamburg	
ILK, Dresden	
Stricker IB, Küssnacht a. Rigi, Switzerland	
LEAG, Cottbus	05/2022
RWE Supply & Trading, Essen	
IGT Tomalla, Kreuztal	
B+T Engineering, Dübendorf, Switzerland	
Stricker IB, Küssnacht a. Rigi, Switzerland	
Vogelsang & Benning, Bochum	04/2022
Frischli, Rehburg-Loccum	
BPS Consulting, Sprengel	03/2022
HS Hannover, Maschinenbau & BioVT	
M+M Turbinentechnik, Bad Salzungen	
Uni. Strathclyde, Glasgow, UK	02/2022
Delta Energy Group, Jiaozhou City, Qingdao, China	
Wetzel IB, Guben	
Wijbenga, PC Geldermalsen, The Netherlands	
Voith Paper, Heidenheim	
HS Zittau/Görlitz, Maschinenwesen	01/2022
Thermische Abfallbehandlung, Lauterbach	
Webb Institute, Glen Cove NY, USA	
TU Berlin, Umweltverfahrenstechnik	
SachsenEnergie, Dresden	
Doosan, Chang-won-si, Gyeongsangnam-do, South Korea	
KW3, LH Veenendaal, The Netherlands	
Université du Luxembourg, Esch-sur-Alzette	
Enseleit IB, Mansfeld	
Caliqua/Equans, Zürich, Switzerland	
Rudnick & Enners, Alpenrod	

2021

Wenisch IB, Vetschau	12/2021
PPCHEM, Hinwil, Switzerland	
KW3, The Netherlands	
BASF Ludwigshafen	
Air-Consult, Jena	
Sjerp & Jongeneel, RB Zoetermeer, The Netherlands	11/2021
Maerz Ofenbau, Zürich, Switzerland	
RWE Supply & Trading, Essen	
Hahn IB, Dresden	10/2021
Therm, South Africa	
RWE Supply & Trading, Essen	
TH Nürnberg, Verfahrenstechnik	09/2021
RWE Supply & Trading, Essen	
Enseleit IB, Mansfeld	

SachsenEnergie, Dresden	
BSH Hausgeräte, Berlin	
Norsk Energi, Oslo, Norway	08/2021
AKM Industrieanlagen, Haltern	
Drill Cool Systems, Bakersfield CA, USA	
Siemens Energy Global, Erlangen	07/2021
Wulff & Umag, Husum	
Planungsbüro Waidhas, Chemnitz	
Burkhardt Energie Technik, Mühlhausen	
Lücke IB, Paderborn	06/2021
TU Dresden, Energieverfahrenstechnik	
Wärme, Hamburg	
AL-KO Therm, Kötz	
PCK Raffinerie, Schwedt	
Vogelsang & Benning, Bochum	05/2021
MTU, München	
VPC Group, Vetschau	
AVG, Köln	04/2021
TH Ulm, Institut für Fahrzeugtechnik	
Marty IB, Oberwil, Switzerland	
HypTec, Lebring, Austria	
Lopez IB, Getxo, Bizkaia, Spain	03/2021
GM Remediation Systems, Leoben, Austria	
Jager Kältetechnik, Osnabrück	
T&M Automation, GR Leidschendam, The Netherlands	
RWE Supply & Trading, Essen	
Stadtwerke Leipzig	
Beuth Hochschule für Technik, Berlin	
Beleth IB, Woeth	02/2021
ZTL, Thal, Austria	
ETABO Bochum	
RWE Supply & Trading, Essen	
Onyx Germany, Berlin	
TU Dresden, Kältetechnik	
GOHL-KTK, Durmersheim	
Therm Development, South Africa	
thermofin, Heinsdorfergrund	
RWE Supply & Trading, Essen	01/2021
STEAG, Essen	
ETA Energieberatung, Pfaffenhofen	
Enex Power, Kirchseeon	

2020

Drill Cool, Bakersfield CA, USA	12/2020
Manders, The Netherlands	
RWE Supply & Trading, Essen	

NEOWAT Lodz, Poland	
University of Duisburg-Essen, Duisburg	11/2020
Stellenbosch University, South Africa	
University De France-COMTe, France	
RWE, Essen	
STEAG, Herne	
Isenmann Ingenieurbüro	
University of Stuttgart, ITLR, Stuttgart	
Norsk Energi, Oslo, Norway	
TGM Kanis, Nürnberg	
Stadtwerke Neuburg	10/2020
Smurfit Kappa, Roermond, The Netherlands	
RWE, Essen	
Hochschule Zittau/Görlitz, Wirtschaftsingenieurwesen	
Stadtwerke, Neuburg	
ILK, Dresden	
ATESTEO, Alsdorf	
Hochschule Zittau/Görlitz, Maschinenwesen	
TH Nürnberg, Verfahrenstechnik	
Drill Cool, Bakersfield CA,USA	09/2020
RWE, Essen	
2Meyers Ingenieurbüro, Nürnberg	
FELUWA, Mürlenbach	
Stadtwerke Neuburg	
Caverion, Wien, Austria	
GMVA Niederrhein, Oberhausen	
INWAT Lodz, Poland	
Troche Ingenieurbüro, Hayingen	08/2020
CEA Saclay, France	
VPC, Vetschau	07/2020
FSK System-Kälte-Klima, Dortmund	
Exergie Etudes, Sarl, Switzerland	
AWG Wuppertal	
STEAG Energy Services, Zwingenberg	
Hochschule Braunschweig	06/2020
DBI, Leipzig	
GOHL-KTK, Dumersheim	
TU Dresden, Energieverfahrenstechnik	
BASF SE, ESI/EE, Ludwigshafen	
Wärme Hamburg	
Ruchti Ingenieurbüro, Uster, Switzerland	
IWB, Basel, Switzerland	
Midiplan, Bietingen-Bissingen	05/2020
Knieschke, Ingenieurbüro	
RWE, Essen	
Leser, Hamburg	

AGRANA, Gmünd, Austria	
EWT Wassertechnik, Celle	
Hochschule Darmstadt	04/2020
MTU München CCP	
HAW Hamburg	03/2020
Hanon, Novi Jicin, Czech Republic	
TU Dresden, Kältetechnik	
MAN, Copenhagen, Denmark	
EnerTech, Radebeul	02/2020
LEAG, Cottbus	
B+B Engineering Magdeburg	
Hochschule Offenburg	
WIB, Dennheritz	01/2020
Universität Duisburg-Essen, Strömungsmaschinen	
Kältetechnik Dresden-Bremen	
TH Ingolstadt	
Vattenfall AB, Jokkmokk, Sweden	
Fraunhofer UMSICHT	

2019

PEU Leipzig, Rötha	12/2019
MB-Holding, Vestenbergsgreuth	
RWE, Essen	
Georg-Büchner-Hochschule, Darmstadt	11/2019
EEB ENERKO, Aldenhoven	
Robert Benoufa Energietechnik, Wiesloch	
Kehrein & Kubanek Klimatechnik, Moers	10/2019
Hanon Systems Autopal Services, Hluk, Czech Republic	
CEA Saclay, Gif Sur Yvette cedex, France	
Saudi Energy Efficiency Center SEEC, Riyadh, Saudi Arabia	
VPC, Vetschau	09/2019
jGanser PM + Engineering, Forchheim	
Endress+Hauser Flowtec AG, Reinach, Switzerland	
Ruchtli IB, Uster, Switzerland	
ZWILAG Zwischenlager Würenlingen, Switzerland	08/2019
Hochschule Zittau/Görlitz, Faculty Maschinenwesen	
Stadtwerke Neubrandenburg	
Physikalisch Technische Bundesanstalt PTB, Braunschweig	
GMVA Oberhausen	07/2019
Endress+Hauser Flowtec AG, Reinach, Switzerland	
WARNICA, Waterloo, Canada	
MIBRAG, Zeitz	06/2019
Pöyry, Zürich, Switzerland	
RWTH Aachen, Institut für Strahlantriebe und Turbomaschinen	
Midiplan, Bietigheim-Bissingen	
GKS Schweinfurt	

Comparex Leipzig for LEAG, Berlin	06/2018
Münstermann, Telgte	05/2018
TH Nürnberg, Verfahrenstechnik	
Universität Madrid, Madrid, Spanien	
HS Zittau/Görlitz, Wirtschaftsingenieurwesen	
HS Niederrhein, Krefeld	
Wilhelm-Büchner HS, Pfungstadt	03/2018
GRS, Köln	
WIB, Dennheritz	
RONAL AG, Härklingen, Schweiz	02/2018
Ingenieurbüro Leipert, Riegelsberg	
AIXPROCESS, Aachen	
KRONES, Neutraubling	
Doosan Lentjes, Ratingen	01/2018

Part SI Units

1 Property Library ASHRAE-LibHuAirProp-SI

1.1 Function Overview

1.1.1 Function Overview for Real Moist Air

Functional Dependence	Function Name	Property or Function	Unit of the Result	Page
$a = f(p, t, W)$	a_ptW_HAP_SI	Thermal diffusivity	m ² /s	3/2
$\alpha_p = f(p, t, W)$	alphap_ptW_HAP_SI	Relative pressure coefficient	1/K	3/3
$\beta_p = f(p, t, W)$	betap_ptW_HAP_SI	Isothermal stress coefficient	kg/m ³	3/4
$c = f(p, t, W)$	c_ptW_HAP_SI	Speed of sound	m/s	3/5
$c_p = f(p, t, W)$	cp_ptW_HAP_SI	Specific isobaric heat capacity	kJ/(kg·K)	3/6
$c_v = f(p, t, W)$	cv_ptW_HAP_SI	Specific isochoric heat capacity	kJ/(kg·K)	3/7
$f = f(p, t)$	f_pt_HAP_SI	Enhancement factor (decimal ratio)	-	3/8
$h = f(p, t, W)$	h_ptW_HAP_SI	Air-specific enthalpy	kJ/kg _a	3/9
$\eta = f(p, t, W)$	Eta_ptW_HAP_SI	Dynamic viscosity	Pa·s	3/10
$\kappa = f(p, t, W)$	Kappa_ptW_HAP_SI	Isentropic exponent	-	3/11
$\lambda = f(p, t, W)$	Lambda_ptW_HAP_SI	Thermal conductivity	W/(m·K)	3/12
$\nu = f(p, t, W)$	Ny_ptW_HAP_SI	Kinematic viscosity	m ² /s	3/13
$p = f(t, s, W)$	p_tsW_HAP_SI	Pressure of humid air	kPa	3/14
$p = f(z_{\text{ele}})$	p_zele_HAP_SI	Pressure of humid air from elevation	kPa	3/15
$p_{\text{Air}} = f(p, t, W)$	pAIR_ptW_HAP_SI	Partial pressure of dry air in moist air	kPa	3/16
$p_{\text{H}_2\text{O}} = f(p, t, W)$	pH2O_ptW_HAP_SI	Partial pressure of water vapor in moist air	kPa	3/17
$p_{\text{H}_2\text{O}_s} = f(p, t)$	pH2Os_pt_HAP_SI	Partial saturation pressure of water vapor	kPa	3/18

Functional Dependence	Function Name	Property or Function	Unit of the Result	Page
$\phi = f(p, t, W)$	phi_ptW_HAP_SI	Relative humidity (decimal ratio)	-	3/19
$Pr = f(p, t, W)$	Pr_ptW_HAP_SI	PRANDTL number	-	3/20
$\psi_{Air} = f(W)$	PsiAir_W_HAP_SI	Mole fraction of dry air in moist air	mol _a /mol	3/21
$\psi_{H_2O} = f(W)$	PsiH2O_W_HAP_SI	Mole fraction of water vapor in moist air	mol _w /mol	3/22
$\rho = f(p, t, W)$	Rho_ptW_HAP_SI	Density	kg/m ³	3/23
$s = f(p, t, W)$	s_ptW_HAP_SI	Air-specific entropy	kJ/(kg _a ·K)	3/24
$t = f(p, h, \phi)$	t_phphi_HAP_SI	Backward function: temperature from total pressure, air-specific enthalpy and relative humidity	°C	3/25
$t = f(p, h, W)$	t_phW_HAP_SI	Backward function: temperature from total pressure, air-specific enthalpy and humidity ratio	°C	3/26
$t = f(p, s, W)$	t_psW_HAP_SI	Backward function: temperature from total pressure, air-specific entropy and humidity ratio	°C	3/27
$t = f(p, t_{wb}, W)$	t_ptwbW_HAP_SI	Backward function: temperature from total pressure, wet-bulb temperature and humidity ratio	°C	3/28
$t_d = f(p, W)$	td_pW_HAP_SI	Dew-point/frost-point temperature	°C	3/29
$t_s = f(p, p_{H_2O})$	ts_ppH2O_HAP_SI	Backward function: saturation temperature of water from total pressure and partial pressure of water vapor	°C	3/30
$t_{wb} = f(p, t, W)$	twb_ptW_HAP_SI	Wet-bulb/ice-bulb temperature	°C	3/31
$u = f(p, t, W)$	u_ptW_HAP_SI	Air-specific internal energy	kJ/kg _a	3/32
$v = f(p, t, W)$	v_ptW_HAP_SI	Air-specific volume	m ³ /kg _a	3/33
$W = f(p, t, p_{H_2O})$	W_ptpH2O_HAP_SI	Humidity ratio from total pressure, temperature, and partial pressure of water vapor	kg _w /kg _a	3/34
$W = f(p, t, \phi)$	W_ptphi_HAP_SI	Humidity ratio from total pressure, temperature, and relative humidity	kg _w /kg _a	3/35
$W = f(p, t_d)$	W_ptd_HAP_SI	Humidity ratio from total pressure and dew-point temperature	kg _w /kg _a	3/36

Functional Dependence	Function Name	Property or Function	Unit of the Result	Page
$W = f(p, t, t_{wb})$	W_pttwb_HAP_SI	Humidity ratio from total pressure, (dry bulb) temperature, and wet-bulb temperature	kg _w /kg _a	3/37
$W_s = f(p, t)$	Ws_pt_HAP_SI	Saturation humidity ratio	kg _w /kg _a	3/38
$\xi_{Air} = f(W)$	XiAir_W_HAP_SI	Mass fraction of dry air in moist air	kg _a /kg	3/39
$\xi_{H_2O} = f(W)$	XiH2O_W_HAP_SI	Mass fraction of water vapor in moist air	kg _w /kg	3/40
$Z = f(p, t, W)$	Z_ptW_HAP_SI	Compression factor (decimal ratio)	-	3/41

Range of Validity of Thermodynamic Properties

Property	Range of Validity
Pressure:	$0.01 \leq p \leq 10\,000$ kPa
Temperature:	$-143.15 \leq t \leq 350$ °C
Humidity ratio:	$0 \leq W \leq 10$ kg _w /kg _a
Relative humidity:	$0 \leq \phi \leq 1$ (decimal ratio)
Dew-point temperature:	$-143.15 \leq t_d \leq 350$ °C
Wet-bulb temperature:	$-143.15 \leq t_{wb} \leq 350$ °C

Units

Symbol	Quantity	Unit
p	Pressure	kPa
t	Temperature	°C
W	Humidity ratio	kg _w /kg _a (kg water / kg dry air)
ϕ	Relative humidity	(decimal ratio)
t_d	Dew point temperature	°C
t_{wb}	Wet bulb temperature	°C

Range of Validity of Transport Properties

Property	Range of Validity
Pressure:	$0.01 \leq p \leq 10\,000$ kPa
Temperature:	$-73.15 \leq t \leq 350$ °C
Humidity ratio:	$0 \leq W \leq 10$ kg _w /kg _a
Relative humidity:	$0 \leq \phi \leq 1$ (decimal ratio)

Molar Masses

Component	Molar Mass	Reference
Dry Air	28.966 kg/kmol	[17]
Water	18.015268 kg/kmol	[5], [6]

Reference States

Property	Dry Air	Steam, Water, and Ice
Pressure	101.325 kPa	$p_s(0.01^\circ\text{C}) = 0.611657$ kPa
Temperature	0°C	0.01°C
Enthalpy	0 kJ/kg	0.000611782 kJ/kg
Entropy	0 kJ/(kg K)	0 kJ/(kg K)

1.1.2 Function Overview for Steam and Water for Temperatures $t \geq 0^\circ\text{C}$

Functional Dependence	Function Name	Property	Unit of the Result	Page
$h_{\text{liq}} = f(p, t)$	hliq_pt_97_SI	Specific enthalpy of liquid water	kJ/kg	3/43
$h_{\text{liq,s}} = f(t)$	hliqs_t_97_SI	Specific enthalpy of saturated liquid water	kJ/kg	3/44
$h_{\text{vap,s}} = f(t)$	hvaps_t_97_SI	Specific enthalpy of saturated water vapor	kJ/kg	3/45
$p_s = f(t)$	ps_t_97_SI	Saturation pressure of water	kPa	3/46
$s_{\text{liq}} = f(p, t)$	sliq_pt_97_SI	Specific entropy of liquid water	kJ/(kg·K)	3/47
$s_{\text{liq,s}} = f(t)$	sliqs_t_97_SI	Specific entropy of saturated liquid water	kJ/(kg·K)	3/48
$s_{\text{vap,s}} = f(t)$	svaps_t_97_SI	Specific entropy of saturated water vapor	kJ/(kg·K)	3/49
$t_s = f(p)$	ts_p_97_SI	Saturation temperature of water	$^\circ\text{C}$	3/50
$v_{\text{liq}} = f(p, t)$	vliq_pt_97_SI	Specific volume of liquid water	m^3/kg	3/51
$v_{\text{liq,s}} = f(t)$	vliqs_t_97_SI	Specific volume of saturated liquid water	m^3/kg	3/52
$v_{\text{vap,s}} = f(t)$	vvaps_t_97_SI	Specific volume of saturated water vapor	m^3/kg	3/53

Range of Validity

Property	Range of Validity
Pressure:	$0.01 \leq p \leq 10\,000$ kPa
Temperature:	$0 \leq t \leq 350$ °C

Reference State

Property	Water Vapor and Liquid Water
Pressure	$p_s(0.01^\circ\text{C}) = 0.611657$ kPa
Temperature	0.01°C
Enthalpy	0.000611782 kJ/kg
Entropy	0 kJ/(kg K)

Units

Symbol	Quantity	Unit
p	Pressure	kPa
t	Temperature	°C

1.1.3 Function Overview for Steam and Ice for Temperatures $t \leq 0^\circ\text{C}$

Functional Dependence	Function Name	Property	Unit of the Result	Page
$h_{\text{ice,sub}} = f(t)$	hicesub_t_06_SI	Specific enthalpy of saturated ice	kJ/kg	3/55
$h_{\text{vap,sub}} = f(t)$	hvapsub_t_95_SI	Specific enthalpy of saturated water vapor	kJ/kg	3/56
$p_{\text{mel}} = f(t)$	pmel_t_08_SI	Melting pressure of ice	kPa	3/57
$p_{\text{sub}} = f(t)$	psub_t_08_SI	Sublimation pressure of ice	kPa	3/58
$s_{\text{ice,sub}} = f(t)$	sicesub_t_06_SI	Specific entropy of saturated ice	kJ/(kg·K)	3/59
$s_{\text{vap,sub}} = f(t)$	svapsub_t_95_SI	Specific entropy of saturated water vapor	kJ/(kg·K)	3/60
$t_{\text{mel}} = f(p)$	tmel_p_08_SI	Melting temperature of ice	$^\circ\text{C}$	3/61
$t_{\text{sub}} = f(p)$	tsub_p_08_SI	Sublimation temperature of ice	$^\circ\text{C}$	3/62
$v_{\text{ice,sub}} = f(t)$	vicesub_t_06_SI	Specific volume of saturated ice	m^3/kg	3/63
$v_{\text{vap,sub}} = f(t)$	vvapsub_t_95_SI	Specific volume of saturated water vapor	m^3/kg	3/64

Range of Validity

Property	Range of Validity
Pressure:	$p_{\text{sub}}(-143.15^\circ\text{C}) = 1.2002 \times 10^{-11} \leq p \leq 10\,000 \text{ kPa}$
Temperature:	$-143.15 \leq t \leq 0 \quad ^\circ\text{C}$

Units

Symbol	Quantity	Unit
p	Pressure	kPa
t	Temperature	$^\circ\text{C}$

Reference State

Property	Water Vapor and Ice
Pressure	$p_s(0.01^\circ\text{C}) = 0.611657 \text{ kPa}$
Temperature	0.01°C
Enthalpy	$0.000611782 \text{ kJ/kg}$
Entropy	$0 \text{ kJ}/(\text{kg K})$

1.2 Conversion of SI and I-P Units

Property	Conversion: SI Units → I-P Units	Conversion: I-P Units → SI Units	Units SI	Units I-P
Thermal diffusivity a	$\frac{a_{IP}}{\frac{ft^2}{s}} = \frac{a_{SI}}{\frac{m^2}{s}} \times 10.76391042$	$\frac{a_{SI}}{\frac{m^2}{s}} = \frac{a_{IP}}{\frac{ft^2}{s}} \times 0.0929304$	m ² /s	ft ² /s
Relative pressure coefficient α_p	$\frac{\alpha_{p,IP}}{\frac{1}{^\circ R}} = \frac{\alpha_{p,SI}}{\frac{1}{K}} \times \frac{9}{5}$	$\frac{\alpha_{p,SI}}{\frac{1}{K}} = \frac{\alpha_{p,IP}}{\frac{1}{^\circ R}} \times \frac{5}{9}$	1/K	1/°R
Isothermal stress coefficient β_p	$\frac{\beta_{p,IP}}{\frac{lb}{ft^3}} = \frac{\beta_{p,SI}}{\frac{kg}{m^3}} \times 0.062428$	$\frac{\beta_{p,SI}}{\frac{kg}{m^3}} = \frac{\beta_{p,IP}}{\frac{lb}{ft^3}} \times 16.018463$	kg/m ³	lb/ft ³
Speed of sound c	$\frac{c_{IP}}{\frac{ft}{s}} = \frac{c_{SI}}{\frac{m}{s}} \times 3.2808399$	$\frac{c_{SI}}{\frac{m}{s}} = \frac{c_{IP}}{\frac{ft}{s}} \times 0.3048$	m/s	ft/s
Specific isobaric heat capacity c_p	$\frac{c_{p,IP}}{\frac{Btu}{lb \cdot ^\circ R}} = \frac{c_{p,SI}}{\frac{kJ}{kg \cdot K}} \times 0.2388459$	$\frac{c_{p,SI}}{\frac{kJ}{kg \cdot K}} = \frac{c_{p,IP}}{\frac{Btu}{lb \cdot ^\circ R}} \times 4.1868$	kJ/(kg·K)	Btu/(lb·°R)
Specific isochoric heat capacity c_v	$\frac{c_{v,IP}}{\frac{Btu}{lb \cdot ^\circ R}} = \frac{c_{v,SI}}{\frac{kJ}{kg \cdot K}} \times 0.2388459$	$\frac{c_{v,SI}}{\frac{kJ}{kg \cdot K}} = \frac{c_{v,IP}}{\frac{Btu}{lb \cdot ^\circ R}} \times 4.1868$	kJ/(kg·K)	Btu/(lb·°R)
Dynamic viscosity η	$\frac{\eta_{IP}}{\frac{lb \cdot s}{ft^2}} = \frac{\eta_{SI}}{\frac{Pa \cdot s}}{\frac{Pa}{s}} \times 0.02088543$	$\frac{\eta_{SI}}{\frac{Pa \cdot s}} = \frac{\eta_{IP}}{\frac{lb \cdot s}{ft^2}} \times 47.880259$	Pa·s	lb·s/ft ²
Enhancement factor f	$f_{IP} = f_{SI}$	$f_{SI} = f_{IP}$	-	-

Property	Conversion: SI Units → I-P Units	Conversion: I-P Units → SI Units	Units SI	Units I-P
Air-specific enthalpy (moist air) h	$\frac{h_{IP}}{\frac{\text{Btu}}{\text{lb}_a}} = \frac{h_{SI}}{\frac{\text{kJ}}{\text{kg}_a}} \times 0.4299226 + 7.68565365666$	$\frac{h_{SI}}{\frac{\text{kJ}}{\text{kg}_a}} = \left(\frac{h_{IP}}{\frac{\text{Btu}}{\text{lb}_a}} - 7.68565365666 \right) \times 2.326$	kJ/kg _a	Btu/lb _a
Specific enthalpy (water, water vapor, ice) h_w	$\frac{h_{IP}}{\frac{\text{Btu}}{\text{lb}}} = \frac{h_{SI}}{\frac{\text{kJ}}{\text{kg}}} \times 0.4299226$	$\frac{h_{SI}}{\frac{\text{kJ}}{\text{kg}}} = \frac{h_{IP}}{\frac{\text{Btu}}{\text{lb}}} \times 2.326$	kJ/kg	Btu/lb
Isentropic exponent κ	$\kappa_{IP} = \kappa_{SI}$	$\kappa_{SI} = \kappa_{IP}$	-	-
Thermal conductivity λ	$\frac{\lambda_{IP}}{\frac{\text{Btu}}{\text{h ft } ^\circ\text{R}}} = \frac{\lambda_{SI}}{\frac{\text{W}}{\text{m K}}} \times 0.57778932$	$\frac{\lambda_{SI}}{\frac{\text{W}}{\text{m K}}} = \frac{\lambda_{IP}}{\frac{\text{Btu}}{\text{h ft } ^\circ\text{R}}} \times 1.73073467$	W/(m·K)	Btu/(h·ft·°R)
Kinematic viscosity ν	$\frac{\nu_{IP}}{\frac{\text{ft}^2}{\text{s}}} = \frac{\nu_{SI}}{\frac{\text{m}^2}{\text{s}}} \times 10.763910417$	$\frac{\nu_{SI}}{\frac{\text{m}^2}{\text{s}}} = \frac{\nu_{IP}}{\frac{\text{ft}^2}{\text{s}}} \times 0.092903040$	m ² /s	ft ² /s
Pressure p	$\frac{p_{IP}}{\text{psi}} = \frac{p_{SI}}{\text{kPa}} \times 0.14503774$	$\frac{p_{SI}}{\text{kPa}} = \frac{p_{IP}}{\text{psi}} \times 6.894757$	kPa	psi
Relative humidity ϕ	$\phi_{IP} = \phi_{SI}$	$\phi_{SI} = \phi_{IP}$	-	-
Prandtl number Pr	$Pr_{IP} = Pr_{SI}$	$Pr_{SI} = Pr_{IP}$	-	-
Mole fraction ψ	$\psi_{IP} = \psi_{SI}$	$\psi_{SI} = \psi_{IP}$	mol/mol	mol/mol
Density ρ	$\frac{\rho_{IP}}{\frac{\text{lb}}{\text{ft}^3}} = \frac{\rho_{SI}}{\frac{\text{kg}}{\text{m}^3}} \times 0.062428$	$\frac{\rho_{SI}}{\frac{\text{kg}}{\text{m}^3}} = \frac{\rho_{IP}}{\frac{\text{lb}}{\text{ft}^3}} \times 16.018463$	kg/m ³	lb/ft ³
Air-specific entropy (moist air) s	$\frac{s_{IP}}{\frac{\text{Btu}}{\text{lb}_a \text{ } ^\circ\text{R}}} = \frac{s_{SI}}{\frac{\text{kJ}}{\text{kg}_a \text{ K}}} \times 0.2388459 + 0.01616365106$	$\frac{s_{SI}}{\frac{\text{kJ}}{\text{kg}_a \text{ K}}} = \left(\frac{s_{IP}}{\frac{\text{Btu}}{\text{lb}_a \text{ } ^\circ\text{R}}} - 0.01616365106 \right) \times 4.1868$	kJ/(kg _a ·K)	Btu/(lb _a ·°R)

Property	Conversion: SI Units → I-P Units	Conversion: I-P Units → SI Units	Units SI	Units I-P
Specific entropy (water, water vapor, ice) s_w	$\frac{s_{IP}}{\frac{\text{Btu}}{\text{lb}_a \cdot ^\circ\text{R}}} = \frac{s_{SI}}{\frac{\text{kJ}}{\text{kg}_a \cdot \text{K}}} \times 0.23884589$	$\frac{s_{SI}}{\frac{\text{kJ}}{\text{kg}_a \cdot \text{K}}} = \frac{s_{IP}}{\frac{\text{Btu}}{\text{lb}_a \cdot ^\circ\text{R}}} \times 4.1868$	kJ/(kg _a ·K)	Btu/(lb _a ·°R)
Temperature t	$\frac{t_{IP}}{^\circ\text{F}} = \frac{t_{SI}}{^\circ\text{C}} \times \frac{9}{5} + 32$	$\frac{t_{SI}}{^\circ\text{C}} = \left(\frac{t_{IP}}{^\circ\text{F}} - 32 \right) \times \frac{5}{9}$	°C	°F
Air-specific internal energy (moist air) u	$(u = h - pv)$ $\frac{u_{IP}}{\frac{\text{Btu}}{\text{lb}_a}} = \frac{h_{SI}}{\frac{\text{kJ}}{\text{kg}_a}} \times 0.4299226 + 7.68565365666$ $- \frac{p_{SI}}{\text{kPa}} \times 0.145037738 \cdot \frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}_a}} \times 16.018453$	$(u = h - pv)$ $\frac{u_{SI}}{\frac{\text{kJ}}{\text{kg}_a}} = \left(\frac{h_{IP}}{\frac{\text{Btu}}{\text{lb}_a}} - 7.68565365666 \right) \times 2.236$ $- \frac{p_{IP}}{\text{psi}} \times 6.894757293 \cdot \frac{v_{IIP}}{\frac{\text{ft}^3}{\text{lb}_a}} \times 0.062428$	kJ/kg _a	Btu/lb _a
Air-specific volume (moist air) v	$\frac{v_{IP}}{\frac{\text{ft}^3}{\text{lb}_a}} = \frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}_a}} \times 16.018453$	$\frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}_a}} = \frac{v_{IP}}{\frac{\text{ft}^3}{\text{lb}_a}} \times 0.062428$	m ³ /kg _a	ft ³ /lb _a
Specific volume (water, water vapor, ice) v_w	$\frac{v_{IP}}{\frac{\text{ft}^3}{\text{lb}}} = \frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}}} \times 16.018453$	$\frac{v_{SI}}{\frac{\text{m}^3}{\text{kg}}} = \frac{v_{IP}}{\frac{\text{ft}^3}{\text{lb}}} \times 0.062428$	m ³ /kg	ft ³ /lb
Humidity ratio W	$W_{IP} = W_{SI}$	$W_{SI} = W_{IP}$	kg _w /kg _a	lb _w /lb _a
Mass fraction ζ	$\zeta_{IP} = \zeta_{SI}$	$\zeta_{SI} = \zeta_{IP}$	kg _w /kg	lb _w /lb
Compression factor Z	$Z_{IP} = Z_{SI}$	$Z_{SI} = Z_{IP}$	-	-

1.3 Calculation Algorithms

1.3.1 Algorithms for Real Moist Air

The properties of moist air are calculated from the modified Hyland-Wexler model given in Herrmann, Kretzschmar, and Gatley (HKG) [1], [2]. The modifications incorporate:

- the value for the universal molar gas constant from the CODATA standard by Mohr and Taylor [22]
- the value for the molar mass of dry air from Gatley et al. [17] and that of water from IAPWS-95 [5], [6]
- the calculation of the ideal-gas parts of the heat capacity, enthalpy, and entropy for dry air from the fundamental equation of Lemmon et al. [14]
- the calculation of the ideal-gas parts of the heat capacity, enthalpy, and entropy for water vapor from IAPWS-IF97 [7], [8], [9] for $t \geq 0^\circ\text{C}$ and from IAPWS-95 [5], [6] for $t \leq 0^\circ\text{C}$
- the calculation of the vapor-pressure enhancement factor from the equation given by the models of Hyland and Wexler [21]
- the calculation of the second and third molar virial coefficients B_{aa} and C_{aaa} for dry air from the fundamental equation of Lemmon et al. [14] according to Feistel et al. [24]
- the calculation of the second and third molar virial coefficients B_{ww} and C_{www} for water and steam from IAPWS-95 [5], [6] according to Feistel et al. [24]
- the calculation of the air-water second molar cross-virial coefficient B_{aw} from Harvey and Huang [15]
- the calculation of the air-water third molar cross-virial coefficients C_{aaw} and C_{aww} from Nelson and Sauer [12], [13]
- the calculation of the saturation pressure of water from IAPWS-IF97 [7], [8], [9] for $t \geq 0^\circ\text{C}$ and of the sublimation pressure of water from IAPWS-08 [11] for $t \leq 0^\circ\text{C}$
- the calculation of the isothermal compressibility of saturated liquid water from IAPWS-IF97 [7], [8], [9] for $t \geq 0^\circ\text{C}$ and that of ice from IAPWS-06 [10] for $t \leq 0^\circ\text{C}$ in the determination of the vapor-pressure enhancement factor
- the calculation of Henry's constant from the IAPWS Guideline 2004 [16] in the determination of the enhancement factor. The mole fractions for the three main components of dry air were taken from Lemmon et al. [14]. Argon was not considered in the calculation of Henry's constant in the former research projects, but it is now the third component of dry air.

The transport properties of moist air are calculated from the model given in Herrmann et al. [3], [4].

1.3.2 Algorithms for Steam and Water for Temperatures $t \geq 0^\circ\text{C}$

The p - T diagram in Fig. 1 shows the formulations used for water and water vapor. The temperature range above 0°C is covered by IAPWS-IF97 [7], [8], [9]:

- The saturation line is calculated from the IAPWS-IF97 saturation pressure equation $p_s^{97}(t)$ and saturation temperature equation $t_s^{97}(p)$.
- The properties in the liquid region including saturated-liquid line are calculated from the fundamental equation of the IAPWS-IF97 region 1.
- The properties in the vapor region including saturated-vapor line are calculated from the fundamental equation of the IAPWS-IF97 region 2.

1.3.3 Algorithms for Steam and Ice for Temperatures $t \leq 0^\circ\text{C}$

- The sublimation curve is covered by the IAPWS-08 sublimation pressure equation $p_{\text{subl}}^{08}(t)$ [11] (see Fig. 1).
- The properties of ice including saturated ice are determined by the fundamental equation of the IAPWS-06 [10].
- The properties of vapor including saturated vapor are calculated from the fundamental equation of IAPWS-95 [5], [6].

1.3.4 Overview of the Applied Formulations for Steam, Water, and Ice

The following p - T diagram shows the used IAPWS Formulations and the ranges where they are applied.

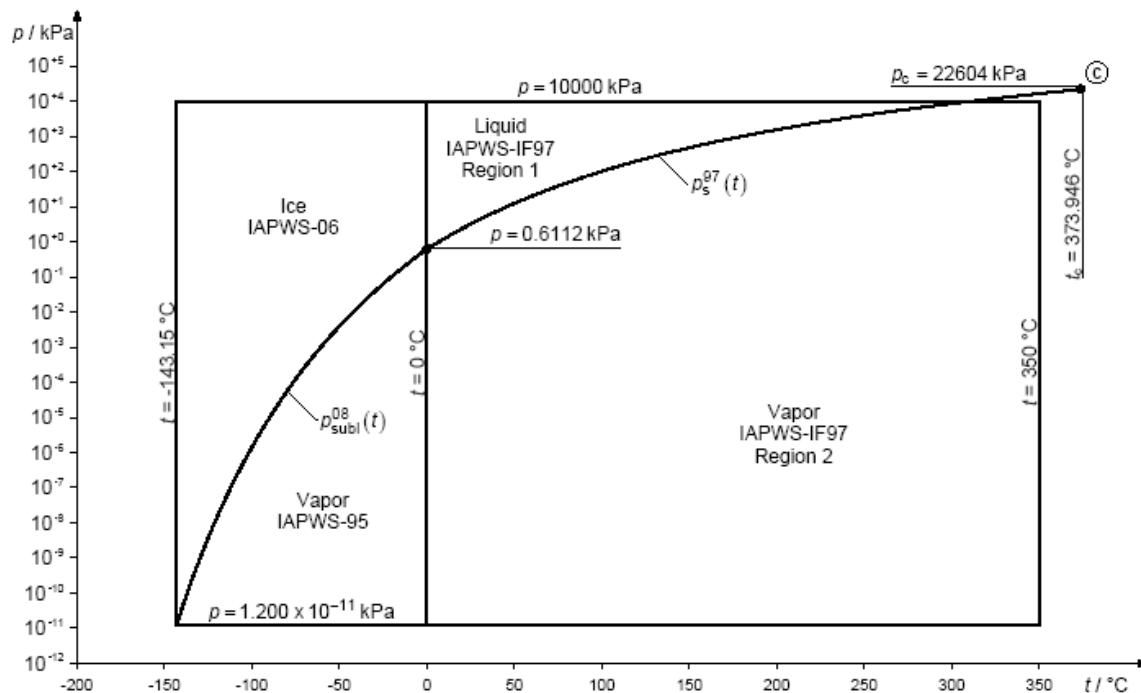


Figure 1: p - T diagram with used IAPWS formulations for steam, water, and ice.

2 Add-In FluidEXL^{Graphics} for Excel[®] for ASHRAE-LibHuAirProp-SI

2.1 Installing FluidEXL^{Graphics}

The FluidEXL^{Graphics} Add-In has been developed to calculate thermophysical properties in Excel[®] more conveniently. Within Excel[®], it enables the direct call of functions relating to real moist air, steam, water, and ice from the ASHRAE-LibHuAirProp-SI property library.

The installation of FluidEXL^{Graphics} and ASHRAE-LibHuAirProp_SI is described in Section 2.1 in "Part I-P Units" of this User's Guide.

2.2 Example: Calculation of $h = f(p, t, W)$

We will now calculate, step by step, the air-specific enthalpy h of real moist air as a function of total pressure p , temperature t and humidity ratio W , using FluidEXL^{Graphics}.

Please carry out the following steps:

- Start Excel[®]
- Enter the value for p in kPa into a cell
(Range of validity: $p = 0.01 \dots 10\,000$ kPa)
⇒ e.g.: Enter the value 101.325 into cell A2
- Enter the value for t in °C into a cell
(Range of validity: $t = -143.15 \dots 350$ °C)
⇒ e.g.: Enter the value 20 into cell B2
- Enter the value for W in kg_w/kg_a (*kg water per kg air*) into a cell
(Range of validity: $W = 0 \dots 10$ kg_w/kg_a)
⇒ e.g.: Enter the value 0.01 into cell C2
- Click the cell in which the air-specific enthalpy h in kJ/kg_a is to be displayed
⇒ e.g.: Click the cell D2
- Click "Calculate" in the FluidEXL^{Graphics} menu bar.
The "Insert Function" window appears (see Figure 2.1.1.)

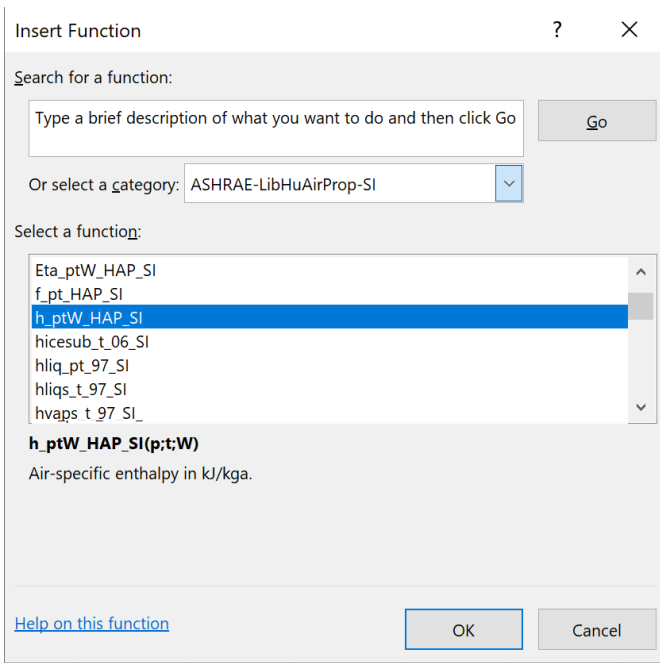


Figure 2.1.1: Choosing the library and function name

- Search and click the "ASHRAE-LibHuAirProp-SI" library under "Or select a category:" in the upper part of the window
 - Search and click the "h_ptW_HAP_SI" function under "Select a function:" right below
 - Click the "OK" button
- The "Function Arguments" menu for the function "h_ptW_HAP_SI" in the next figure will now appear.

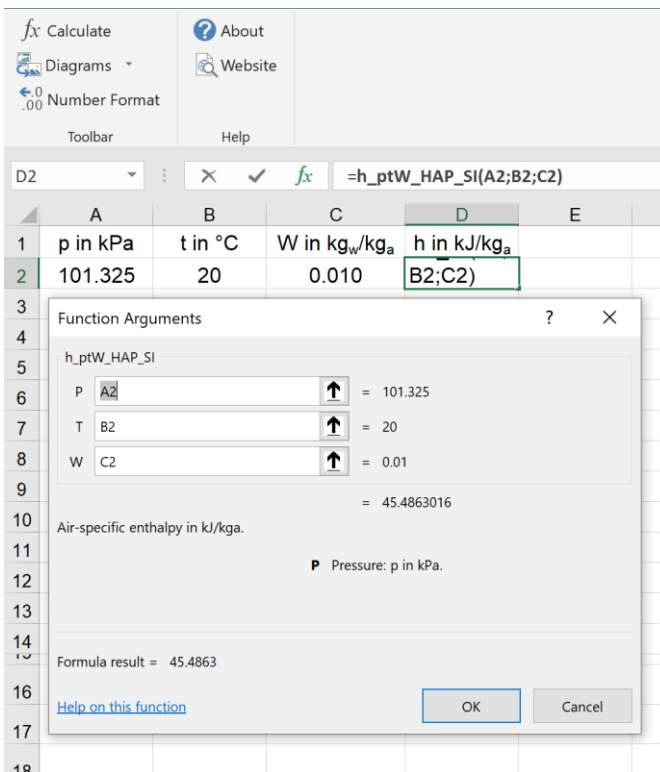


Figure 2.1.2: Input menu for the function

- The cursor is now situated on the line next to "P". You can now enter the value for the mixture pressure p either by clicking the cell with the value for p , by entering the name of the cell, or by entering the value for p directly into the line next to "P".

⇒ e. g.: [Click the cell A2](#)

- Situate the cursor on the line next to "T" and enter the value for t either by clicking the cell with the value for t , by entering the name of the cell, or by entering the value for t directly into the line next to "T".

⇒ e. g.: [Type B2 into the line next to "T"](#)

- Situate the cursor on the line next to "W" and enter the value for the humidity ratio W either by clicking the cell with the value for W , by entering the name of the cell, or by entering the value for W directly into the line next to "W".

⇒ e. g.: [Click the cell C2](#)

- Here it is possible to get detailed information on the "h_ptW_HAP_SI" property function.
- Click the blue "Help on this function" link in the lower left-hand edge of the "Function Arguments" window.

You may be informed that the "LibHuAirProp_SI.chm" function help cannot be found. In this case, confirm the question whether you want to look for it yourself with "Yes". Search and click on the "LibHuAirProp_SI.chm" file in the installation menu of FluidEXL *Graphics* in the window which is opened, in the standard case

C:\Users\[your name]\AppData\Roaming\FluidEXL_Graphics\,

where [your name] is your user name in the Windows system (see Sec. 2.1.1 in "Part I-P Units" of this User's Guide), and click "Yes" in order to complete the search.

- Now you should see the help page of the "h_ptW_HAP_SI" property function (see Figure 2.1.3).

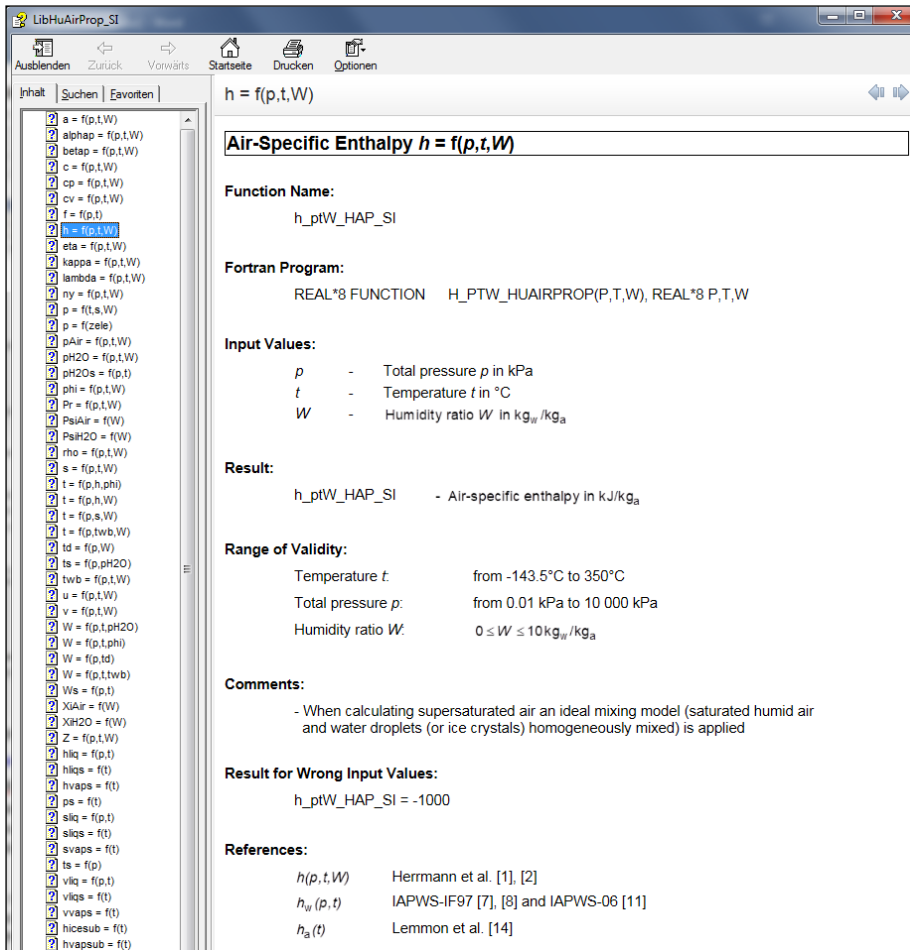


Figure 2.1.3: Help page for the "h_ptW_HAP_SI" function

- Click the "OK" button

The result for h in kJ/kg_a appears in the cell selected above.

⇒ The cell D2 now contains the value 45.4863016.

The calculation of $h = f(p, t, W)$ has thus been completed.

You can now arbitrarily change the values for p , t or W in the appropriate cells. The specific enthalpy h is recalculated and updated every time you change the data. This shows that the Excel® data flow and the DLL calculations are working together successfully

Note:

If the calculation results in -1000 , this indicates that the values entered are located outside the range of validity of real moist air. More detailed information on each function and its range of validity is available in Chapter 3.

For further property functions calculable in FluidEXL *Graphics* see the function table in Chapter 1.

2.3 Removing FluidEXL *Graphics* including LibHuAirProp

The de-installation of FluidEXL *Graphics* and ASHRAE-LibHuAirProp_SI is described in Section 2.4 in "Part I-P Units" of this User's Guide.

3 Property Functions of ASHRAE-LibHuAirProp-SI

3.1 Functions for Real Moist Air

Thermal Diffusivity $a = f(p, t, W)$
--

Function Name:

a_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION A_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:a_ptW_HAP_SI - Thermal diffusivity of humid air in m²/s**Range of Validity:**

Temperature t : from -73.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Thermal diffusivity $a = \frac{\lambda}{\rho \cdot c_p}$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

a_ptW_HAP_SI = -1000

References:

$\lambda(p, t, W)$ Herrmann et al. [3], [4]
 $\rho(p, t, W)$ Herrmann et al. [1], [2]
 $c_p(p, t, W)$ Herrmann et al. [1], [2]

Relative Pressure Coefficient $\alpha_p = f(p, t, W)$
Function Name:

alphap_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION ALPHAP_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

alphap_ptW_HAP_SI - Relative pressure coefficient of humid air in 1/K

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Relative pressure coefficient $\alpha_p = \frac{1}{p} \left(\frac{\partial p}{\partial T} \right)_v$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

alphap_ptW_HAP_SI = -1000

References:

$\rho(p, t, W)$ Herrmann et al. [1], [2]

Isothermal Stress Coefficient $\beta_p = f(p, t, W)$
Function Name:

betap_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION BETAP_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:betap_ptW_HAP_SI - Isothermal stress coefficient of humid air in kg/m³**Range of Validity:**

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Isothermal stress coefficient $\beta_p = -\frac{1}{p} \left(\frac{\partial p}{\partial v} \right)_T$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

betap_ptW_HAP_SI = -1000

References: $v(p, t, W)$ Herrmann et al. [1], [2]

Speed of Sound $c = f(p, t, W)$

Function Name:

c_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION C_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

c_ptW_HAP_SI - Speed of sound of humid air in m/s

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Speed of sound $c = v \sqrt{-\left(\frac{\partial p}{\partial v}\right)_s}$

- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

c_ptW_HAP_SI = -1000

References:

$v(p, t, W)$ Herrmann et al. [1], [2]

Specific Isobaric Heat Capacity $c_p = f(p, t, W)$
Function Name:

cp_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION CP_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

cp_ptW_HAP_SI - Specific isobaric heat capacity of humid air in kJ/(kg K)

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Specific isobaric heat capacity $c_p = \left(\frac{\partial h}{\partial T} \right)_p$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

cp_ptW_HAP_SI = -1000

References: $h(p, t, W)$ Herrmann et al. [1], [2]

Specific Isochoric Heat Capacity $c_v = f(p, t, W)$
Function Name:

cv_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION CV_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

cv_ptW_HAP_SI - Specific isochoric heat capacity of humid air in kJ/(kg K)

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Specific isochoric heat capacity $c_v = \left(\frac{\partial u}{\partial T} \right)_v$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

cv_ptW_HAP_SI = -1000

References:

$c_v(p, t, W)$ Herrmann et al. [3], [4]

Enhancement Factor $f = f(p,t)$ **Function Name:**

f_pt_HAP_SI

Fortran Program:

REAL*8 FUNCTION F_PT_HUAIRPROP(P,T), REAL*8 P,T

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C

Result:

f_pt_HAP_SI - Enhancement factor of water (decimal ratio)

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa

Comments:

- Enhancement factor $f = \frac{\rho_{\text{H}_2\text{O},s}}{\rho_s(t)}$

with $\rho_s(t)$ for $t \geq 0.01^\circ\text{C}$ - Steam pressure of water

for $t < 0.01^\circ\text{C}$ - Sublimation pressure of water

- Describes the enhancement of the saturation pressure of water in the air atmosphere under elevated pressure

- Derived iteratively from the isothermal compressibility of liquid water, from Henry's constant [15], [16] and from the virial coefficients of air, water, and the air-water mixture

Result for Wrong Input Values:

f_pt_HAP_SI = -1000

References:

$f(p,t)$ Herrmann et al. [1], [2]

Air-Specific Enthalpy $h = f(p, t, W)$
--

Function Name:

h_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION H_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:h_ptW_HAP_SI - Air-specific enthalpy in kJ/kg_a **Range of Validity:**

Temperature t : from -143.5°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{kg}_w/\text{kg}_a$

Comments:

- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

h_ptW_HAP_SI = -1000

References:

$h(p, t, W)$ Herrmann et al. [1], [2]
 $h_w(p, t)$ IAPWS-IF97 [7], [8] and IAPWS-06 [11]
 $h_a(t)$ Lemmon et al. [14]

Dynamic Viscosity $\eta = f(p, t, W)$ **Function Name:**

Eta_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION ETA_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

Eta_ptW_HAP_SI - Dynamic viscosity of humid air in Pa s

Range of Validity:

Temperature t : from -73.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- A new very accurate algorithm is implemented between 0°C and 350°C
- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

Eta_ptW_HAP_SI = -1000

References:

$\eta(p, t, W)$ Herrmann et al. [3], [4]
 $\eta_a(t)$ Lemmon et al. [18]
 $\eta_w(p, t)$ IAPWS-IF97 [7], [8] and IAPWS-08 [19]

Isentropic Exponent $\kappa = f(p, t, W)$

Function Name:

Kappa_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION KAPPA_PTW_HUAIRPROP(P,T, W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

Kappa_ptW_HAP_SI - Isentropic exponent

Range of Validity:

Temperature t : from -143.5°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Isentropic exponent $\kappa = -\frac{v}{p} \left(\frac{\partial p}{\partial v} \right)_s$
- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets homogeneously mixed) is applied for $t \geq 0.01^\circ\text{C}$. For temperatures below (ice fog) the value of the saturated state is applied.

Result for Wrong Input Values:

Kappa_ptW_HAP_SI = -1000

References:

$v(p, t, W)$ Herrmann et al. [1], [2]

Thermal Conductivity $\lambda = f(p, t, W)$
Function Name:

Lambda_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION LAMBDA_PTW_HUAIRPROP(P,T, W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

Lambda_ptW_HAP_SI - Thermal conductivity in $\text{W}/(\text{m K})$

Range of Validity:

Temperature t : from -73.5°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- A new very accurate algorithm is implemented between 0°C and 350°C
- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

Lambda_ptW_HAP_SI = -1000

References:

$\lambda(p, t, W)$ Herrmann et al. [3], [4]
 $\lambda_a(t)$ Lemmon et al. [18]
 $\lambda_w(p, t)$ IAPWS-IF97 [7], [8] and IAPWS-08 [20]

Kinematic Viscosity $\nu = f(p, t, W)$

Function Name:

Ny_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION NY_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

Ny_ptW_HAP_SI - Kinematic viscosity in m^2/s

Range of Validity:

Temperature t : from -73.5°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Kinematic Viscosity $\nu = \frac{\eta}{\rho}$

Result for Wrong Input Values:

Ny_ptW_HAP_SI = -1000

References:

$\eta(p, t, W)$ Herrmann et al. [3], [4]
 $\rho(p, t, W)$ Herrmann et al. [1], [2]

Backward Function: Total Pressure $p = f(t,s,W)$ **Function Name:**

p_tsW_HAP_SI

Fortran Program:

REAL*8 FUNCTION P_TSW_HUAIRPROP(T,S,W), REAL*8 T,S,W

Input Values:

t - Temperature t in °C
 s - Air-specific entropy s in kJ/(kg_a K)
 W - Humidity ratio W in kg_w/kg_a

Result:

p_tsW_HAP_SI - Total pressure in kPa

Range of Validity:

Temperature t : from -143.5°C to 350°C
 Air-specific entropy s : from -26.53 kJ/(kg_a K) to 38.990 kJ/(kg_a K)
 Humidity ratio W : $0 \leq W \leq 10$ kg_w/kg_a

Comments:- Iteration of total pressure p from $s = f(p,t,W)$ **Result for Wrong Input Values:**

p_tsW_HAP_SI = -1000

References: $s(p,t,W)$ Herrmann et al. [1], [2]

Pressure $p = f(z_{\text{ele}})$
Function Name:

p_zele_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION P_ZELE_HUAIRPROP(ZELE), REAL*8 ZELE
```

Input Values:

z_{ele} - Elevation z_{ele} in m

Result:

p_zele_HAP_SI - Pressure of humid air in kPa

Range of Validity:

Elevation z_{ele} from -5,000 m to 11,000 m

Comments:

- Pressure of humid air from elevation

$$- p(z_{\text{ele}}) = 101.325 \text{ kPa} \cdot \left(1 - 2.25577 \cdot 10^{-5} \cdot \frac{z_{\text{ele}}}{\text{m}} \right)^{5.256}$$

Result for Wrong Input Values:

p_zele_HAP_SI = -1000

References:

$p(z_{\text{ele}})$ ASHRAE [23]

Partial Pressure of Dry Air $p_{\text{Air}} = f(p, t, W)$
Function Name:

pAir_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION PAIR_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

pAir_ptW_HAP_SI - Partial pressure of (dry) air in humid air in kPa

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Partial pressure of (dry) air in humid air $p_{\text{Air}} = 1 - p_{\text{H}_2\text{O}}$
- Partial pressure of water vapor at saturation is calculated in case of supersaturated humid air ($W > W_s(p, t)$)
- The temperature value is used to calculate the saturation state

Result for Wrong Input Values:

pAir_ptW_HAP_SI = -1000

References:
 $p_{\text{H}_2\text{O}}(p, W)$ Herrmann et al. [1], [2]

Partial Pressure of Water Vapor $p_{\text{H}_2\text{O}} = f(p, t, W)$

Function Name:

pH2O_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION PH2O_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

pH2O_ptW_HAP_SI - Partial pressure of water vapor in humid air in kPa

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Partial pressure of water vapor in humid air $p_{\text{H}_2\text{O}} = \frac{W \cdot p}{\left(\frac{R_a}{R_w} + W\right)}$
- Partial pressure of water vapor at saturation is calculated in case of supersaturated humid air ($W > W_s(p, t)$)
- The temperature value is used to calculate the saturation state

Result for Wrong Input Values:

pH2O_ptW_HAP_SI = -1000

References:

$p_{\text{H}_2\text{O}}(p, W)$ Herrmann et al. [1], [2]

Partial Saturation Pressure of Water Vapor $p_{\text{H}_2\text{O},s} = f(p, t)$
Function Name:

pH2Os_pt_HAP_SI

Fortran Program:

REAL*8 FUNCTION PH2OS_PT_HUAIRPROP(P,T), REAL*8 P,T

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C

Result:

pH2Os_pt_HAP_SI - Partial saturation pressure of water vapor in humid air in kPa

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa

Comments:

- Partial pressure of steam at saturation $p_{\text{H}_2\text{O},s} = f \cdot p_s(t)$
 with $p_s(t)$ for $t \geq 0.01^\circ\text{C}$ - Steam pressure of water
 for $t < 0.01^\circ\text{C}$ - Sublimation pressure of water

Result for Wrong Input Values:

pH2Os_pt_HAP_SI = -1000

References:

$f(p, t)$		Herrmann et al. [1], [2]
$p_s(t)$	for $t \geq 0.01^\circ\text{C}$	IAPWS-IF97 [7], [8]
	for $t < 0.01^\circ\text{C}$	IAPWS-08 [11]

Relative Humidity $\varphi = f(p, t, W)$

Function Name:

phi_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION PHI_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

phi_ptW_HAP_SI - Relative humidity (decimal ratio)

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Relative humidity $\varphi = \frac{p_{\text{H}_2\text{O}}}{p_{\text{H}_2\text{O},s}}$

- This equation is valid for $p_{\text{H}_2\text{O}} \leq p_{\text{H}_2\text{O},s}$ and for $0 \leq \varphi \leq 1$

Result for Wrong Input Values:

phi_ptW_HAP_SI = -1000

References:

$\varphi(p, t, W)$ Herrmann et al. [1], [2]

Prandtl Number $Pr = f(p, t, W)$ **Function Name:**

Pr_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION PR_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

Pr_ptW_HAP_SI - Prandtl number

Range of Validity:

Temperature t : from -73.5°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Prandtl number $Pr = \frac{\eta \cdot c_p}{\lambda}$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

Pr_ptW_HAP_SI = -1000

References:

$\eta(p, t, W)$ Herrmann et al. [3], [4]
 $c_p(p, t, W)$ Herrmann et al. [3], [4]
 $\lambda(p, t, W)$ Lemmon et al. [20]

Mole Fraction of Dry Air $\psi_{\text{Air}} = f(W)$
Function Name:

PsiAir_W_HAP_SI

Fortran Program:

REAL*8 FUNCTION PSIAIR_W_HUAIRPROP(W), REAL*8 W

Input Values: W - Humidity ratio W in kg_w/kg_a **Result:**PsiAir_W_HAP_SI - Mole fraction of (dry) air in humid air in mol_a/mol **Range of Validity:**Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$ **Comments:**

- Mole fraction of air $\psi_{\text{Air}} = 1 - \psi_{\text{H}_2\text{O}} = 1 - \left(\frac{W}{\frac{R_a}{R_{\text{H}_2\text{O}}} + W} \right)$

Result for Wrong Input Values:

PsiAir_W_HAP_SI = -1000

References: $\psi_{\text{Air}}(W)$ Herrmann et al. [1], [2]

Mole Fraction of Water $\psi_{H_2O} = f(W)$
Function Name:

PsiH2O_W_HAP_SI

Fortran Program:

REAL*8 FUNCTION PSIH2O_W_HUAIRPROP(W), REAL*8 W

Input Values: W - Humidity ratio W in kg_w/kg_a **Result:**

PsiH2O_W_HAP_SI - Mole fraction of water in humid air in molw/mol

Range of Validity:Humidity ratio W : $0 \leq W \leq 10 kg_w/kg_a$ **Comments:**

- Mole fraction of water $\psi_{H_2O} = \frac{W}{\frac{R_a}{R_{H_2O}} + W}$

Result for Wrong Input Values:

PsiH2O_W_HAP_SI = -1000

References: $\psi_{H_2O}(W)$ Herrmann et al. [1], [2]

Density $\rho = f(p, t, W)$ **Function Name:**

Rho_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION RHO_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:Rho_ptW_HAP_SI - Density of humid air in kg/m^3 **Range of Validity:**

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{kg}_w/\text{kg}_a$

Comments:

- Density of humid air obtained from air-specific volume: $\rho = \frac{1+W}{v}$

Result for Wrong Input Values:

Rho_ptW_HAP_SI = -1000

References: $\rho(p, t, W)$ Herrmann et al. [1], [2]

Air-Specific Entropy $s = f(p, t, W)$ **Function Name:**

s_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION S_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:s_ptW_HAP_SI - Air-specific entropy in kJ/(kg_a K)**Range of Validity:**

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

s_ptW_HAP_SI = -1000

References:s(p, t, W) Herrmann et al. [1], [2]

Backward Function: Temperature $t = f(p, h, \varphi)$
Function Name:

t_phphi_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION T_PHPHI_HUAIRPROP(P,H,PHI), REAL*8 P,H,PHI
```

Input Values:

- p - Total pressure p in kPa
- h - Air-specific enthalpy h in kJ/kg_a
- φ - Relative humidity φ (decimal ratio)

Result:

t_phphi_HAP_SI - Temperature from pressure, enthalpy, and relative humidity in °C

Range of Validity:

- Total pressure p : from 0.01 kPa to 10 000 kPa
- Air-specific enthalpy h : from -5745 kJ/kg_a to 29690 kJ/kg_a
- Relative humidity φ : $0 \leq \varphi \leq 1$

Comments:

- Iteration of temperature t from $h = f(p, t, W)$ using $W = f(p, t, \varphi)$

Result for Wrong Input Values:

t_phphi_HAP_SI = -1000

References:

$h(p, t, W)$ Herrmann et al. [1], [2]

Backward Function: Temperature $t = f(p, h, W)$ **Function Name:**

t_phW_HAP_SI

Fortran Program:

REAL*8 FUNCTION T_PHW_HUAIRPROP(P,H,W), REAL*8 P,H,W

Input Values:

p - Total pressure p in kPa
 h - Air-specific enthalpy h in kJ/kg_a
 W - Humidity ratio W in kg_w/kg_a

Result:

t_phW_HAP_SI - Temperature from pressure, enthalpy, and humidity ratio in °C

Range of Validity:

Total pressure p : from 0.01 kPa to 10 000 kPa
 Air-specific enthalpy h : from -5745 kJ/kg_a to 29690 kJ/kg_a
 Humidity ratio W : $0 \leq W \leq 10$ kg_w/kg_a

Comments:- Iteration of temperature t from $h = f(p, t, W)$ **Result for Wrong Input Values:**

t_phW_HAP_SI = -1000

References: $h(p, t, W)$ Herrmann et al. [1], [2]

Backward Function: Temperature $t = f(p, s, W)$
Function Name:

t_psW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION T_PSW_HUAIRPROP(P,S,W), REAL*8 P,S,W
```

Input Values:

p - Total pressure p in kPa
 s - Air-specific entropy s in kJ/(kg_a K)
 W - Humidity ratio W in kg_w/kg_a

Result:

t_psW_HAP_SI - Temperature from pressure, entropy, and humidity ratio in °C

Range of Validity:

Total pressure p : from 0.01 kPa to 10 000 kPa
 Air-specific entropy s : from -26.53 kJ/(kg_a K) to 38.990 kJ/(kg_a K)
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Iteration of temperature t from $s = f(p, t, W)$

Result for Wrong Input Values:

t_psW_HAP_SI = -1000

References:

$s(p, t, W)$ Herrmann et al. [1], [2]

Backward Function: Temperature $t = f(p, t_{wb}, W)$
Function Name:

t_ptwbW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION T_PTWBW_HUAIRPROP(P,TWB,W), REAL*8 P,TWB,W
```

Input Values:

p - Total pressure p in kPa
 t_{wb} - Wet-bulb temperature in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

t_ptwbW_HAP_SI - Temperature from pressure, wet bulb temperature and humidity ratio in °C

Range of Validity:

Total pressure p : from 0.01 kPa to 10 000 kPa
Wet bulb temperature t_{wb} : from -143.15°C to 350°C
Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Iteration of temperature t from $t_{wb} = f(p, t, W)$

Result for Wrong Input Values:

t_ptwbW_HAP_SI = -1000

References:

$t_{wb}(p, t, W)$ Herrmann et al. [1], [2]

Dew-Point/Frost-Point Temperature $t_d = f(p, W)$
Function Name:

td_pW_HAP_SI

Fortran Program:

REAL*8 FUNCTION TD_PW_HUAIRPROP(P,W), REAL*8 P,W

Input Values:

p - Total pressure p in kPa
 W - Humidity ratio W in kg_w/kg_a

Result:

td_pW_HAP_SI - Dew-point/frost-point temperature in °C

Range of Validity:

Total pressure p : from 0.01 kPa to 10 000 kPa
Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

Dew-point temperature $t_d = t_s(\rho_{\text{H}_2\text{O}})$ for $t \geq 0.01^\circ\text{C}$ (saturation temperature of water in humid air)

$t_d = t_{\text{sub}}(\rho_{\text{H}_2\text{O}})$ for $t \leq 0.01^\circ\text{C}$ (sublimation temperature of water in humid air)

Result for Wrong Input Values:

td_pW_HAP_SI = -1000

References:

$t_s(\rho_{\text{H}_2\text{O}})$ for $t_d \geq 0.01^\circ\text{C}$ IAPWS-IF97 [7], [8]

$t_{\text{sub}}(\rho_{\text{H}_2\text{O}})$ for $t_d \leq 0.01^\circ\text{C}$ IAPWS-08 [11]

$\rho_{\text{H}_2\text{O}}$ Herrmann et. al. [1], [2]

Saturation Temperature $t_s = f(p, p_{H_2O})$
Function Name:

ts_ppH2O_HAP_SI

Fortran Program:

REAL*8 FUNCTION TS_PPH2O_HUAIRPROP(P,PH2O), REAL*8 P,PH2O

Input Values:

p - Total pressure p in kPa
 p_{H_2O} - Partial pressure of water vapor p_{H_2O} in kPa

Result:

ts_ppH2O_HAP_SI - Saturation temperature in °C

Range of Validity:

Total pressure p : from 0.01 kPa to 10 000 kPa
 Partial Pressure p_{H_2O} : from 0.01 kPa to 10 000 kPa

Comments:

- Iteration of saturation temperature t_s from $p_{H_2O,s} = f(p, t)$

Result for Wrong Input Values:

ts_ppH2O_HAP_SI = -1000

References:

$p_{H_2O,s}$ Herrmann et. al. [1], [2]

Wet-Bulb/Ice-Bulb Temperature $t_{wb} = f(p, t, W)$
Function Name:

twb_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION TWB_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

twb_ptW_HAP_SI - Wet-bulb/ice-bulb temperature in °C

Range of Validity:

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$

Comments:

- Iteration of wet-bulb/ice-bulb temperature t_{wb}
 from $h^{\text{unsaturated}}(p, t, W) = h^{\text{fog}}(p, t_{wb}, W)$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

twb_ptW_HAP_SI = -1000

References: $t_{wb}(p, t, W)$ Herrmann et al. [1], [2]

Air-Specific Internal Energy $u = f(p, t, W)$ **Function Name:**

u_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION U_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:u_ptW_HAP_SI - Air-specific internal energy in kJ/kg_a**Range of Validity:**

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10$ kg_w/kg_a

Comments:- Internal energy $u = h - pv$ **Result for Wrong Input Values:**

u_ptW_HAP_SI = -1000

References: $u(p, t, W)$ Herrmann et al. [1], [2]

Air-Specific Volume $v = f(p, t, W)$
--

Function Name:

v_ptW_HAP_SI

Fortran Program:

REAL*8 FUNCTION V_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:v_ptW_HAP_SI - Air-specific volume in m^3/kg_a **Range of Validity:**

Temperature t : from -143.15°C to 350°C
 Total pressure p : from 0.01 kPa to 10 000 kPa
 Humidity ratio W : $0 \leq W \leq 10 \text{kg}_w/\text{kg}_a$

Comments:

- When calculating supersaturated air an ideal mixing model (saturated humid air and water droplets (or ice crystals) homogeneously mixed) is applied

Result for Wrong Input Values:

v_ptW_HAP_SI = -1000

References:v(p, t, W) Herrmann et al. [1], [2]

Humidity Ratio from Partial Pressure of Steam $W = f(p, t, p_{H_2O})$ **Function Name:**

W_ptpH2O_HAP_SI

Fortran Program:

REAL*8 FUNCTION W_PTPH2O_HUAIRPROP(P,T,PH2O), REAL*8 P,T,PH2O

Input Values:

- p - Total pressure p in kPa
 t - Temperature t in °C
 p_{H_2O} - Partial pressure of water p_{H_2O} in kPa

Result:

W_ptpH2O_HAP_SI - Humidity ratio from temperature and partial pressure of water vapor in kg_w/kg_a

Range of Validity:

- Total pressure p : from 0.01 kPa to 10 000 kPa
 Temperature t : from -143.15°C to 350°C
 Partial pressure p_{H_2O} : from 0.01 kPa to 10 000 kPa

Comments:

- Iteration of humidity ratio W from $p_{H_2O} = f(p, t, W)$
- Result for supersaturated humid air is W_s

Result for Wrong Input Values:

W_ptpH2O_HAP_SI = -1000

References: $p_{H_2O}(p, t, W)$ Herrmann et al. [1], [2]

Humidity Ratio from Relative Humidity $W = f(p, t, \varphi)$

Function Name:

`W_ptphi_HAP_SI`

Fortran Program:

```
REAL*8 FUNCTION W_PTPHI_HUAIRPROP(P,T,PHI), REAL*8 P,T,PHI
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 φ - Relative humidity (decimal ratio)

Result:

`W_ptphi_HAP_SI` - Humidity ratio from temperature and relative humidity
in kg_w/kg_a

Range of Validity:

Temperature t : from -143.15°C to 350°C
Total pressure p : from 0.01 kPa to 10 000 kPa
Relative humidity φ : $0 \leq \varphi \leq 1$

Comments:

- Iteration of humidity ratio W from $\varphi = f(p, t, W)$

Result for Wrong Input Values:

`W_ptphi_HAP_SI = -1000`

References:

$\varphi(p, t, W)$ Herrmann et al. [1], [2]

Humidity Ratio from Dew-Point Temperature $W = f(p, t_d)$

Function Name:

W_ptd_HAP_SI

Fortran Program:

REAL*8 FUNCTION W_PTD_HUAIRPROP(P,TD), REAL*8 P,TD

Input Values:

p - Total pressure p in kPa
 t_d - Dew-point temperature t_d in °C

Result:

W_ptd_HAP_SI - Humidity ratio from temperature and dew-point temperature
in kg_w/kg_a

Range of Validity:

Dew point temperature t_d : from -143.15°C to 350°C
Total pressure p : from 0.01 kPa to 10 000 kPa

Comments:

- Iteration of humidity ratio W from $t_d = f(p, W)$

Result for Wrong Input Values:

W_ptd_HAP_SI = -1000

References:

$t_d(p, W)$ Herrmann et al. [1], [2]

Humidity Ratio from Wet-Bulb Temperature $W = f(p, t, t_{wb})$

Function Name:

W_pttwb_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION W_PTTWB_HUAIRPROP(P,T,TWB), REAL*8 P,T,TWB
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 t_{wb} - Wet-bulb temperature in °C

Result:

W_pttwb_HAP_SI - Humidity ratio from temperature and wet-bulb temperature
in kg_w/kg_a

Range of Validity:

Total pressure p : from 0.01 kPa to 10 000 kPa
Temperature t : from -143.15°C to 350°C
Wet-bulb temperature t_{wb} : from -143.15°C to 350°C

Comments:

- Iteration of humidity ratio W from $t_{wb} = f(p, t, W)$
- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

W_pttwb_HAP_SI = -1000

References:

$t_{wb}(p, t, W)$ Herrmann et al. [1], [2]

Saturation Humidity Ratio $W_s = f(p, t)$

Function Name:

Ws_pt_HAP_SI

Fortran Program:

REAL*8 FUNCTION WS_PT_HUAIRPROP(P,T), REAL*8 P,T

Input Values: p - Total pressure p in kPa t - Temperature t in °C**Result:**Ws_pt_HAP_SI - Saturation humidity ratio (mass fraction) in kg_w/kg_a **Range of Validity:**Total pressure p : from 0.01 kPa to 10 000 kPaTemperature t : from -143.15°C to 350°C**Comments:**

- Calculation of saturation humidity ratio W_s from $W_s = \frac{M_{\text{H}_2\text{O}}}{M_a} \frac{p_{\text{H}_2\text{O},s}}{(p - p_{\text{H}_2\text{O},s})}$

Result for Wrong Input Values:

Ws_pt_HAP_SI = -1000

References: $p_{\text{H}_2\text{O},s}$ Herrmann et al. [1], [2]

Mass Fraction of Dry Air $\xi_{\text{Air}} = f(W)$
Function Name:

XiAir_W_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION XIAIR_W_HUAIRPROP(W), REAL*8 W
```

Input Values:

W - Humidity ratio W in kg_w/kg_a

Result:

XiAir_W_HAP_SI - Mass fraction of (dry) air in humid air in kg_a/kg

Range of Validity:

Humidity ratio W : $0 \leq W \leq 10 \text{kg}_w/\text{kg}_a$

Comments:

- Mass fraction of (dry) air $\xi_{\text{Air}} = 1 - \xi_{\text{H}_2\text{O}} = 1 - \frac{W}{1 + W}$

Result for Wrong Input Values:

XiAir_W_HAP_SI = -1000

References:

$\xi_{\text{Air}}(W)$ Herrmann et al. [1], [2]

Mass Fraction of Water Vapor $\xi_{\text{H}_2\text{O}} = f(W)$
Function Name:

XiH2O_W_HAP_SI

Fortran Program:

REAL*8 FUNCTION XIH2O_W_HUAIRPROP(W), REAL*8 W

Input Values: W - Humidity ratio W in kg_w/kg_a **Result:**XiH2O_W_HAP_SI - Mass fraction of water vapor in humid air in kg_w/kg **Range of Validity:**Humidity ratio W : $0 \leq W \leq 10 \text{ kg}_w/\text{kg}_a$ **Comments:**- Mass fraction of water vapor $\xi_{\text{H}_2\text{O}} = \frac{W}{1+W}$ **Result for Wrong Input Values:**

XiH2O_W_HAP_SI = -1000

References: $\xi_{\text{H}_2\text{O}}(W)$ Herrmann et al. [1], [2]

Compression Factor $Z = f(p, t, W)$

Function Name:

Z_ptW_HAP_SI

Fortran Program:

```
REAL*8 FUNCTION Z_PTW_HUAIRPROP(P,T,W), REAL*8 P,T,W
```

Input Values:

p - Total pressure p in kPa
 t - Temperature t in °C
 W - Humidity ratio W in kg_w/kg_a

Result:

Z_ptW_HAP_SI - Compression factor (decimal ratio)

Range of Validity:

Total pressure p : from 0.01 kPa to 10 000 kPa
 Temperature t : from -143.15°C to 350°C
 Humidity ratio W : $0 \leq W \leq W_s$

Comments:

- Compression factor $Z = 1 + \frac{B_m}{\bar{v}} + \frac{C_m}{\bar{v}^2}$

$$\text{with } \bar{v} = \frac{M}{\rho} = \frac{Mv}{1+W}$$

and M is the molar mass of humid air

- Calculation for supersaturated humid air ($W > W_s$) is not possible

Result for Wrong Input Values:

Z_ptW_HAP_SI = -1000

References:

$B_m(t, W), C_m(t, W)$ Herrmann et al. [1], [2]

$\rho(p, t, W), v(p, t, W)$ Herrmann et al. [1], [2]

3.2 Functions for Steam and Water for Temperatures $t \geq 0^\circ\text{C}$

Specific Enthalpy of Liquid Water $h_{\text{liq}} = f(p, t)$
Function Name:

hliq_pt_97_SI

Fortran Program:

REAL*8 FUNCTION HLIQ_PT_97(P,T), REAL*8 P,T

Input Values:

p - Pressure p in kPa
 t - Temperature t in °C

Result:

hliq_pt_97_SI - Specific enthalpy of liquid water in kJ/kg

Range of Validity:

Pressure p : from $p_s(0^\circ\text{C}) = 0.6112$ kPa to 10000 kPa
 Temperature t : from 0°C to 350°C

Comments:

- Specific enthalpy of liquid water $h_{\text{liq}} = h^{97}(p, t)$ (Region 1)

Result for Wrong Input Values:

hliq_pt_97_SI = -1000

References:

$h^{97}(p, t)$ IAPWS-IF97 [7], [8]

Specific Enthalpy of Saturated Liquid Water $h_{\text{liq,s}} = f(t)$
Function Name:

hliqs_t_97_SI

Fortran Program:

REAL*8 FUNCTION HLIQS_T_97(T), REAL*8 T

Input Values: t - Temperature t in °C**Result:**

hliqs_t_97_SI - Specific enthalpy of saturated liquid water in kJ/kg

Range of Validity:Temperature t : from 0°C to 350°C**Comments:**- Specific enthalpy of liquid water $h_{\text{liq,s}} = h^{97}(p_s, t)$ (Region 1)with $p_s = p_s^{97}(t)$ **Result for Wrong Input Values:**

hliqs_t_97_SI = -1000

References: $h^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Specific Enthalpy of Saturated Water Vapor $h_{\text{vap},s} = f(t)$

Function Name:

hvaps_t_97_SI

Fortran Program:

```
REAL*8 FUNCTION HVAPS_T_97(T), REAL*8 T
```

Input Values:

t - Temperature t in °C

Result:

hvaps_t_97_SI - Specific enthalpy of saturated water vapor in kJ/kg

Range of Validity:

Temperature t : from 0°C to 350°C

Comments:

- Specific enthalpy of saturated water vapor $h_{\text{vap},s} = h^{97}(p_s, t)$ (Region 2)

with $p_s = p_s^{97}(t)$

Result for Wrong Input Values:

hvaps_t_97_SI = -1000

References:

$h^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Saturation Pressure of Water $p_s = f(t)$

Function Name:

ps_t_97_SI

Fortran Program:

```
REAL*8 FUNCTION PS_T_97(T), REAL*8 T
```

Input Values:

t - Temperature t in °C

Result:

ps_t_97_SI - Saturation pressure of water in kPa

Range of Validity:

Temperature t : from 0°C to 350°C

Comments:

- Saturation pressure of water $p_s = p_s^{97}(t)$ (Region 4)

Result for Wrong Input Values:

ps_t_97_SI -1000

References:

$p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Specific Entropy of Liquid Water $s_{\text{liq}} = f(p, t)$

Function Name:

sliq_pt_97_SI

Fortran Program:

```
REAL*8 FUNCTION SLIQ_PT_97(P,T), REAL*8 P,T
```

Input Values:

p - Pressure p in kPa
 t - Temperature t in °C

Result:

sliq_pt_97_SI - Specific entropy of liquid water in kJ/(kg K)

Range of Validity:

Pressure p : from $p_s(0^\circ\text{C}) = 0.6112$ kPa to 10000 kPa
 Temperature t : from 0°C to 350°C

Comments:

- Specific entropy of liquid water $s_{\text{liq}} = s^{97}(p, t)$ (Region 1)

Result for Wrong Input Values:

sliq_pt_97_SI = -1000

References:

$s^{97}(p, t)$ IAPWS-IF97 [7], [8]

Specific Entropy of Saturated Liquid Water $s_{\text{liq,s}} = f(t)$
Function Name:

sliqs_t_97_SI

Fortran Program:

REAL*8 FUNCTION SLIQS_T_97(T), REAL*8 T

Input Values: t - Temperature t in °C**Result:**

sliqs_t_97_SI - Specific entropy of saturated liquid water in kJ/(kg K)

Range of Validity:Temperature t : from 0°C to 350°C**Comments:**- Specific entropy of liquid water $s_{\text{liq,s}} = s^{97}(p_s, t)$ (Region 1)with $p_s = p_s^{97}(t)$ **Result for Wrong Input Values:**

sliqs_t_97_SI = -1000

References: $s^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Specific Entropy of Saturated Water Vapor $s_{\text{vap},s} = f(t)$

Function Name:

svaps_t_97_SI

Fortran Program:

REAL*8 FUNCTION SVAPS_T_97(T), REAL*8 T

Input Values: t - Temperature t in °C**Result:**

svaps_t_97_SI - Specific entropy of saturated water vapor in kJ/(kg K)

Range of Validity:Temperature t : from 0°C to 350°C**Comments:**

- Specific entropy of saturated water vapor $s_{\text{vap},s} = s^{97}(p_s, t)$ (Region 2)
 with $p_s = p_s^{97}(t)$

Result for Wrong Input Values:

svaps_t_97_SI = -1000

References: $s^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

Saturation Temperature of Water $t_s = f(p)$ **Function Name:**

ts_p_97_SI

Fortran Program:

REAL*8 FUNCTION TS_P_97(P), REAL*8 P

Input Values: p - Pressure p in kPa**Result:**

ts_p_97_SI - Saturation temperature of water in °C

Range of Validity:Pressure p : from 0.6112 kPa to 10 000 kPa**Comments:**- Saturation temperature of water $t_s = t_s^{97}(p)$ (Region 4)**Result for Wrong Input Values:**

ts_p_97_SI = -1000

References: $t_s^{97}(p)$ IAPWS-IF97 [7], [8]

Specific Volume of Liquid Water $v_{\text{liq}} = f(p, t)$

Function Name:

vliq_pt_97_SI

Fortran Program:

```
REAL*8 FUNCTION VLIQ_PT_97(P,T), REAL*8 P,T
```

Input Values:

p - Pressure p in kPa
 t - Temperature t in °C

Result:

vliq_pt_97_SI - Specific volume of liquid water in m³/kg

Range of Validity:

Pressure p : from $p_s(0^\circ\text{C}) = 0.6112$ kPa to 10 000 kPa
 Temperature t : from 0°C to 350°C

Comments:

- Specific volume of liquid water $v_{\text{liq}} = v^{97}(p, t)$ (Region 1)

Result for Wrong Input Values:

vliq_pt_97_SI = -1000

References:

$v^{97}(p, t)$ IAPWS-IF97 [7], [8]

Specific Volume of Saturated Liquid Water $v_{\text{liq,s}} = f(t)$
Function Name:

vliqs_t_97_SI

Fortran Program:

REAL*8 FUNCTION VLIQS_T_97(T), REAL*8 T

Input Values: t - Temperature t in °C**Result:**vliqs_t_97_SI - Specific volume of saturated liquid water in m^3/kg **Range of Validity:**Temperature t : from 0°C to 350°C**Comments:**- Specific volume of liquid water $v_{\text{liq,s}} = v^{97}(\rho_s, t)$ (Region 1)with $\rho_s = \rho_s^{97}(t)$ **Result for Wrong Input Values:**

vliqs_t_97_SI = -1000

References: $v^{97}(\rho, t), \rho_s^{97}(t)$ IAPWS-IF97 [7], [8]

Specific Volume of Saturated Water Vapor $v_{\text{vap},s} = f(t)$
Function Name:

vvaps_t_97_SI

Fortran Program:

```
REAL*8 FUNCTION  VVAPS_T_97(T), REAL*8 T
```

Input Values:

t - Temperature t in °C

Result:

vvaps_t_97_SI - Specific volume of saturated water vapor in m^3/kg

Range of Validity:

Temperature t : from 0°C to 350°C

Comments:

- Specific volume of saturated water vapor $v_{\text{vap},s} = v^{97}(p_s, t)$ (Region 2)

with $p_s = p_s^{97}(t)$

Result for Wrong Input Values:

vvaps_t_97_SI = -1000

References:

$v^{97}(p, t), p_s^{97}(t)$ IAPWS-IF97 [7], [8]

3.3 Functions for Steam and Ice for Temperatures $t \leq 0^\circ\text{C}$

Specific Enthalpy of Saturated Ice $h_{\text{ice,sub}} = f(t)$
Function Name:

hicesub_t_06_SI

Fortran Program:

```
REAL*8 FUNCTION HICESUB_T_06(T), REAL*8 T
```

Input Values:

t - Temperature t in °C

Result:

hicesub_t_06_SI - Specific enthalpy of saturated ice in kJ/kg

Range of Validity:

Temperature t : from -143.15°C to 0°C

Comments:

- Specific enthalpy of saturated ice $h_{\text{ice,sub}} = h^{06}(\rho_{\text{sub}}, t)$
 with $\rho_{\text{sub}} = \rho_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

hicesub_t_06_SI = -1000

References:

$h^{06}(\rho, t)$ IAPWS-06 [10]

$\rho_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Specific Enthalpy of Saturated Water Vapor $h_{\text{vap,sub}} = f(t)$
Function Name:

hvapsub_t_95_SI

Fortran Program:

```
REAL*8 FUNCTION HVAPSUB_T_95(T), REAL*8 T
```

Input Values:

t - Temperature t in °C

Result:

hvapsub_t_95_SI - Specific enthalpy of saturated water vapor in kJ/kg

Range of Validity:

Temperature t : from -143.15°C to 0°C

Comments:

- Specific enthalpy of saturated water vapor $h_{\text{vap,sub}} = h^{95}(p_{\text{sub}}, t)$

with $p_{\text{sub}} = p_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

hvapsub_t_95_SI = -1000

References:

$h^{95}(p, t)$ IAPWS-95 [5], [6]

$p_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Melting Pressure $p_{\text{mel}} = f(t)$
Function Name:

pmel_t_08_SI

Fortran Program:

```
REAL*8 FUNCTION PMEL_T_08 (T), REAL*8 T
```

Input Values:

t - Temperature t in °C

Result:

pmel_t_08_SI - Melting pressure of ice in kPa

Range of Validity:

Temperature t : from -21.985°C to 0°C

Result for Wrong Input Values:

pmel_t_08_SI = -1000

References:

$p_{\text{mel}}^{08}(t)$ IAPWS-08 [11]

Sublimation Pressure $p_{\text{sub}} = f(t)$

Function Name:

psub_t_08_SI

Fortran Program:

```
REAL*8 FUNCTION PSUB_T_08 (T), REAL*8 T
```

Input Values:

t - Temperature t in °C

Result:

psub_t_08_SI - Sublimation pressure of ice in kPa

Range of Validity:

Temperature t : from -143.15°C to 0°C

Result for Wrong Input Values:

psub_t_08_SI = -1000

References:

$p_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Specific Entropy of Saturated Ice $s_{\text{ice,sub}} = f(t)$

Function Name:

sicesub_t_06_SI

Fortran Program:

REAL*8 FUNCTION SICESUB_T_06(T), REAL*8 T

Input Values: t - Temperature t in °C**Result:**

sicesub_t_06_SI - Specific entropy of saturated ice in kJ/(kg K)

Range of Validity:Temperature t : from -143.15°C to 0°C**Comments:**

- Specific entropy of saturated ice $s_{\text{ice,sub}} = s^{06}(p_{\text{sub}}, t)$
 with $p_{\text{sub}} = p_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

sicesub_t_06_SI = -1000

References: $s^{06}(p, t)$ IAPWS-06 [10] $p_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Specific Entropy of Saturated Water Vapor $s_{\text{vap,sub}} = f(t)$
Function Name:

svapsub_t_95_SI

Fortran Program:

REAL*8 FUNCTION SVAPSUB_T_95(T), REAL*8 T

Input Values: t - Temperature t in °C**Result:**

svapsub_t_95_SI - Specific entropy of saturated water vapor in kJ/(kg K)

Range of Validity:Temperature t : from -143.15°C to 0°C**Comments:**- Specific entropy of saturated water vapor $s_{\text{vap,sub}} = s^{95}(p_{\text{sub}}, t)$ with $p_{\text{sub}} = p_{\text{sub}}^{08}(t)$ **Result for Wrong Input Values:**

svapsub_t_95_SI = -1000

References: $s^{95}(p, t)$ IAPWS-95 [7], [8] $p_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Melting Temperature $t_{\text{mel}} = f(p)$

Function Name:

tmel_p_08_SI

Fortran Program:

```
REAL*8 FUNCTION TMEL_P_08(P), REAL*8 P
```

Input Values:

p - Pressure p in kPa

Result:

tmel_p_08_SI - Melting temperature of ice in °C

Range of Validity:

Pressure p : from $p_s(0^\circ\text{C}) = 0.6112$ kPa to 10 000 kPa

Result for Wrong Input Values:

tmel_p_08_SI = -1000

References:

$t_{\text{mel}}^{08}(p)$ IAPWS-08 [11]

Sublimation Temperature $t_{\text{sub}} = f(p)$
Function Name:

tsub_p_08_SI

Fortran Program:

REAL*8 FUNCTION TSUB_P_08(P), REAL*8 P

Input Values: p - Pressure p in kPa**Result:**

tsub_p_08_SI - Sublimation temperature of ice in °C

Range of Validity:Pressure p : from $p_{\text{subl}}(-143.15^\circ\text{C}) = 1.2002 \times 10^{-11}$ kPa to $p_{\text{subl}}(0^\circ\text{C}) = 0.6112$ kPa**Result for Wrong Input Values:**

tsub_p_08_SI = -1000

References: $t_{\text{sub}}^{08}(p)$ IAPWS-08 [11]

Specific Volume of Saturated Ice $v_{\text{ice,sub}} = f(t)$
Function Name:

vicesub_t_06_SI

Fortran Program:

REAL*8 FUNCTION VICESUB_T_06(T), REAL*8 T

Input Values: t - Temperature t in °C**Result:**vicesub_t_06_SI - Specific volume of saturated ice in m^3/kg **Range of Validity:**Temperature t : from -143.15°C to 0°C **Comments:**- Specific volume of saturated ice $v_{\text{ice,sub}} = v^{06}(\rho_{\text{sub}}, t)$ with $\rho_{\text{sub}} = \rho_{\text{sub}}^{08}(t)$ **Result for Wrong Input Values:**

vicesub_t_06_SI = -1000

References: $v^{06}(\rho, t)$ IAPWS-06 [10] $\rho_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

Specific Volume of Saturated Water Vapor $v_{\text{vap,sub}} = f(t)$
Function Name:

vvapsub_t_95_SI

Fortran Program:

```
REAL*8 FUNCTION  VVAPSUB_T_95(T), REAL*8 T
```

Input Values:

t - Temperature t in °C

Result:

vvapsub_t_95_SI - Specific volume of saturated water vapor in m³/kg

Range of Validity:

Temperature t : from -143.15°C to 0°C

Comments:

- Specific volume of saturated water vapor $v_{\text{vap,sub}} = v^{95}(\rho_{\text{sub}}, t)$

with $\rho_{\text{sub}} = \rho_{\text{sub}}^{08}(t)$

Result for Wrong Input Values:

vvapsub_t_95_SI = -1000

References:

$v^{95}(\rho, t)$ IAPWS-95 [7], [8]

$\rho_{\text{sub}}^{08}(t)$ IAPWS-08 [11]

4. Property Libraries for Calculating Heat Cycles, Boilers, Turbines and Refrigerators

Water and Steam

Library LibIF97

- Industrial Formulation IAPWS-IF97 (Revision 2007)
- Supplementary Standards IAPWS-IF97-S01, -S03rev, -S04, and -S05
- IAPWS Revised Advisory Note No. 3 on Thermodynamic Derivatives (2008)

Library LibIF97_META

- Industrial Formulation IAPWS-IF97 (Revision 2007) for metastable steam

Humid Combustion Gas Mixtures

Library LibHuGas

- Model: Ideal mixture of the real fluids:
 CO₂ - Span, Wagner H₂O - IAPWS-95
 O₂ - Schmidt, Wagner N₂ - Span et al.
 Ar - Tegeler et al.
 and of the ideal gases:
 SO₂, CO, Ne
 (Scientific Formulation of Bückner et al.)
- Consideration of:
- Dissociation from VDI 4670
 - Poynting effect

Humid Air

Library LibHuAir

- Model: Ideal mixture of the real fluids:
- Dry air from Lemmon et al.
 - Steam, water and ice from IAPWS-IF97 and IAPWS-06
- Consideration of:
- Condensation and freezing of steam
 - Dissociation from VDI 4670
 - Poynting effect from ASHRAE RP-1485

Extremely Fast Property Calculations

- Spline-Based Table
 Look-up Method (SBTL)
- Library LibSBTL_IF97**
Library LibSBTL_95
Library LibSBTL_HuAir
- For steam, water, humid air, carbon dioxide and other fluids and mixtures according IAPWS Guideline 2015 for Computational Fluid Dynamics (CFD), real-time and non-stationary simulations

Carbon Dioxide Including Dry Ice

Library LibCO2

Formulation of Span and Wagner (1996)

Seawater

Library LibSeaWa

IAPWS Industrial Formulation 2013

Ice

Library LibICE

Ice from IAPWS-06, Melting and sublimation pressures from IAPWS-08, Water from IAPWS-IF97, Steam from IAPWS-95 and -IF97

Ideal Gas Mixtures

Library LibIdGasMix

Model: Ideal mixture of the ideal gases:

Ar	NO	He	Propylene
Ne	H ₂ O	F ₂	Propane
N ₂	SO ₂	NH ₃	Iso-Butane
O ₂	H ₂	Methane	n-Butane
CO	H ₂ S	Ethane	Benzene
CO ₂	OH	Ethylene	Methanol
Air			

Consideration of:

- Dissociation from the VDI Guideline 4670

Library LibIDGAS

Model: Ideal gas mixture from VDI Guideline 4670

Consideration of:

- Dissociation from the VDI Guideline 4670

Humid Air

Library ASHRAE LibHuAirProp

Model: Virial equation from ASHRAE Report RP-1485 for real mixture of the real fluids:
 - Dry air
 - Steam

Consideration of:

- Enhancement of the partial saturation pressure of water vapor at elevated total pressures

www.ashrae.org/bookstore

Dry Air Including Liquid Air

Library LibRealAir

Formulation of Lemmon et al. (2000)

Refrigerants

Ammonia

Library LibNH3

Formulation of Tillner-Roth et al. (1993)

R134a

Library LibR134a

Formulation of Tillner-Roth and Baehr (1994)

Iso-Butane

Library LibButane_Iso

Formulation of Bückner and Wagner (2006)

n-Butane

Library LibButane_n

Formulation of Bückner and Wagner (2006)

Mixtures for Absorption Processes

Ammonia/Water Mixtures

Library LibAmWa

IAPWS Guideline 2001 of Tillner-Roth and Friend (1998)

Helmholtz energy equation for the mixing term (also useable for calculating the Kalina Cycle)

Water/Lithium Bromide Mixtures

Library LibWaLi

Formulation of Kim and Infante Ferreira (2004)

Gibbs energy equation for the mixing term

Liquid Coolants

Liquid Secondary Refrigerants

Library LibSecRef

Liquid solutions of water with

C ₂ H ₆ O ₂	Ethylene glycol
C ₃ H ₈ O ₂	Propylene glycol
C ₂ H ₅ OH	Ethanol
CH ₃ OH	Methanol
C ₃ H ₈ O ₃	Glycerol
K ₂ CO ₃	Potassium carbonate
CaCl ₂	Calcium chloride
MgCl ₂	Magnesium chloride
NaCl	Sodium chloride
C ₂ H ₃ KO ₂	Potassium acetate
CHKO ₂	Potassium formate
LiCl	Lithium chloride
NH ₃	Ammonia

Formulation of the International Institute of Refrigeration (IIR 2010)

Ethanol**Library LibC2H5OH**

Formulation of
Schroeder et al. (2014)

Methanol**Library LibCH3OH**

Formulation of
de Reuck and Craven (1993)

Propane**Library LibPropane**

Formulation of
Lemmon et al. (2009)

Siloxanes as ORC Working Fluids

Octamethylcyclotetrasiloxane $C_8H_{24}O_4Si_4$ **Library LibD4**

Decamethylcyclopentasiloxane $C_{10}H_{30}O_5Si_5$ **Library LibD5**

Tetradecamethylhexasiloxane $C_{14}H_{42}O_6Si_6$ **Library LibMD4M**

Hexamethyldisiloxane $C_6H_{18}OSi_2$ **Library LibMM**

Formulation of Colonna et al. (2006)

Dodecamethylcyclohexasiloxane $C_{12}H_{36}O_6Si_6$ **Library LibD6**

Decamethyltetrasiloxane $C_{10}H_{30}O_3Si_4$ **Library LibMD2M**

Dodecamethylpentasiloxane $C_{12}H_{36}O_4Si_5$ **Library LibMD3M**

Octamethyltrisiloxane $C_8H_{24}O_2Si_3$ **Library LibMDM**

Formulation of Colonna et al. (2008)

Nitrogen and Oxygen**Libraries
LibN2 and LibO2**

Formulations of Span et al. (2000)
and Schmidt and Wagner (1985)

Hydrogen**Library LibH2**

Formulation of
Leachman et al. (2009)

Helium**Library LibHe**

Formulation of
Arp et al. (1998)

Hydrocarbons

Decane $C_{10}H_{22}$ **Library LibC10H22**

Isopentane C_5H_{12} **Library LibC5H12_Iso**

Neopentane C_5H_{12} **Library LibC5H12_Neo**

Isohexane C_6H_{14} **Library LibC6H14**

Toluene C_7H_8 **Library LibC7H8**

Formulation of Lemmon and Span (2006)

Further Fluids

Carbon monoxide **CO** **Library LibCO**

Carbonyl sulfide **COS** **Library LibCOS**

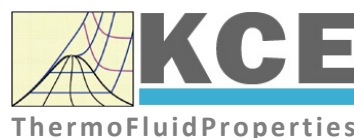
Hydrogen sulfide **H₂S** **Library LibH2S**

Nitrous oxide **N₂O** **Library LibN2O**

Sulfur dioxide **SO₂** **Library LibSO2**

Acetone C_3H_6O **Library LibC3H6O**

Formulation of Lemmon and Span (2006)

**For more information please contact:**

KCE-ThermoFluidProperties UG
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The following thermodynamic and transport properties can be calculated^a:**Thermodynamic Properties**

- Vapor pressure p_s
- Saturation temperature T_s
- Density ρ
- Specific volume v
- Enthalpy h
- Internal energy u
- Entropy s
- Exergy e
- Isobaric heat capacity c_p
- Isochoric heat capacity c_v
- Isentropic exponent κ
- Speed of sound w
- Surface tension σ

Transport Properties

- Dynamic viscosity η
- Kinematic viscosity ν
- Thermal conductivity λ
- Prandtl number Pr
- Thermal diffusivity a

Backward Functions

- $T, v, s(p, h)$
- $T, v, h(p, s)$
- $p, T, v(h, s)$
- $p, T(v, h)$
- $p, T(v, u)$

Thermodynamic Derivatives

- Partial derivatives used in process modeling can be calculated.

^a Not all of these property functions are available in all property libraries.

Property Software for Calculating Heat Cycles, Boilers, Turbines and Refrigerators

Add-In FluidEXL^{Graphics} for Excel[®]

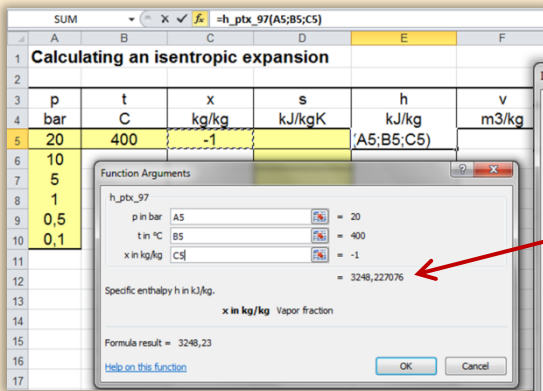
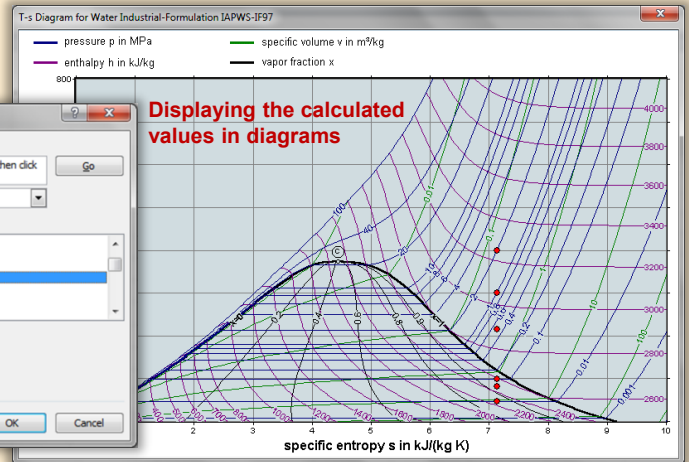


Table with 6 columns: bar, C, kg/kg, kJ/kgK, kJ/kg, m³/kg. Row 5: 20, 400, -1, (A5:B5:C5).
Function Arguments dialog for h_ptx_97:
p in bar: A5 = 20
t in °C: B5 = 400
x in kg/kg: C5 = -1
Specific enthalpy h in kJ/kg: = 3248,227076
Formula result = 3248,23

Choosing a property library and a function

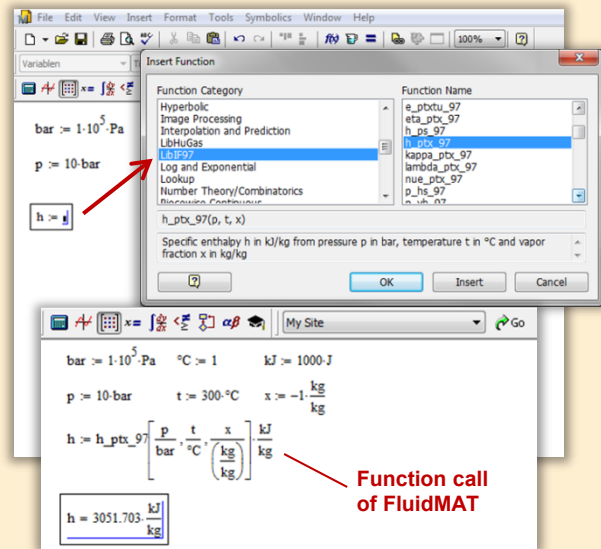


Displaying the calculated values in diagrams

Menu for the input of given property values

Add-On FluidMAT for Mathcad[®]
Add-On FluidPRIME for Mathcad Prime[®]

The property libraries can be used in Mathcad[®] and Mathcad Prime[®].

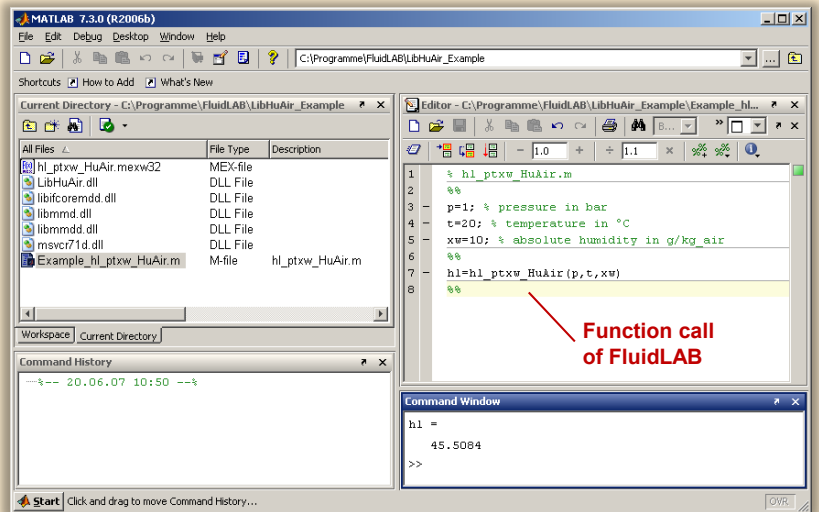


Mathcad interface showing the function call: $h = h_{ptx_97} \left[\frac{p}{\text{bar}}, \frac{t}{\text{°C}}, \frac{x}{\left(\frac{\text{kg}}{\text{kg}}\right)} \right] \frac{\text{kJ}}{\text{kg}}$.
Result: $h = 3051.703 \frac{\text{kJ}}{\text{kg}}$

Function call of FluidMAT

Add-On FluidLAB for MATLAB[®] and SIMULINK[®]

Using the Add-In FluidLAB the property functions can be called in MATLAB[®] and SIMULINK[®].

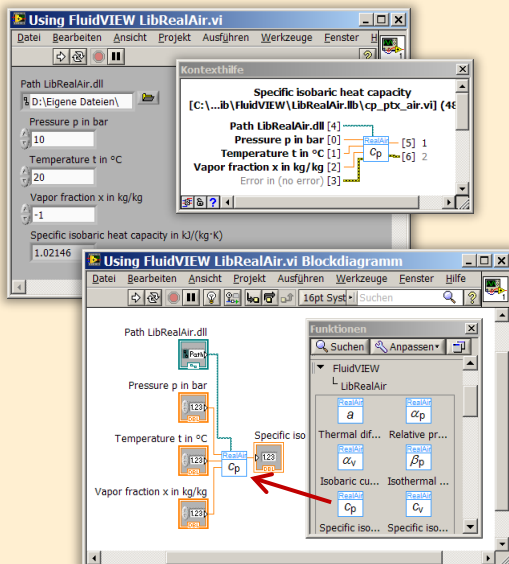


MATLAB 7.3.0 (R2006b) interface. Script file content:
`hl = hl_ptxw_HuAir(m, p, t, x)`
Command Window output:
`hl = 45.5084`

Function call of FluidLAB

Add-On FluidVIEW for LabVIEW[™]

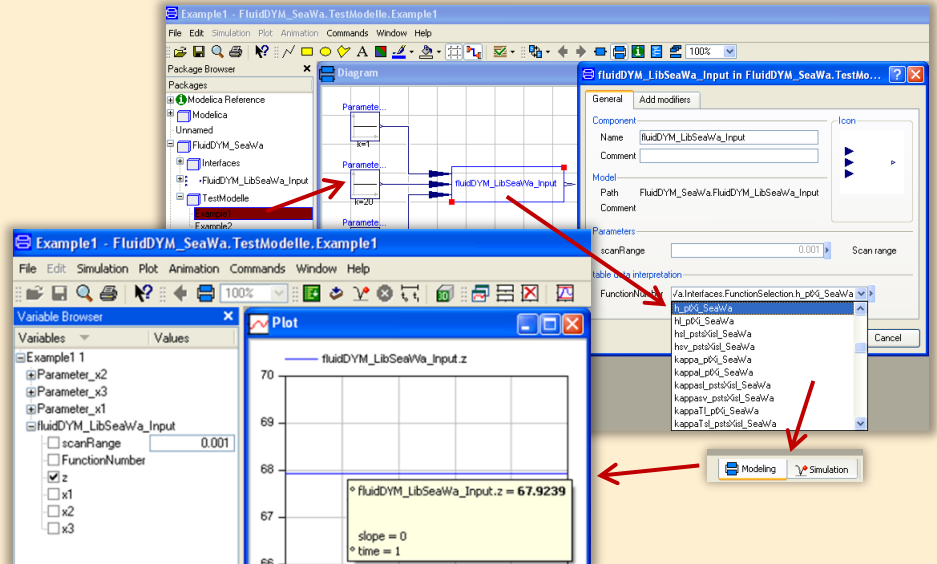
The property functions can be calculated in LabVIEW[™].



LabVIEW interface showing a block diagram with FluidVIEW property function blocks. A 'Specific iso' block is highlighted with input values for pressure, temperature, and vapor fraction.

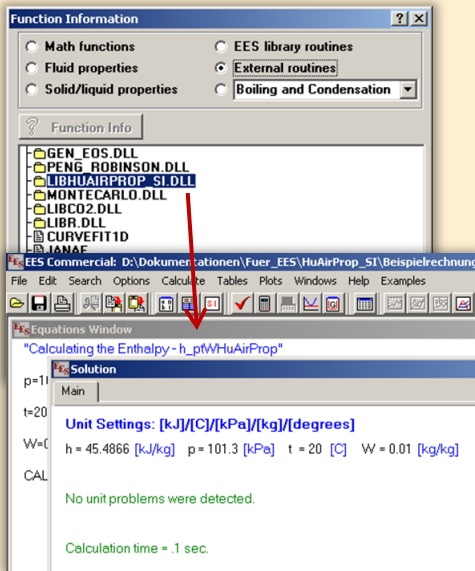
Add-On FluidDYM for DYMOLA[®] (Modelica) and SimulationX[®]

The property functions can be called in DYMOLA[®] and SimulationX[®].



SimulationX interface showing a block diagram with FluidDYM function blocks. Variable browser shows 'fluidDYM_LibSeaWa_Input.z' with value 67.9239. Plot shows the function call result over time.

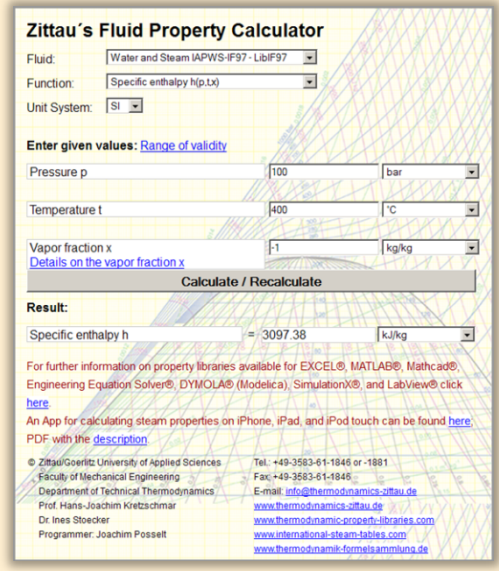
Add-On FluidEES for Engineering Equation Solver®



App International Steam Tables for iPhone, iPad, iPod touch, Android Smartphones and Tablets



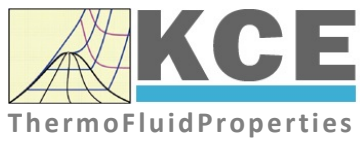
Online Property Calculator at www.thermofluidprop.com



Property Software for Pocket Calculators

<p>FluidCasio</p> <p>fx 9750 G II CFX 9850 fx-GG20 CFX 9860 G Graph 85 ALGEBRA FX 2.0</p>				<p>FluidHP</p> <p>HP 48 HP 49</p>		<p>FluidTI</p> <p>TI Nspire CX CAS TI 83 TI Nspire CAS TI 84 TI 89 TI Voyage 200 TI 92</p>	
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For more information please contact:



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 Fax: +49-3222-1095810

The following thermodynamic and transport properties^a can be calculated in Excel®, MATLAB®, Mathcad®, Engineering Equation Solver® (EES), DYMOLA® (Modelica), SimulationX® and LabVIEW™:

- | | | | |
|--|---|---|---|
| <p>Thermodynamic Properties</p> <ul style="list-style-type: none"> • Vapor pressure p_s • Saturation temperature T_s • Density ρ • Specific volume v • Enthalpy h • Internal energy u • Entropy s • Exergy e • Isobaric heat capacity c_p • Isochoric heat capacity c_v • Isentropic exponent κ • Speed of sound w • Surface tension σ | <p>Transport Properties</p> <ul style="list-style-type: none"> • Dynamic viscosity η • Kinematic viscosity ν • Thermal conductivity λ • Prandtl number Pr • Thermal diffusivity a | <p>Backward Functions</p> <ul style="list-style-type: none"> • $T, v, s(p, h)$ • $T, v, h(p, s)$ • $p, T, v(h, s)$ • $p, T(v, h)$ • $p, T(v, u)$ | <p>Thermodynamic Derivatives</p> <ul style="list-style-type: none"> • Partial derivatives used in process modeling can be calculated. |
|--|---|---|---|

^a Not all of these property functions are available in all property libraries.

5 References

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6 Satisfied Customers

Period from 2018 to 2022

The following companies and institutions use the property libraries:

- FluidEXL *Graphics* for Excel® incl. VBA
- FluidLAB for MATLAB® and Simulink
- FluidMAT for Mathcad®
- FluidPRIME for Mathcad Prime®
- FluidEES for Engineering Equation Solver® EES
- FluidDYM for Dymola® (Modelica) and SimulationX®
- FluidVIEW for LabVIEW™
- FluidPYT for Python
- FluidJAVA for Java
- DLLs for Windows Applications
- Shared Objects for Linux
- Shared Objects for macOS.

2022

ASTG, Graz, Austria	12/2022
Wandschneider + Gutjahr, Hamburg	
RWE Supply & Trading, Essen	11/2022
Stadtwerke Rosenheim	
CEA, Saclay, France	10/2022
RWE Supply & Trading, Essen	
SEEC Saudi Energy Efficiency Center, Riyadh, Saudi Arabia	
MAN, Copenhagen, Denmark	
Hermeler & Partner Consulting Engineers, Sassenberg	09/2022
Envi Con, Nürnberg	
Drill Cool Systems, Bakersfield CA, USA	
RWE Supply & Trading, Essen	
Maerz Ofenbau, Zürich, Switzerland	
Saale Energie, Schkopau	
ERGO, Dresden	
Mainova, Frankfurt/Main	
Bundeswehr, Koblenz	08/2022
RWE Supply & Trading, Essen	
Grenzebach Corporation, Newnan GE, USA	
AGRANA, Gmuend, Austria	07/2022
MIBRAG, Zeitz	
Hochschule Niederrhein, Krefeld	
ULT, Löbau	06/2022
LEAG, Cottbus	

VPC Group, Vetschau	
Wärme, Hamburg	
ILK, Dresden	
Stricker IB, Küsnacht a. Rigi, Switzerland	
LEAG, Cottbus	05/2022
RWE Supply & Trading, Essen	
IGT Tomalla, Kreuztal	
B+T Engineering, Dübendorf, Switzerland	
Stricker IB, Küsnacht a. Rigi, Switzerland	
Vogelsang & Benning, Bochum	04/2022
Frischli, Rehburg-Loccum	
BPS Consulting, Sprengel	03/2022
HS Hannover, Maschinenbau & BioVT	
M+M Turbinentechnik, Bad Salzungen	
Uni. Strathclyde, Glasgow, UK	02/2022
Delta Energy Group, Jiaozhou City, Qingdao, China	
Wetzel IB, Guben	
Wijbenga, PC Geldermalsen, The Netherlands	
Voith Paper, Heidenheim	
HS Zittau/Görlitz, Maschinenwesen	01/2022
Thermische Abfallbehandlung, Lauterbach	
Webb Institute, Glen Cove NY, USA	
TU Berlin, Umweltverfahrenstechnik	
SachsenEnergie, Dresden	
Doosan, Chang-won-si, Gyeongsangnam-do, South Korea	
KW3, LH Veenendaal, The Netherlands	
Université du Luxembourg, Esch-sur-Alzette	
Enseleit IB, Mansfeld	
Caliqua/Equans, Zürich, Switzerland	
Rudnick & Enners, Alpenrod	

2021

Wenisch IB, Vetschau	12/2021
PPCHEM, Hinwil, Switzerland	
KW3, The Netherlands	
BASF Ludwigshafen	
Air-Consult, Jena	
Sjerp & Jongeneel, RB Zoetermeer, The Netherlands	11/2021
Maerz Ofenbau, Zürich, Switzerland	
RWE Supply & Trading, Essen	
Hahn IB, Dresden	10/2021
Therm, South Africa	
RWE Supply & Trading, Essen	
TH Nürnberg, Verfahrenstechnik	09/2021
RWE Supply & Trading, Essen	
Enseleit IB, Mansfeld	

SachsenEnergie, Dresden	
BSH Hausgeräte, Berlin	
Norsk Energi, Oslo, Norway	08/2021
AKM Industrieanlagen, Haltern	
Drill Cool Systems, Bakersfield CA, USA	
Siemens Energy Global, Erlangen	07/2021
Wulff & Umag, Husum	
Planungsbüro Waidhas, Chemnitz	
Burkhardt Energie Technik, Mühlhausen	
Lücke IB, Paderborn	06/2021
TU Dresden, Energieverfahrenstechnik	
Wärme, Hamburg	
AL-KO Therm, Kötz	
PCK Raffinerie, Schwedt	
Vogelsang & Benning, Bochum	05/2021
MTU, München	
VPC Group, Vetschau	
AVG, Köln	04/2021
TH Ulm, Institut für Fahrzeugtechnik	
Marty IB, Oberwil, Switzerland	
HypTec, Lebring, Austria	
Lopez IB, Getxo, Bizkaia, Spain	03/2021
GM Remediation Systems, Leoben, Austria	
Jager Kältetechnik, Osnabrück	
T&M Automation, GR Leidschendam, The Netherlands	
RWE Supply & Trading, Essen	
Stadtwerke Leipzig	
Beuth Hochschule für Technik, Berlin	
Beleth IB, Woeth	02/2021
ZTL, Thal, Austria	
ETABO Bochum	
RWE Supply & Trading, Essen	
Onyx Germany, Berlin	
TU Dresden, Kältetechnik	
GOHL-KTK, Durmersheim	
Therm Development, South Africa	
thermofin, Heinsdorfergrund	
RWE Supply & Trading, Essen	01/2021
STEAG, Essen	
ETA Energieberatung, Pfaffenhofen	
Enex Power, Kirchseeon	

2020

Drill Cool, Bakersfield CA, USA	12/2020
Manders, The Netherlands	
RWE Supply & Trading, Essen	

NEOWAT Lodz, Poland	
University of Duisburg-Essen, Duisburg	11/2020
Stellenbosch University, South Africa	
University De France-COMTe, France	
RWE, Essen	
STEAG, Herne	
Isenmann Ingenieurbüro	
University of Stuttgart, ITLR, Stuttgart	
Norsk Energi, Oslo, Norway	
TGM Kanis, Nürnberg	
Stadtwerke Neuburg	10/2020
Smurfit Kappa, Roermond, The Netherlands	
RWE, Essen	
Hochschule Zittau/Görlitz, Wirtschaftsingenieurwesen	
Stadtwerke, Neuburg	
ILK, Dresden	
ATESTEO, Alsdorf	
Hochschule Zittau/Görlitz, Maschinenwesen	
TH Nürnberg, Verfahrenstechnik	
Drill Cool, Bakersfield CA,USA	09/2020
RWE, Essen	
2Meyers Ingenieurbüro, Nürnberg	
FELUWA, Mürlenbach	
Stadtwerke Neuburg	
Caverion, Wien, Austria	
GMVA Niederrhein, Oberhausen	
INWAT Lodz, Poland	
Troche Ingenieurbüro, Hayingen	08/2020
CEA Saclay, France	
VPC, Vetschau	07/2020
FSK System-Kälte-Klima, Dortmund	
Exergie Etudes, Sarl, Switzerland	
AWG Wuppertal	
STEAG Energy Services, Zwingenberg	
Hochschule Braunschweig	06/2020
DBI, Leipzig	
GOHL-KTK, Dumersheim	
TU Dresden, Energieverfahrenstechnik	
BASF SE, ESI/EE, Ludwigshafen	
Wärme Hamburg	
Ruchti Ingenieurbüro, Uster, Switzerland	
IWB, Basel, Switzerland	
Midiplan, Bietingen-Bissingen	05/2020
Knieschke, Ingenieurbüro	
RWE, Essen	
Leser, Hamburg	

AGRANA, Gmünd, Austria	
EWT Wassertechnik, Celle	
Hochschule Darmstadt	04/2020
MTU München CCP	
HAW Hamburg	03/2020
Hanon, Novi Jicin, Czech Republic	
TU Dresden, Kältetechnik	
MAN, Copenhagen, Denmark	
EnerTech, Radebeul	02/2020
LEAG, Cottbus	
B+B Engineering Magdeburg	
Hochschule Offenburg	
WIB, Dennheritz	01/2020
Universität Duisburg-Essen, Strömungsmaschinen	
Kältetechnik Dresden-Bremen	
TH Ingolstadt	
Vattenfall AB, Jokkmokk, Sweden	
Fraunhofer UMSICHT	

2019

PEU Leipzig, Rötha	12/2019
MB-Holding, Vestenbergsgreuth	
RWE, Essen	
Georg-Büchner-Hochschule, Darmstadt	11/2019
EEB ENERKO, Aldenhoven	
Robert Benoufa Energietechnik, Wiesloch	
Kehrein & Kubanek Klimatechnik, Moers	10/2019
Hanon Systems Autopal Services, Hluk, Czech Republic	
CEA Saclay, Gif Sur Yvette cedex, France	
Saudi Energy Efficiency Center SEEC, Riyadh, Saudi Arabia	
VPC, Vetschau	09/2019
jGanser PM + Engineering, Forchheim	
Endress+Hauser Flowtec AG, Reinach, Switzerland	
Ruchtli IB, Uster, Switzerland	
ZWILAG Zwischenlager Würenlingen, Switzerland	08/2019
Hochschule Zittau/Görlitz, Faculty Maschinenwesen	
Stadtwerke Neubrandenburg	
Physikalisch Technische Bundesanstalt PTB, Braunschweig	
GMVA Oberhausen	07/2019
Endress+Hauser Flowtec AG, Reinach, Switzerland	
WARNICA, Waterloo, Canada	
MIBRAG, Zeitz	06/2019
Pöyry, Zürich, Switzerland	
RWTH Aachen, Institut für Strahlantriebe und Turbomaschinen	
Midiplan, Bietigheim-Bissingen	
GKS Schweinfurt	

Comparex Leipzig for LEAG, Berlin	06/2018
Münstermann, Telgte	05/2018
TH Nürnberg, Verfahrenstechnik	
Universität Madrid, Madrid, Spanien	
HS Zittau/Görlitz, Wirtschaftsingenieurwesen	
HS Niederrhein, Krefeld	
Wilhelm-Büchner HS, Pfungstadt	03/2018
GRS, Köln	
WIB, Dennheritz	
RONAL AG, Härklingen, Schweiz	02/2018
Ingenieurbüro Leipert, Riegelsberg	
AIXPROCESS, Aachen	
KRONES, Neutraubling	
Doosan Lentjes, Ratingen	01/2018