

Errata to
HVAC2 Toolkit: Algorithms and Subroutines for Secondary HVAC System Energy Calculations
(1993)

January 27, 2020

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HX.DRYWETCOIL

```
50      CONTINUE

C2*** Boundary temperature not converged after maximum specified iterations.
C2*** Print error message, set return error flag

      WRITE(*,1001) itmax
1001  FORMAT(/1X,'*** ERROR IN SUBROUTINE PARTWET ***'/
&        1X,'   Liquid temperature not converged at boundary ',
&        'after ',I2,' iterations'/)
      ErrStat = 1

C1*** Estimate new value for fraction wet surface area

60      CONTINUE

C1*** If surface is dry, calculate dry coil performance and return

      IF(FWet .LE. 0.0 .AND. tSurfBnd .GE. TDewPt) THEN

          dryUA = aTot/(1./UIntTot+1./DryUExtTot)
          CALL DRYCOIL(Prop,MLiq,TLiqEnt,MAir,TAirEnt,WAirEnt,
&                    dryUA,configHX,
&                    TLiqLvg,TAirLvg,WAirLvg,QTot,
&                    ErrStat)

          QSen = QTot
          FWet = 0.
          GO TO 999
      ENDIF

      error = tSurfBnd - TDewPt

      FWet = XITERATE(FWet,error,X1,F1,X2,F2,iter,icvg)

C1*** If converged, leave iteration loop

      IF (icvg .EQ. 1) GO TO 110

C2*** Surface temperature not converged. Repeat calculations with new
C2*** estimate of fraction wet surface area.

      IF(FWet .GT. 1) FWet = 1.
      IF(FWet .LT. 0) FWet = 0.

100     CONTINUE

C2*** Surface temperature not converged after maximum specified iterations.
C2*** Print error message, set return error flag

      WRITE(*,1002) itmax
1002  FORMAT(/1X,'*** ERROR IN SUBROUTINE PARTWET ***'/
&        1X,'   Wet/Dry boundary surface temperature not '
&        'converged after ',I2,' iterations'/)
      ErrStat = 1

110     CONTINUE

C1*** Calculate sum of total and sensible heat transfer from dry
C1*** and wet parts.

      QTot = qDry+qTotWet
      QSen = qDry+qSenWet

999     RETURN
      END
```

4.1.6 WCOILOUT: Outlet Conditions for Wet Coil

GENERAL DESCRIPTION

This subroutine calculates the leaving air temperature, the leaving air humidity ratio, and the sensible cooling capacity for a wet or partially wet coil given the total capacity, entering air conditions, and air-side overall heat transfer coefficient.

MATHEMATICAL DESCRIPTION

The leaving air dry bulb temperature is calculated using an effectiveness method. The condensate temperature on the coil is unknown but assumed to be constant. Therefore, the condensate represents a fluid stream with infinite thermal capacity rate, and the following effectiveness relationship applies.

$$(4-19)$$

Using this relationship together with the known air enthalpy at the entrance to the wet coil and leaving air enthalpy, the saturated enthalpy at the condensate temperature for the calculated effectiveness can be determined.

$$h_{\text{sat,cond}} = h_{\text{a,exit}} - \frac{h_{\text{a,exit}} - h_{\text{a,entr}}}{e} \quad (4-20)$$

If the coil surface is part wet, the air conditions at the wet/dry boundary are used as entering conditions. The temperature of the condensate (surface) is determined from the saturated enthalpy using standard psychrometric relationships. Given condensate temperature, t_c , the leaving dry bulb temperature is calculated by the following.

$$(4-21)$$

The sensible cooling capacity can now be determined using a simple energy balance.

$$q_{\text{sens}} = (\dot{m} c_p)_a (t_{\text{a,entr}} - t_{\text{a,exit}}) \quad (4-22)$$

REFERENCES

ARI. 1972. "Standard for Forced Circulation Air-Cooling and Air Heating Coils," ARI Standard 410-72, Air-Conditioning and Refrigeration Institute, Washington, D.C.

HX.WCOILOUT

NOMENCLATURE

		Description	Units	Minimum	Maximum
Input Variables					
\dot{m}_a	MAir	Dry air mass flow rate	(kg/s)	0	BIG
$t_{a,ent}$	TAirEnt	Entering air dry bulb temperature	(C)	-100	200
$w_{a,ent}$	WAirEnt	Entering air humidity ratio	(-)	0	$w_{sat}(t_{a,i})$
$h_{a,ent}$	HAirEnt	Entering air enthalpy	(J/kg)	0	$h(t_{a,i}, w_{a,i})$
$h_{a,lvg}$	HAirLvg	Leaving air enthalpy	(J/kg)	-BIG	$h_{a,i}$
	UAExt	Heat transfer coefficient for external surface	(W/C)		
Output Variables					
	TAirLvg	Leaving air dry bulb temperature	(C)		
	WAirLvg	Leaving air humidity ratio	(-)		
	QSen	Sensible heat transfer rate	(W)		
Properties					
$c_{p,a}$	CpAir	Specific heat of air	(J/kg C)	SMALL	BIG
$c_{p,v}$	CpVap	Specific heat of water vapor	(J/kg C)	SMALL	BIG
Selected Internal Variables					
Ntu	ntu	Number of heat transfer units	(-)		
ϵ	effectiveness	Heat exchanger effectiveness	(-)		
$h_{sat,cond}$	hSatCond	Saturated air enthalpy at condensate temp	(J/kg)		

ALGORITHM

- Determine the effectiveness of heat exchange between the air and the condensate, noting that the condensate temperature is constant ($C_{min}/C_{max} = 0$).
- Calculate coil surface enthalpy using the effectiveness relationships.
- Calculate condensate temperature from saturated enthalpy by psychrometric.
- Calculate leaving air conditions and sensible capacity using condensate temperature.

SOURCE CODE

```

      SUBROUTINE WCOILOUT (Prop,MAir,TAirEnt,WAirEnt,HAirEnt,HAirLvg,
      & UAExt,TAirLvg,WAirLvg,QSen,ErrStat)
C*****
C* Copyright ASHRAE. Toolkit for HVAC System Energy Calculations
C*****
C* SUBROUTINE:          WCOILOUT
C*
C* LANGUAGE:           FORTRAN 77
C*
C* PURPOSE:            Calculate the leaving air temperature,
C*                    the leaving air humidity ratio and the
C*                    sensible cooling capacity of wet cooling
C*                    coil.
C*****
C* INPUT VARIABLES
C* MAir                Dry air mass flow rate                (kg/s)
C* TAirEnt             Entering air dry bulb temperature      (C)
C* WAirEnt             Entering air humidity ratio            (-)
C* HAirEnt             Entering air enthalpy                  (J/kg)
C* HAirLvg             Leaving air enthalpy                   (J/kg)
C* UAExt               Heat transfer coefficient for external surface (W/C)
C*
C* OUTPUT VARIABLES
C* TAirLvg             Leaving air dry bulb temperature      (C)
C* WAirLvg             Leaving air humidity ratio            (-)
C* Qsen                Sensible heat transfer rate           (W)
C* ErrStat             Error status indicator, 0 = ok, 1 = error (-)
C*
C* PROPERTIES
C* Patm                Atmospheric pressure                  (-)
C* CpAir                Specific heat of air                  (J/kg C)
C* CpVap                Specific heat of water vapor          (J/kg C)
C*****
C MAJOR RESTRICTIONS:  Assumes condensate at uniform temperature.
C
C DEVELOPER:           Shauna Gabel
C                     Michael J. Brandemuehl, PhD, PE
C                     University of Colorado at Boulder
C
C DATE:                January 1, 1992
C
C INCLUDE FILES:       prop.inc
C SUBROUTINES CALLED:  None
C FUNCTIONS CALLED:    TAIRSAT
C                     DRYBULB
C                     HUMTH
C                     DEWPOINT
C
C REVISION HISTORY:    None
C
C REFERENCE:           Elmahdy, A.H. and Mitalas, G.P. 1977.
C                     "A Simple Model for Cooling and
C                     Dehumidifying Coils for Use In Calculating
C                     Energy Requirements for Buildings,"
C                     ASHRAE Transactions, Vol.83 Part 2,
C                     pp. 103-117.
C*****
C INTERNAL VARIABLES:
C capAir                Air capacity rate                    (W/C)
C ntu                   Number of heat transfer units        (-)
C effectiveness          Heat exchanger effectiveness        (-)
C hCondSat              Saturated air enthalpy at temperature of
C                      condensate                            (J/kg)
C tempCond              Temperature of condensate             (C)
C*****
      INCLUDE: 'prop.inc'

      INTEGER ErrStat
      REAL ntu,MAir
      DATA small/1.E-9/

      ErrStat = 0

```

EVAPHUM

4.9 EVAPHUM: Direct Evaporative Humidifier/Cooler

GENERAL DESCRIPTION

This subroutine calculates the leaving air temperature and humidity ratio using an adiabatic saturation effectiveness model. The model represents an air stream passing over a pan of water or through a saturated porous medium, adiabatically increasing the humidity and decreasing the temperature of the air. The temperature of the water is assumed to be equal to the leaving temperature of the humidified air.



MATHEMATICAL DESCRIPTION

Figure 4-10: Schematic of direct evaporative cooler.

The leaving humidity ratio is calculated using a saturation effectiveness method. The model performs effectiveness calculations using heat exchanger effectiveness-Ntu relationships assuming that the effective capacity rate of the evaporation source is infinite. The effectiveness-Ntu calculations are performed in the utility routine HEATEX. Using these relationships, the leaving humidity ratio is calculated by the following.

$$w_{a,hg} = w_{a,ent} + (w_{a,hg,ent} - w_{a,ent}) \epsilon_{sat} \quad (6-3)$$

The outlet saturated humidity ratio, $w_{a,hg,ent}$, is evaluated at the inlet wet bulb temperature. The saturation effectiveness can be determined from the following relationship as described in the documentation for HEATEX.

$$\begin{aligned} \epsilon_{sat} &= 1 - e^{-N} \\ N &= \frac{UA_{sat}}{C_{sat}} \end{aligned} \quad (6-4)$$

For this model, the saturation capacity rate, C_{sat} , is the mass flow rate of the air and the overall saturation transfer coefficient, UA_{sat} , is a measure of the size of the evaporative humidifier. The value of UA_{sat} is determined from a single point of performance data. Given the flow rate and entering air conditions and the corresponding saturation effectiveness at some operating conditions, the overall coefficient can be determined as described above using the UAHX routine.

REFERENCE

Clark, D.R.. 1985. HVACSIM+ Building Systems and Equipment Simulation Program: Reference Manual. NBSIR 84-2996, U.S. Department of Commerce, Washington, D.C.

Threlkeld, J.L. 1970. Thermal Environmental Engineering, 2nd Edition, Englewood Cliffs: Prentice-Hall, Inc.

NOMENCLATURE

		Description	Units	Minimum	Maximum
Variables					
\dot{m}_a	MAir	Dry air mass flow rate	(kg/s)	0	BIG
$t_{a,ent}$	TAirEnt	Entering air temperature	(C)	-100	200
$w_{a,ent}$	WAirEnt	Entering air humidity ratio	(-)	0	$w_{sat}(t_{a,ent})$
Output Variables					
$t_{a,lvg}$	TAirLvg	Leaving air temperature	(C)		
$w_{a,lvg}$	WAirLvg	Leaving air humidity ratio	(-)		
Parameters					
$\epsilon_{evap,rat}$	EffEvapRat	Humidity effectiveness at rating	(-)	0	1
$\dot{m}_{evap,rat}$	MEvapRat	Humidifier dry air mass flow rate at rating	(kg/s)	0	BIG
$t_{evap,rat}$	TEvapRat	Humidifier air dry bulb temperature at rating	(C)	-100	200
$w_{evap,rat}$	WEvapRat	Humidifier air humidity ratio at rating	(-)	0	$w_{sat}(t_{a,ent})$
Properties					
P_{atm}	Patm	Atmospheric pressure	(Pa)		
$c_{p,a}$	CpAir	Specific heat of air	(J/kg C)		
$c_{p,v}$	CpVap	Specific heat of water vapor	(J/kg C)		
Selected Internal Variables					
C_{sat}	capAir	Capacity rate of air stream	(kg/s)		
UA_{sat}	P(UAEvap)	Overall transfer coefficient	(kg/s)		
ϵ_{sat}		Saturation effectiveness	(-)		
N		Number of transfer coefficients	(-)		

ALGORITHM

- Calculate overall transfer coefficient from rating data
- Calculate psychrometric properties of the entering air
- Calculate saturated leaving air humidity ratio at the entering wet bulb temperature
- Calculate the leaving air humidity ratio from effectiveness-Ntu model with entering and saturated conditions
- Calculate the leaving air temperature from leaving humidity ratio and entering enthalpy

DUALDUCT

```
      READ(LUR5,*) MZDes(i),QZsen,QZlat,TZSetPt

C2*** Calculate the required zone entering air temperature to satisfy
C2*** zone sensible load

      tZSAir(i) = TZSetPt-QZsen/(Prop(CpAir)*MZDes(i))

C2*** Sum the design air mass flow rate and the total latent load
C2*** for all zones

      mZDesTot = MZDes(i)+mZDesTot
      qZlatTot = QZlat+qZlatTot

C2*** Zone return air calculation

      tAirRet = TZSetPt
      TotTAirRet = tAirRet+TotTAirRet

      WRITE(LUW,1012) i,MZDes(i),QZsen,QZlat,TZSetPt,tZSAir(i)

200    CONTINUE

C2*** Zone calculation end

C1*** Averaged return air temperature

      tAirRet = TotTAirRet/zNum

C1*** Iterate on humidity ratio

C2*** Initial guess at cooling coil leaving air humidity ratio,
C2*** relating to air leaving conditions of 55 DB and 90% RH, and
C2*** initial guess at the heating coil leaving air humidity ratio
C2*** equivalent to the entering air humidity ratio

      wCCAirlvg = 0.0077
      wHCAirlvg = wAirAmb

      DO 300 iter=1,itmax

      oldw = wCCAirlvg
      mHotTot = 0.0
      mColdTot = 0.0

C1*** Begin zone loop for hot and cold air flow calculations

      DO 400 i = 1,zNum

C2*** Determine the hot and cold air mass flow rates for zone

          CALL MIXIAIR (Prop,MZDes(i),tZSAir(i),TColdDes,wCCAirlvg,
          &              THotDes,wHCAirlvg,mCold,mHot,wZEnt,ErrStat)

C2*** Sum the cold and hot air mass flow rate totals

          mHotTot = mHot+mHotTot
          mColdTot = mCold+mColdTot

400    CONTINUE

C2*** End zone loop for hot and cold air flow calculations

C1*** Return air humidity ratio calculation

      wAirRet = wZent+qZlatTot/(Prop(Hfg)*mZDesTot)

C1*** Calculate the mixed air temperature and humidity ratio using
C1*** an economizer option

      tPHSetPt = TColdDes-1.

      CALL ECON (Prop,tAirRet,wAirRet,TAirAmb,wAirAmb,mZDesTot,
      &          wAmbMin,tPHSetPt,TAirAmb,EconClose,EconMode,
      &          tAirMix,wAirMix,mAirRet,mAirAmb,ErrStat)

C1*** Determine if preheat is necessary and calculate the coil load
```


C1*** if required, otherwise set the cooling coil entering air
 C1*** temperature and humidity ratio equal to the mixed air temperature

```

    IF (tAirMix .LT. tPHSetPt) THEN
      CALL COILINV (HCDET,Prop,PPHCoil,tHCLiqEnt,mZDesTot,
&                tAirMix,wAirMix,TPHSetPt,wAirMix,mPHLiq,
&                tLiqPHLvg,qPHtot,qPHsen,pHFwet,Errstat)
    ELSE
      qPHtot = 0.0
      qPHsen = 0.0
      mPHLiq = 0.0
      tPHSetPt = tAirMix
    ENDIF
  
```

C1*** Calculate the supply fan power and fan leaving air temperature

```

    CALL FANSIM (PROP,PSFan,mZDesTot,tPHSetPt,wAirMix,tAirMix,
&              wAirMix,sFanPow,Errstat)
  
```

C1*** Calculate the heating coil load

```

    IF (tAirMix .LT. tHotDes) THEN
      CALL COILINV (HCDET,Prop,PHCoil,tHCLiqEnt,mHotTot,tAirMix,
&                wAirMix,tHotDes,wHCAirLvg,mHCLiq,tLiqHCLvg,
&                qHCtot,qHCsen,hCFwet,Errstat)
    ELSE
      mHCLiq = 0.0
      qHCtot = 0.0
      qHCsen = 0.0
    ENDIF
  
```

C1*** Calculate the cooling coil load and leaving air humidity ratio

```

    IF (tAirMix .GT. TColdDes) THEN
      CALL COILINV (CCDET,Prop,PCCoil,tCCLiqEnt,mColdTot,tAirMix,
&                wAirMix,TColdDes,wCCAirLvg,mCCLiq,tLiqCCLvg,
&                qCCtot,qCCsen,cCFwet,Errstat)
    ELSE
      mCCLiq = 0.0
      qCCtot = 0.0
      qCCsen = 0.0
    ENDIF

    error = oldw-wCCAirLvg
    wCCAirLvg = XITERATE(wCCAirLvg,error,X1,F1,X2,F2,iter,icvg)
  
```

C1*** If converged, leave loop
 IF (icvg .EQ. 1) GO TO 500

300 CONTINUE
 C2*** End humidity ratio loop

C1*** If not converged after itmax iterations, return error code

```

    WRITE(*,1010) itmax
1010 FORMAT(/1X,'*** ERROR IN PROGRAM DUAL ***'/
&          1X,' The humidity ratio has not converged after,'12,
&          iterations'/)
    ErrStat = 1
  
```

500 CONTINUE

C *** Write hourly results

```

    WRITE(LUW,1015) qCCtot,qCCsen,qHCsen,qPHsen,sFanPow
  
```

C1*** Sum the coil loads and fan power

```

    TotSFanPow = sFanPow+TotSFanPow
    TotQPHsen = qPHsen+TotQPHsen
    TotQHCsen = qHCsen+TotQHCsen
    QtotCCTot = qCCtot+QtotCCTot
    QsenCCTot = qCCsen+QsenCCTot
  
```