

STANDARD

**ANSI/ASHRAE/IES Addendum bo to
ANSI/ASHRAE/IES Standard 90.1-2022**

Energy Standard for Sites and Buildings Except Low-Rise Residential Buildings

Approved by the ASHRAE Standard Committee on April 24, 2023; by the Illuminating Engineering Society on May 8, 2023; and by the American National Standards Institute on May 16, 2023.

This addendum was approved by a Standing Standard Project Committee (SSPC) for which the Standards Committee has established a documented program for regular publication of addenda or revisions, including procedures for timely, documented, consensus action on requests for change to any part of the standard. Instructions for how to submit a change can be found on the ASHRAE® website (<https://www.ashrae.org/continuous-maintenance>).

The latest edition of an ASHRAE Standard may be purchased from the ASHRAE website (www.ashrae.org) or from ASHRAE Customer Service, 180 Technology Parkway, Peachtree Corners, GA 30092. E-mail: orders@ashrae.org. Fax: 678-539-2129. Telephone: 404-636-8400 (worldwide), or toll free 1-800-527-4723 (for orders in US and Canada). For reprint permission, go to www.ashrae.org/permissions.

© 2023 ASHRAE

ISSN 1041-2336



ASHRAE Standard Project Committee 90.1

Cognizant TC: 7.6 Systems Energy Utilization

SPLS Liaison: Jennifer Isenbeck • ASHRAE Staff Liaisons: Emily Toto • IES Liaison: Mark Lien

Donald Brundage*, <i>Chair</i>	Melissa Goren*	Vladimir Kochkin*	Robert Ross*
Thomas Culp*, <i>Co-Vice Chair</i>	Mark Graham	Michael Lane*	Armin Rudd
Richard Lord, <i>Co-Vice Chair*</i>	Aaron Gunzner	Toby Lau	Marty Salzberg*
Rahul Athalye	David Handwork*	Chonghui Liu	Christopher Schaffner
William Babbington	Rick Heiden	Emily Lorenz	Greg Schluterman
John Bade*	David Herron*	Christopher Mathis*	Amy Schmidt
Sean Beilman*	Armin Hauer	Merle McBride*	Leonard Sciarra*
Kyle Bergeron	Gary Heikkinen	James McClendon*	Kelly Seeger*
Jeffrey Boldt	Mark Heizer	Benjamin Meyer*	Wayne Stoppelmoor*
Paula Cino*	Scott Hintz*	James C. Moore	Matthew Swenka
Glen Clapper	Emily Hoffman	Frank Morrison*	Christian Taber*
Ernest Conrad*	Mike Houston*	Michael Myer	Steven Taylor*
Shannon Corcoran*	Jonathan Humble*	Frank Myers*	Douglas Tucker
Jay Crandell*	Michael Ivanovich	Michael Patterson*	Jason Vandever
Brandon Damas*	Harold Jepsen	Timothy Peglow*	Martha VanGeem*
Julie Donovan*	Chad Johnson	Tien Peng	Michael Waite*
Craig Drumheller*	Greg Johnson*	Christopher Perry	McHenry Wallace*
James Earley	Duane Jonlin*	Laura Petrillo-Groh*	Jerry White*
D. Andrew Fouss	Michael Jouaneh	Michael Rosenberg*	Jeremiah Williams*
Phillip Gentry	Maria Karpman*	Steven Rosenstock*	Amber Wood
Jason Glazer*	Andrew Klein	Loren Ross	

* Denotes members of voting status when the document was approved for publication

ASHRAE STANDARDS COMMITTEE 2022–2023

Susanna S. Hanson, <i>Chair</i>	Phillip A. Johnson	Lawrence C. Markel	Christopher J. Seeton
Jonathan Humble, <i>Vice-Chair</i>	Srinivas Katipamula	Patrick C. Marks	Christian R. Taber
William P. Bahnfleth	Gerald J. Kettler	Margaret M. Mathison	Paolo M. Tronville
Thomas E. Cappellin	Jay A. Kohler	Kathleen Owen	William F. Walter
Douglas D. Fick	Cesar L. Lim	Gwelen Paliaga	Steven C. Sill, <i>BOD ExO</i>
Patricia Graef	Paul A. Lindahl, Jr.	Karl L. Peterman	Sarah E. Maston, <i>CO</i>
Jaap Hogeling	James D. Lutz	Justin M. Prosser	
Jennifer A. Isenbeck	Julie Majurin	David Robin	

Connor Barbaree, *Senior Manager of Standards*

SPECIAL NOTE

This American National Standard (ANS) is a national voluntary consensus Standard developed under the auspices of ASHRAE. *Consensus* is defined by the American National Standards Institute (ANSI), of which ASHRAE is a member and which has approved this Standard as an ANS, as “substantial agreement reached by directly and materially affected interest categories. This signifies the concurrence of more than a simple majority, but not necessarily unanimity. Consensus requires that all views and objections be considered, and that an effort be made toward their resolution.” Compliance with this Standard is voluntary until and unless a legal jurisdiction makes compliance mandatory through legislation.

ASHRAE obtains consensus through participation of its national and international members, associated societies, and public review.

ASHRAE Standards are prepared by a Project Committee appointed specifically for the purpose of writing the Standard. The Project Committee Chair and Vice-Chair must be members of ASHRAE; while other committee members may or may not be ASHRAE members, all must be technically qualified in the subject area of the Standard. Every effort is made to balance the concerned interests on all Project Committees.

The Senior Manager of Standards of ASHRAE should be contacted for

- interpretation of the contents of this Standard,
- participation in the next review of the Standard,
- offering constructive criticism for improving the Standard, or
- permission to reprint portions of the Standard.

DISCLAIMER

ASHRAE uses its best efforts to promulgate Standards and Guidelines for the benefit of the public in light of available information and accepted industry practices. However, ASHRAE does not guarantee, certify, or assure the safety or performance of any products, components, or systems tested, installed, or operated in accordance with ASHRAE's Standards or Guidelines or that any tests conducted under its Standards or Guidelines will be nonhazardous or free from risk.

ASHRAE INDUSTRIAL ADVERTISING POLICY ON STANDARDS

ASHRAE Standards and Guidelines are established to assist industry and the public by offering a uniform method of testing for rating purposes, by suggesting safe practices in designing and installing equipment, by providing proper definitions of this equipment, and by providing other information that may serve to guide the industry. The creation of ASHRAE Standards and Guidelines is determined by the need for them, and conformance to them is completely voluntary.

In referring to this Standard or Guideline and in marking of equipment and in advertising, no claim shall be made, either stated or implied, that the product has been approved by ASHRAE.

(This foreword is not part of this standard. It is merely informative and does not contain requirements necessary for conformance to the standard. It has not been processed according to the ANSI requirements for a standard and may contain material that has not been subject to public review or a consensus process. Unresolved objections on informative material are not offered the right to appeal at ASHRAE or ANSI.)

FOREWORD

Addendum bo updates fan power limits in Section 6.5.3.1 based on updates to California Title 24-2022, and in consideration of the cost-effectiveness requirements used for Standard 90.1. The increase in stringency ranges is, on average, about 10%, though the amount varies by fan system type.

A spreadsheet tool¹ allows users to check compliance for each of three system types: single fan, supply/return fan, or complex fan systems. In each worksheet, the user can enter fan system parameters and see how the resulting power allowance for the proposal compares against the two existing options in ASHRAE/IES Standard 90.1-2022 (i.e., the motor nameplate method and the brake horsepower method). (Note: Users only need to modify the orange input cells.)

Addendum bo solves many problems with the current requirements:

- The present method limits fan shaft power and does not consider the actual electric input power. Further, it does not cover the efficiency of the fan transmission, motor, or variable-speed controller. Addendum bo provides requirements for fan system electrical input power.*
- The existing requirements are based on pressure losses for a large air handler (e.g., 3.5 in. of water for duct losses for a multizone system). Addendum bo provides requirements for small, medium, and large systems.*
- Fan power limits do not apply to alterations. Addendum bo adds scope alterations with additional fan power allowances to account for existing duct systems and adapter curbs. Reviewers should note that direct replacement of existing fans is exempted from this requirement.*
- New fan power allowances have been created for components that have become more common, including hot-gas reheat coils, water economizer coils, and series energy recovery.*
- Addendum bo recognizes the efficiency of using direct-drive instead of v-belt transmissions.*
- Any supply fan that does not move air through a source of heating or cooling. For example, large energy recovery ventilators are out of scope. The scope would now cover these products.*
- The existing language excludes fans that do not serve conditioned spaces. Addendum bo includes all fans serving interior spaces.*
- The existing language includes only fan systems where the fan nameplate horsepower totals more than 5 hp (3.7 kW). This excludes all fan systems up to approximately 5000 cfm (2400 L/s). The power threshold is reduced to 1 kW input power.*

There are five steps to calculating the fan power budget:

- a. Determine the type of fan system employed.*
- b. Determine the total fan power allowances in W/cfm (W/L/s) from Tables 6.5.3.1-1 and 6.5.3.1-2.*
- c. Multiply the fan power allowances by the airflow in standard (not actual) cfm (L/s)*
- d. Divide by 1000 to arrive at the allow input power in kW.*
- e. Apply the altitude correction factor for sites 3000 ft (900 m) or higher.*

The electrical input power for each fan or fan array in the system can be calculated in one of four ways:

- The information is supplied by the equipment manufacturer. This will be the typical scenario.*
- If the motor nameplate horsepower (kilowatts) is known, there is a table that provides default input power for systems with and without variable-speed drives.*
- If the motor nameplate electrical input power is provided, that value can be used.*
- If only the shaft input power is known, the electrical input power can be calculated using one of the methods in AMCA 208, Fan Energy Index. This would be a last resort and rarely needed.*

The input electrical power of all the fans in the fan system is summed and must be less than the fan power budget.

Cost Effectiveness

The Addendum bo values reduce the allowed fan system electrical input power by about 10% on average; the amount varies by system. A large multizone VAV system will see a reduction of about 13% if it includes

1. Download at <http://sspc901.ashraepcs.org/documents.php>.

MERV 13 filters. On the other hand, with the new credit for single-zone VAV systems that are configured to turn down to 50% of airflow, there is no increase in stringency at all.

There are many ways to improve a system to achieve the goal. Though the improvements here are based on the cost difference between a belt-drive centrifugal fan and a direct-drive plenum fan, there are many options to reduce pressure drop in the fan system that will yield the same results for less money. In fact, the California Title 24 cost effectiveness was based entirely on improving the design of the duct system while leaving the current minimum-efficiency air handler systems unchanged. Some of the options for improving fan system performance include

- reducing duct pressure drop through the selection of high-performance fittings,
- using angle filters in place of flat filters,
- locating equipment so that duct runs, and in particular vertical shafts, are straight, and
- careful consideration of design and the placement of the first turn in the duct system after leaving the air handler (this is often the highest pressure drop in the system).

However, for the purpose of this exercise, the cost of a belt-driven centrifugal fan with a variable-frequency drive was compared to a direct-drive plenum fan. The reduction in transmission losses alone make up for most of the required improvement in electrical input power. The two systems were run in the prototype buildings used by ASHRAE/IES Standard 90.1 in all climate zones. The majority of fans in the prototype buildings that are large enough to meet the threshold of 1 kW of input power in the proposal are variable-speed fans. Manufacture cost data were used to compare the cost per design cfm (L/s) of the two different fans at two different sizes:

- 3000 cfm (1400 L/s)—\$0.346 per cfm (\$0.163 L/s)
- 10,000 cfm (4700 L/s)—\$0.192 per cfm (\$0.091 L/s)

The following tables show the annual energy cost savings for various buildings. (Note: Only I-P units are used for generating the tables, because these are intended only for cost justification purposes.) The savings vary by climate, with warmer and wetter climates generally showing higher savings. The annual savings were multiplied by 12, which is the ASHRAE scalar limit for equipment with a 15-year lifespan. In nearly all cases, the cost per cfm of an improved fan is less than the scalar limit.

- Primary school—These typically have fans that are about 3000 cfm or a little more. In all cases, the savings are greater than the \$0.346 additional cost.

	Elec Energy Savings (kWh)	Gas Energy Savings (Therm)	Elec Energy Cost Savings (\$)	Gas Energy Cost Savings (\$)	Total Energy Cost Savings (\$)	Annual Savings X12	Modeled Airflow	\$/cfm
Albuquerque	13085	-84	1438	-67	1371	\$16,450	25169.5	\$0.65
Atlanta	12935	-7	1422	-5	1416	\$16,994	25169.5	\$0.68
Buffalo	11531	-51	1267	-41	1226	\$14,717	25169.5	\$0.58
Denver	12004	-118	1319	-95	1224	\$14,694	25169.5	\$0.58
Dubai	18103	0	1990	0	1990	\$23,875	25169.5	\$0.95
ElPaso	13822	-50	1519	-40	1479	\$17,744	25169.5	\$0.70
Fairbanks	14078	-157	1547	-126	1422	\$17,059	25169.5	\$0.68
GreatFalls	11509	-40	1265	-32	1232	\$14,790	25169.5	\$0.59
HoChiMinh	14873	0	1635	0	1635	\$19,615	25169.5	\$0.78
InternationalFalls	12749	-95	1401	-76	1325	\$15,904	25169.5	\$0.63
Miami	15460	0	1699	0	1699	\$20,384	25169.5	\$0.81
NewDelhi	16277	1	1789	1	1790	\$21,476	25169.5	\$0.85
NewYork	11932	-12	1311	-10	1302	\$15,622	25169.5	\$0.62
PortAngeles	10436	-1	1147	-1	1146	\$13,756	25169.5	\$0.55
Rochester	12563	-72	1381	-58	1323	\$15,872	25169.5	\$0.63
SanDiego	11373	-10	1250	-8	1242	\$14,903	25169.5	\$0.59
Seattle	11632	-139	1278	-111	1167	\$14,004	25169.5	\$0.56
Tampa	16769	-1	1843	-1	1842	\$22,108	25169.5	\$0.88
Tucson	12771	0	1404	0	1404	\$16,847	25169.5	\$0.67

- *Large hotel—These typically use large VAV fans. Again, in all cases, the additional cost of \$0.192 per cfm is much less than the projected savings.*

	Elec Energy Savings (kWh)	Gas Energy Savings (Therm)	Elec Energy Cost Savings (\$)	Gas Energy Cost Savings (\$)	Total Energy Cost Savings (\$)	Annual Savings X12	Modeled Airflow	\$/cfm
Albuquerque	24756	-20	2721	-16	2704	\$32,451	40110.4	\$0.81
Atlanta	20992	-24	2307	-19	2288	\$27,453	40110.4	\$0.68
Buffalo	19504	-60	2144	-49	2095	\$25,140	40110.4	\$0.63
Denver	24984	-45	2746	-36	2710	\$32,520	40110.4	\$0.81
Dubai	24856	-3	2732	-2	2729	\$32,752	40110.4	\$0.82
ElPaso	23902	-12	2627	-10	2617	\$31,407	40110.4	\$0.78
Fairbanks	16880	-72	1855	-58	1797	\$21,565	40110.4	\$0.54
GreatFalls	21103	-55	2319	-44	2275	\$27,300	40110.4	\$0.68
HoChiMinh	26707	-10	2935	-8	2927	\$35,128	40110.4	\$0.88
Honolulu	22710	-3	2496	-3	2493	\$29,918	40110.4	\$0.75
InternationalFalls	18937	-73	2081	-59	2022	\$24,267	40110.4	\$0.61
NewDelhi	24433	-8	2685	-7	2679	\$32,143	40110.4	\$0.80
NewYork	20083	-38	2207	-31	2177	\$26,118	40110.4	\$0.65
PortAngeles	19082	-24	2097	-19	2078	\$24,937	40110.4	\$0.62
Rochester	19824	-84	2179	-67	2112	\$25,338	40110.4	\$0.63
SanDiego	19085	-16	2097	-13	2084	\$25,013	40110.4	\$0.62
Seattle	19438	-27	2136	-22	2115	\$25,375	40110.4	\$0.63
Tampa	23725	-9	2607	-7	2600	\$31,201	40110.4	\$0.78
Tucson	23380	-11	2569	-9	2560	\$30,726	40110.4	\$0.77

- *Standalone retail—These prototypes use a mix of small and large fans. However, the 12-year savings are much higher than the per cfm cost of both sizes.*

	Elec Energy Savings (kWh)	Gas Energy Savings (Therm)	Elec Energy Cost Savings (\$)	Gas Energy Cost Savings (\$)	Total Energy Cost Savings (\$)	Annual Savings X12	Modeled Airflow	\$/cfm
Albuquerque	7589	-85	834	-68	766	\$9,195	23371.2	\$0.39
Atlanta	4501	-43	495	-35	460	\$5,521	23371.2	\$0.24
Buffalo	6972	-152	766	-122	645	\$7,736	23371.2	\$0.33
Denver	7759	-136	853	-109	744	\$8,927	23371.2	\$0.38
Dubai	10695	0	1175	0	1175	\$14,103	23371.2	\$0.60
ElPaso	10139	-66	1114	-53	1061	\$12,736	23371.2	\$0.54
Fairbanks	7159	-186	787	-149	638	\$7,653	23371.2	\$0.33
GreatFalls	7475	-171	822	-137	684	\$8,210	23371.2	\$0.35
HoChiMinh	10356	0	1138	0	1138	\$13,657	23371.2	\$0.58
InternationalFalls	6591	-140	724	-113	612	\$7,341	23371.2	\$0.31
Miami	9071	-1	997	-1	996	\$11,956	23371.2	\$0.51
NewDelhi	9863	-15	1084	-12	1072	\$12,863	23371.2	\$0.55
NewYork	6897	-121	758	-97	661	\$7,927	23371.2	\$0.34
PortAngeles	6750	-133	742	-106	635	\$7,625	23371.2	\$0.33
Rochester	7617	-179	837	-144	693	\$8,320	23371.2	\$0.36
SanDiego	6986	-11	768	-9	759	\$9,109	23371.2	\$0.39
Seattle	6975	-114	767	-92	675	\$8,100	23371.2	\$0.35
Tampa	7270	-12	799	-10	789	\$9,472	23371.2	\$0.41
Tucson	7817	-10	859	-8	851	\$10,216	23371.2	\$0.44

- *Large office—These prototypes use large VAV fans. In this case, the additional cost of \$0.192 per cfm meets the scalar for most climate zones. It does not meet the scalar for Climate Zone 8.*

	Elec Energy Savings	Gas Energy Savings	Total Energy Savings	Elec Energy Cost Savings	Gas Energy Cost Savings	Total Energy Cost Savings	Elec Energy Cost Savings	Gas Energy Cost Savings	Total Energy Cost Savings	Annual Savings X12	Modeled Airflow	\$/cfm
Albuquerque	222.89	-9.75	213.14	61963	-92	6810	-74	6736	\$80,828	255854.8	\$0.32	
Atlanta	172.59	-0.7	171.89	47980	-7	5273	-5	5268	\$63,212	255854.8	\$0.25	
Buffalo	152.66	-1.6	151.06	42439	-15	4664	-12	4652	\$55,823	255854.8	\$0.22	
Denver	200.94	-15.33	185.61	55861	-145	6139	-117	6023	\$72,271	255854.8	\$0.28	
Dubai	224.07	-0.08	223.99	62291	-1	6846	-1	6845	\$82,143	255854.8	\$0.32	
ElPaso	231.17	-3.94	227.23	64265	-37	7063	-30	7033	\$84,394	255854.8	\$0.33	
Fairbanks	52.95	-4.04	48.91	14720	-38	1618	-31	1587	\$19,044	255854.8	\$0.07	
GreatFalls	148.99	-7.86	141.13	41419	-75	4552	-60	4492	\$53,906	255854.8	\$0.21	
HoChiMinh	352.43	-0.45	351.98	97976	-4	10768	-3	10764	\$129,169	255854.8	\$0.50	
InternationalFalls	189.47	-1.72	187.75	52673	-16	5789	-13	5776	\$69,308	255854.8	\$0.27	
Miami	334.69	-0.31	334.38	93044	-3	10226	-2	10223	\$122,678	255854.8	\$0.48	
NewDelhi	215.16	-1.05	214.11	59814	-10	6574	-8	6566	\$78,788	255854.8	\$0.31	
NewYork	226.87	-0.49	226.38	63070	-5	6931	-4	6928	\$83,132	255854.8	\$0.32	
PortAngeles	191.2	-16.32	174.88	53154	-155	5842	-124	5717	\$68,610	255854.8	\$0.27	
Rochester	102.91	-0.29	102.62	28609	-3	3144	-2	3142	\$37,703	255854.8	\$0.15	
SanDiego	158.62	-1.12	157.5	44096	-11	4846	-9	4838	\$58,052	255854.8	\$0.23	
Seattle	240.28	-13.24	227.04	66798	-126	7341	-101	7240	\$86,885	255854.8	\$0.34	
Tampa	222.8	-0.17	222.63	61938	-2	6807	-1	6806	\$81,669	255854.8	\$0.32	
Tucson	219.17	-1.47	217.7	60929	-14	6696	-11	6685	\$80,219	255854.8	\$0.31	

Informative Note: In this addendum, changes to the current standard are indicated in the text by underlining (for additions) and ~~strike through~~ (for deletions) unless the instructions specifically mention some other means of indicating the changes.

Addendum bo to Standard 90.1-2022

Modify Section 3.2 as shown (I-P and SI).

fan electrical input power: the electrical input power in *kilowatts* required to operate an individual fan or fan array at design conditions. It includes the power consumption of motor controllers, if present.

fan nameplate electrical input power: the nominal electrical input power rating stamped on a fan assembly nameplate.

fan system: all the fans that contribute to the movement of air serving *spaces* that pass through a point of a common duct, plenum, or cabinet.

fan system, complex: a fan system that combines a single-cabinet fan system with other supply fans, exhaust fans, or both.

fan system, exhaust/relief: a fan system dedicated to the removal of air from interior spaces to the outdoors.

fan system, return: a fan system dedicated to removing air from interior spaces where some or all the air is to be recirculated except during economizer operation.

fan system, supply-only: a fan system that provides supply air to interior spaces and does not recirculate the air.

fan system, single-cabinet: a fan system where a single fan, single fan array, single set of fans operating in parallel, or fans or fan arrays in series are embedded in the same cabinet that both supply air to a space and recirculate the air.

fan system, transfer: a fan system that exclusively moves air from one occupied space to another.

fan system airflow: the sum of the airflow of all fans with fan electrical input power greater than 1 kW at fan system design conditions, excluding the airflow that passes through downstream fans with fan electrical input power not greater than 1 kW.

fan system design conditions: operating conditions that can be expected to occur during normal system operation that result in the highest supply-airflow rate of to conditioned spaces served by the system, other than during air economizer operation.

fan system electrical input power: sum of the fan electrical power fan electrical input power, in *kilowatts*, of all fans that are required to operate at fan system design conditions to supply air from the heating or cooling source to the conditioned spaces, return it to the source, exhaust it to the outdoors, or transfer it to another space.

Modify Section 6.1.4 as shown (I-P and SI).

6.1.4 Alterations to Heating, Ventilating, Air Conditioning, and Refrigeration in Existing Buildings

6.1.4.1 New HVACR equipment as a direct replacement of existing HVACR equipment shall comply with the following sections as applicable for the equipment being replaced:

- a. 6.3, "Simplified Approach Option for HVAC Systems"
- b. 6.4.1, "Equipment Efficiencies, Verification, and Labeling Requirements"
- c. 6.4.3.1, "Zone Thermostatic Controls"
- d. 6.4.3.2, "Set-Point Overlap Restrictions"
- e. 6.4.3.3, "Off-Hour Controls" except for Section 6.4.3.3.4, "Zone Isolation"
- f. 6.4.3.4, "Ventilation System Controls"
- g. 6.4.3.7, "Freeze Protection and Snow/Ice Melting Systems"
- h. 6.4.3.8, "Ventilation Controls for High-Occupancy Areas" only for single-zone equipment
- i. 6.4.3.9, "Heated or Cooled Vestibules"
- j. 6.4.5, "Walk-In Coolers and Walk-In Freezers"
- k. 6.5.1.1, "Air Economizers" for units located outdoors
- l. 6.5.1.3, "Integrated Economizer Control"
- m. 6.5.1.4, "Economizer Heating System Impact"
- n. 6.5.3.1.1 "Fan Power Limits"
- no. 6.5.3.1.3, "Fan Efficiency"
- op. 6.5.3.2.1, "Supply Fan Airflow Control"
- pq. 6.5.3.6, "Fractional Horsepower Fan Motors"
- qr. 6.5.4.1, "Boiler Turndown"
- rs. 6.5.4.3, "Chiller and Boiler Isolation"
- st. 6.5.5.2, "Fan Speed Control"

Modify Section 6.5.3.1 as shown (I-P and SI). (Note: For readability, new equations are not underlined.)

6.5.3 Air System Design and Control

6.5.3.1 Fan System Power and Efficiency

6.5.3.1.1 Fan Power Limits. Each ~~HVAC~~ fan system that includes at least one fan or fan array with fan electrical input power greater than 1 kW, fan system electrical input power determined per Section 6.5.3.1.1.2 at the fan system design airflow shall not exceed the limit as calculated per Section 6.5.3.1.1.1. ~~system having a total fan system motor nameplate horsepower/kilowatts exceeding 5 hp/3.7 kW at fan system design conditions shall not exceed the allowable fan system motor nameplate horsepower/kilowatts (Option 1) or fan system bhp/input kW (Option 2) as shown in Table 6.5.3.1-1. This includes supply fans, return/relief fans, exhaust fans, and fan-powered terminal units associated with systems providing heating or cooling capability that operate at fan system design conditions. Single-zone VAV systems shall comply with the constant volume fan power limitation.~~

6.5.3.1.1.1 Calculation of the Fan Power Limit¹. To determine the maximum fan system electrical input power allowed for a fan system, complete the following steps:

- a. Determine the fan system's classification. A fan system is considered to be multizone VAV if it meets the following requirements. Fan systems that do not meet the requirements shall be classified as other fans:
 1. The fan system must serve three or more HVAC zones, and airflow to each must be individually controlled based on heating, cooling, and/or ventilation requirements.
 2. The sum of the minimum airflows for each HVAC zone must be 40% or less of the fan system design conditions.

Exceptions to 6.5.3.1.1.1(a): Hospital, vivarium, and laboratory systems that use flow control devices on exhaust and/or return to maintain space pressure relationships necessary for occupant health and safety or environmental control may shall use the multizone VAV variable volume fan power limitation allowances.

- b. Determine the fan system type and choose the appropriate table(s) for the calculation of the fan power allowance:
 1. For single-cabinet fan systems, use the power allowances in both Table 6.5.3.1-1 and Table 6.5.3.1-2.
 2. For supply-only fan systems, use the power allowances in Table 6.5.3.1-1.
 3. For exhaust/relief fan systems, use the design exhaust or relief airflow and the power allowances in Table 6.5.3.1-2.
 4. For return and transfer fan systems, use the power allowances in Table 6.5.3.1-2.
 5. For complex fan systems, separately calculate the fan power allowance for the supply and return/exhaust systems and sum them. For the supply airflow, use supply airflow at the fan system design conditions and the power allowances in Table 6.5.3.1-1. For the return exhaust airflow, use return/exhaust airflow at the fan system design conditions and the power allowances in Table 6.5.3.1-2.
- c. For each fan system, determine the components included in the fan system and sum the fan power allowances from Table 6.5.3.1-1 and Table 6.5.3.1-2 for those components. All fan systems shall include the system base allowance. If, for a given component, only a portion of the fan system airflow passes through the component, calculate the fan power allowance for that component per this equation:

$$FPA_{adj} = \frac{Q_{comp}}{Q_{sys}} \times FPA_{comp}$$

where

FPA_{adj} = corrected fan power allowance for the component, W/cfm (W/L/s)

Q_{comp} = airflow through component, cfm (L/s)

Q_{sys} = fan system airflow, cfm (L/s)

FPA_{comp} = fan power allowance of the component from Table 6.5.3.1-1 and Table 6.5.3.1-2, W/cfm (W/L/s)

- d. Multiply the fan system design airflow by the sum of the fan power allowances for the fan system, then divide by 1000 to convert to kW. —

$$FPL = \frac{Q_{sys} \times FPA_{sum}}{1000}$$

where

1. A spreadsheet tool for checking compliance can be downloaded at <http://sspc901.ashraepcs.org/documents.php>.

Table 6.5.3.1.1 Fan Power Limitation^a (I-P)

	Limit	Constant Volume	Variable Volume
Option 1: Fan system motor nameplate hp	Allowable motor nameplate hp	$hp \leq cfm_g \times 0.0011$	$hp \leq cfm_g \times 0.0015$
Option 2: fan system bhp	Allowable fan system bhp	$bhp \leq cfm_g \times 0.00094 + A$	$bhp \leq cfm_g \times 0.0013 + A$

a: where

cfm_g = maximum design supply airflow rate to conditioned spaces served by the system in cubic feet per minute

hp = maximum combined motor nameplate horsepower

bhp = maximum combined fan brake horsepower

A = sum of $(PD \times cfm_D / 4131)$

where

PD = each applicable pressure drop adjustment from Table 6.5.3.1.2 in in. of water

cfm_D = the design airflow through each applicable device from Table 6.5.3.1.2 in cubic feet per minute

Table 6.5.3.1.2 Fan Power Limitation Pressure Drop Adjustment (I-P)

Device	Adjustment
Credits	
Return or exhaust systems required by code or accreditation standards to be fully ducted, or systems required to maintain air pressure differentials between adjacent rooms.	0.5 in. of water (2.15 in. of water for laboratory and vivarium systems)
Return and/or exhaust airflow control devices	0.5 in. of water
Exhaust filters, scrubbers, or other exhaust treatment	The pressure drop of device calculated at fan system design condition
Particulate Filtration Credit: MERV 9 through 12	0.5 in. of water
Particulate Filtration Credit: MERV 13 through 15	0.9 in. of water
Particulate Filtration Credit: MERV 16 and greater and electronically enhanced filters	Pressure drop calculated at 2× clean filter pressure drop at fan system design condition
Carbon and other gas phase air cleaners	Clean filter pressure drop at fan system design condition
Biosafety cabinet	Pressure drop of device at fan system design condition
Energy recovery device, other than coil runaround loop	For each airstream $[(2.2 \times \text{Enthalpy Recovery Ratio}) - 0.5]$ in. of water
Coil runaround loop	0.6 in. of water for each airstream
Evaporative humidifier/cooler in series with another cooling coil	Pressure drop of device at fan system design condition
Sound attenuation section (fans serving spaces with design background noise goals below NC35)	0.15 in. of water
Exhaust system serving fume hoods	0.35 in. of water
Laboratory and vivarium exhaust systems in high-rise buildings	0.25 in. of water/100 ft of vertical duct exceeding 75 ft
Deductions	
Systems without central cooling device	-0.6 in. of water
Systems without central heating device	-0.3 in. of water
Systems with central electric resistance heat	-0.2 in. of water

$$FPL \quad \equiv \quad \text{fan power limit, kW}$$

Table 6.5.3.1-1 Fan Power Limitation^a (SI)

	Limit	Constant Volume	Variable Volume
Option 1: Fan system motor nameplate kW	Allowable motor nameplate kW	$kW \leq L/s_g \times 0.0017$	$kW \leq L/s_g \times 0.0024$
Option 2: fan system input kW	Allowable fan system input kW	$kW_t \leq L/s_g \times 0.0015 + A$	$kW_t \leq L/s_g \times 0.0021 + A$

a: where

L/s_g = maximum design supply airflow rate to conditioned spaces served by the system in litres per second

kW = maximum combined motor nameplate kilowatts

kW_t = maximum combined fan input kW

A = sum of $(PD \times L/s_D / 65,000)$

where

PD = each applicable pressure drop adjustment from Table 6.5.3.1-2 in Pa

L/s_D = the design airflow through each applicable device from Table 6.5.3.1-2 in litres per second

Table 6.5.3.1-2 Fan Power Limitation Pressure Drop Adjustment (SI)

Device	Adjustment
Credits	
Return or exhaust systems required by code or accreditation standards to be fully ducted, or systems required to maintain air pressure differentials between adjacent rooms	+25 Pa (535 Pa for laboratory and vivarium systems)
Return and/or exhaust airflow control devices	+25 Pa
Exhaust filters, scrubbers, or other exhaust treatment	The pressure drop of device calculated at fan system design condition
Particulate Filtration Credit: MERV 9 through 12	+25 Pa
Particulate Filtration Credit: MERV 13 through 15	+25 Pa
Particulate Filtration Credit: MERV 16 and greater and electronically enhanced filters	Pressure drop calculated at 2× clean filter pressure drop at fan system design condition
Carbon and other gas phase air cleaners	Clean filter pressure drop at fan system design condition
Biosafety cabinet	Pressure drop of device at fan system design condition
Energy recovery device, other than coil runaround loop	For each airstream [(550 × Enthalpy Recovery Ratio) — 125] Pa
Coil runaround loop	+50 Pa for each airstream
Evaporative humidifier/cooler in series with another cooling coil	Pressure drop of device at fan system design condition
Sound attenuation section (fans serving spaces with design background noise goals below NC35)	38 Pa
Exhaust system serving fume hoods	85 Pa
Laboratory and vivarium exhaust systems in high-rise buildings	60 Pa/30 m of vertical duct exceeding 25 m
Deductions	
Systems without central cooling device	+50 Pa
Systems without central heating device	75 Pa
Systems with central electric resistance heat	50 Pa

- Q_{sys} = fan system airflow, cfm (L/s)
 FPA_{sum} = sum of the fan power allowances for the system, W/cfm (W/L/s)
 1000 = conversion from W to kW

- e. For building sites at elevations greater than 3,000 ft (900m), multiply the fan power limit by the correction factor from Table 6.5.3.1-3.

$$FPL_{alt} = FPL \times C_{alt}$$

where

- FPL_{alt} = adjusted fan power limit, kW
 FPL = fan power limit calculated in Step (d), kW
 C_{alt} = altitude correction factor from Table 6.5.3.1-3

6.5.3.1.1.2 Calculation of the Fan System Electrical Input Power. The fan system electrical input power is the sum of the fan electrical input power of each fan or fan array included in the fan system other than fans with fan electrical input power <1 kW. If variable-speed drives are used, their efficiency losses shall be included. Fan system input power shall be calculated with midlife filter pressure drop, which is the mean of the clean filter pressure drop and design final filter pressure drop. The fan electrical input power for each fan or fan array shall be determined using one of the following methods. There is no requirement to use the same method for all fans in a fan system:

- Use the default fan electrical input power in Table 6.5.3.1-4 for one or more of the fans. This method cannot be used for complex fan systems.
- Use the fan electrical input power at fan system design conditions provided by the manufacturer of the fan, fan array, or equipment that includes the fan or fan array, calculated per a test procedure included in 10 CFR Part 430, 10 CFR Part 431, ANSI/AMCA Standard 210, ASHRAE Standard 51, AHRI Standard 430, AHRI Standard 440, or ISO 5801.
- Use the fan electrical input power provided by the manufacturer, calculated at fan system design conditions per one of the methods listed in ANSI/AMCA 208, Section 5.3.
- Use the fan nameplate electrical input power.

Add the following new tables to Section 6.5.3.1 (I-P and SI).

Table 6.5.3.1-1 Fan Power Allowances for Supply Fan Systems (I-P)

Air System Component	Multizone VAV Fan System ^a Airflow, cfm			All Other Fan Systems Airflow, cfm		
	<u><5000</u>	<u>5000 to <10,000</u>	<u>>10,000</u>	<u><5000</u>	<u>5,000 to <10,000</u>	<u>>10,000</u>
	W/cfm					
Supply <i>system</i> base allowance for each <i>fan system</i>	0.413	0.472	0.480	0.243	0.267	0.248
Particle Filtration (select all that apply)						
Filter MERV 12 or less	0.094	0.079	0.073	0.097	0.084	0.075
MERV 13 to MERV 16 Filter	0.210	0.177	0.165	0.217	0.185	0.168
HEPA filter	0.347	0.292	0.277	0.357	0.304	0.278
Heating (select all that apply)						
Hydronic heating coil (central)	0.047	0.050	0.055	0.049	0.053	0.057
Electric heat	0.047	0.040	0.037	0.049	0.042	0.038
Gas or oil furnace <90% E_f or <90% AFUE	0.071	0.060	0.073	0.061	0.063	0.075
Gas or oil furnace >90% E_f or >90% AFUE	0.117	0.099	0.092	0.122	0.104	0.094
Cooling and Dehumidification (select all that apply)						
Hydronic/DX cooling coil, or heat pump coil (wet) (Healthcare facilities can select twice.)	0.141	0.118	0.110	0.146	0.125	0.112
Fluid economizer coil	0.141	0.118	0.110	0.146	0.125	0.112
Desiccant <i>system</i> —solid or liquid	0.164	0.138	0.128	0.170	0.145	0.131
Hot gas reheat coil	0.047	0.040	0.037	0.049	0.042	0.038
Series energy recovery	0.141	0.118	0.110	0.146	0.125	0.112
Evaporative humidifier/cooler in series with a cooling coil. Value shown is allowed W/cfm per 1.0 in. of water. Determine pressure loss (in. of water) at 400 fpm or maximum velocity allowed by the manufacturer, whichever is less. (Calculation required; see footnote [b].)	0.233	0.196	0.184	0.241	0.205	0.186
Energy Recovery^f						
Enthalpy recovery ratio >0.50 and <0.55	0.141	0.118	0.110	0.146	0.125	0.112
Enthalpy recovery ratio >0.55 and <0.60	0.166	0.140	0.130	0.172	0.147	0.133
Enthalpy recovery ratio >0.60 and <0.65	0.191	0.161	0.151	0.198	0.169	0.153
Enthalpy recovery ratio >0.65 and <0.70	0.217	0.182	0.171	0.224	0.191	0.173
Enthalpy recovery ratio >0.70 and <0.75	0.242	0.204	0.191	0.250	0.213	0.193
Enthalpy recovery ratio >0.75 and <0.80	0.267	0.225	0.212	0.276	0.235	0.213
Enthalpy recovery ratio >0.8	0.292	0.246	0.232	0.301	0.257	0.234
Run-around liquid or refrigerant coils	0.141	0.118	0.110	0.146	0.125	0.112
Gas-Phase Filtration						
Gas phase filtration	0.233	0.196	0.184	0.241	0.205	0.186

a. See section 6.5.3.1.1(a) for requirements a for a multizone VAV System

b. Power allowances require further calculation. Multiply the actual pressure drop of the device or component by the fan power allowance in Table 6.5.3.1-1.

c. The 100% outdoor air system must serve three or more HVAC zones.

e. A low-turndown single-zone VAV fan system must be capable of and configured to reduce airflow to 50% of design airflow and use no more than 30% of the design wattage at that airflow. No more than 10% of the design load served by the equipment shall have fixed loads

f. The deduction of 0.500 W/cfm is a default value for multizone VAV fan systems. If the terminal unit or fan-coil manufacturer can demonstrate that the share of the unit's fan power required to move the fan system's air is less than 0.500 W/cfm, that value may be used. The W/cfm shall be calculated by dividing the power required to operate the terminal unit's fan at fan system design conditions by the airflow of the terminal unit at those conditions.

g. Substitute sensible recovery ratio for enthalpy recovery ratio when a sensible energy recovery device meets the requirements of Section 6.5.6.1.1(b) or Section 6.5.6.1.2.1(b).

Table 6.5.3.1-1 Fan Power Allowances for Supply Fan Systems (I-P) (Continued)

Air System Component	Multizone VAV Fan System^a Airflow,			All Other Fan Systems Airflow,		
	cfm			cfm		
	<5000	5000 to <10,000	≥10,000	<5000	5,000 to <10,000	≥10,000
	W/cfm					
Other						
Economizer return damper	0.049	0.042	0.038	0.049	0.043	0.039
100% outdoor air system meeting the requirements of footnote (c)	0.000	0.000	0.000	0.073	0.104	0.112
Low-turndown single-zone VAV fan systems meeting the requirements in footnote (d)	0.000	0.000	0.000	0.073	0.104	0.094
Air blender	0.047	0.040	0.037	0.049	0.042	0.038
Project is an alteration where the duct system is not replaced	0.358	0.386	0.372	0.460	0.468	0.434
Sound attenuation section (fans serving spaces with design background noise goals below NC35)	0.035	0.030	0.027	0.036	0.032	0.029
Deduction for systems that feed a terminal unit or fan coil with a fan with electrical input power < 1 kW ^g	-0.500	-0.500	-0.500	-0.100	-0.100	-0.100

a. See section 6.5.3.1.1.(a) for requirements a for a multizone VAV System

b. Power allowances require further calculation. Multiply the actual pressure drop of the device or component by the fan power allowance in Table 6.5.3.1-1.

c. The 100% outdoor air system must serve three or more HVAC zones.

e. A low-turndown single-zone VAV fan system must be capable of and configured to reduce airflow to 50% of design airflow and use no more than 30% of the design wattage at that airflow. No more than 10% of the design load served by the equipment shall have fixed loads

f. The deduction of 0.500 W/cfm is a default value for multizone VAV fan systems. If the terminal unit or fan-coil manufacturer can demonstrate that the share of the unit's fan power required to move the fan system's air is less than 0.500 W/cfm, that value may be used. The W/cfm shall be calculated by dividing the power required to operate the terminal unit's fan at fan system design conditions by the airflow of the terminal unit at those conditions.

g. Substitute sensible recovery ratio for enthalpy recovery ratio when a sensible energy recovery device meets the requirements of Section 6.5.6.1.1(b) or Section 6.5.6.1.2.1(b).

Table 6.5.3.1-2 Fan Power Allowances for Exhaust, Return, Relief, Transfer Fan Systems (I-P)

Air System Component	Multizone VAV Fan System ^a Airflow, cfm			All Other Fan Systems Airflow, cfm		
	<5000	5000 to <10,000	> 10,000	<5000	5000 to <10,000	> 10,000
	W/cfm					
Exhaust, return, relief, and transfer system base allowance for each fan system	0.231	0.256	0.248	0.194	0.192	0.200
Particle Filtration						
Filter (any MERV value) ^b	0.049	0.042	0.038	0.049	0.043	0.039
Energy Recovery ^d						
Enthalpy recovery ratio ≥0.50 and <0.55	0.146	0.125	0.112	0.146	0.128	0.114
Enthalpy recovery ratio ≥0.55 and <0.60	0.173	0.148	0.133	0.173	0.150	0.135
Enthalpy recovery ratio ≥0.60 and <0.65	0.199	0.170	0.153	0.199	0.173	0.155
Enthalpy recovery ratio ≥0.65 and <0.70	0.225	0.192	0.173	0.226	0.196	0.176
Enthalpy recovery ratio ≥0.70 and <0.75	0.250	0.214	0.193	0.252	0.218	0.196
Enthalpy recovery ratio ≥0.75 and <0.80	0.276	0.236	0.213	0.277	0.240	0.216
Enthalpy recovery ratio ≥0.8	0.302	0.258	0.234	0.303	0.263	0.236
Run-around liquid or refrigerant coils	0.146	0.125	0.112	0.146	0.128	0.114
Special Exhaust and Return System Requirements (select all that apply)						
Return or exhaust systems required to be fully ducted by code or accreditation standards	0.122	0.105	0.094	0.122	0.107	0.096
Return and/or exhaust airflow control devices required by code or accreditation standards to maintain pressure relationships between spaces	0.122	0.105	0.094	0.122	0.107	0.096
Laboratory and vivarium exhaust systems in high-rise buildings for vertical duct exceeding 75 ft. Value shown is allowed W/cfm per 0.25 in. of water for each 100 ft exceeding 75 ft. (Calculation required; see footnote [c].)	0.061	0.053	0.047	0.061	0.054	0.048
Exhaust systems serving fume hoods	0.085	0.074	0.066	0.085	0.075	0.067
Biosafety cabinet. Value shown is allowed W/cfm per 1.0 in. of water air pressure drop. (Calculation required; see footnote [c].)	0.241	0.206	0.186	0.242	0.210	0.188
Exhaust filters, scrubbers, or other exhaust treatment required by code or standard. Value shown is allowed W/cfm per 1.0 in. of water air pressure drop. (Calculation required; see footnote [c].)	0.241	0.206	0.186	0.242	0.210	0.188
Other						
Project is an alteration where the duct system is not replaced.	0.253	0.256	0.232	0.289	0.291	0.262
Sound attenuation section (fans serving spaces with design background noise goals below NC35)	0.036	0.032	0.029	0.036	0.032	0.029

a. See Section 6.5.3.1.1(a) for requirements for a multizone VAV system.

b. Particle filter pressure loss can only be counted once per fan system.

c. Power allowances require further calculation. Multiply the actual pressure drop of the device or component by the fan power allowance in Table 6.5.3.1-2.

d. Substitute sensible recovery ratio for enthalpy recovery ratio when a sensible energy recovery device meets the requirements of Section 6.5.6.1.1(b) or Section 6.5.6.1.2.1(b).

Table 6.5.3.1-3 Fan Power Limit Altitude Correction Factor (I-P)

<u>Altitude, ft</u>	<u>Correction Factor</u>
<u><3000</u>	<u>1.000</u>
<u>≥3000 and <4000</u>	<u>0.896</u>
<u>≥4000 and <5000</u>	<u>0.864</u>
<u>≥5000 and <6000</u>	<u>0.832</u>
<u>≥6000</u>	<u>0.801</u>

Table 6.5.3.1-4 Default Values for Fan Electrical Input Power Based on Motor Nameplate Horsepower (I-P)

<u>Motor Nameplate Horsepower</u>	<u>Variable-Speed Drive, kW</u>	<u>Without Variable-Speed Drive, kW</u>
<u>≤1.0</u>	<u>0.96</u>	<u>0.89</u>
<u>>1.0 and ≤1.5</u>	<u>1.38</u>	<u>1.29</u>
<u>>1.5 and <2</u>	<u>1.84</u>	<u>1.72</u>
<u>>2 and ≤3</u>	<u>2.73</u>	<u>2.57</u>
<u>>3 and ≤5</u>	<u>4.38</u>	<u>4.17</u>
<u>>5 and ≤7.5</u>	<u>6.43</u>	<u>6.15</u>
<u>>7.5 and ≤10</u>	<u>8.46</u>	<u>8.13</u>
<u>>10 and ≤15</u>	<u>12.47</u>	<u>12.03</u>
<u>>15 and ≤20</u>	<u>16.55</u>	<u>16.04</u>
<u>>20 and ≤25</u>	<u>20.58</u>	<u>19.92</u>
<u>>25 and ≤30</u>	<u>24.59</u>	<u>23.77</u>
<u>>30 and ≤40</u>	<u>32.74</u>	<u>31.70</u>
<u>>40 and ≤50</u>	<u>40.71</u>	<u>39.46</u>
<u>>50 and ≤60</u>	<u>48.50</u>	<u>47.10</u>
<u>>60 and ≤75</u>	<u>60.45</u>	<u>58.87</u>
<u>>75 and ≤100</u>	<u>80.40</u>	<u>78.17</u>

a. This table cannot be used for motor nameplate horsepower values greater than 100.

b. This table is to be used only with motors with a service factor ≤1.15. If the service factor is not provided, this table may not be used.

Table 6.5.3.1-1 Fan Power Allowances for Supply Fan Systems (SI)

Air System Component	Multi-Zone VAV Fan System^a Airflow, L/s			All Other Fan Systems Airflow, L/s		
	<2360	2360 to <4720	>4720	<2360	2360 to <4720	>4720
	W/L/s					
Supply system base allowance for each <i>fan system</i>	0.195	0.223	0.227	0.115	0.126	0.117
Particle Filtration (select all that apply)						
Filter MERV 12 or less	0.044	0.037	0.035	0.046	0.039	0.036
MERV 13 to MERV 16 filter	0.099	0.083	0.078	0.102	0.088	0.079
HEPA filter	0.164	0.138	0.131	0.168	0.144	0.131
Heating (select all that apply)						
Hydronic heating coil (central)	0.022	0.023	0.026	0.023	0.025	0.027
Electric heat	0.022	0.019	0.017	0.023	0.020	0.018
Gas or oil furnace <90% E_f or <90% AFUE	0.033	0.028	0.035	0.029	0.030	0.036
Gas or oil furnace ≥90% E_f or ≥90% AFUE	0.055	0.047	0.043	0.057	0.049	0.044
Cooling and Dehumidification (select all that apply)						
Hydronic/DX cooling coil, or heat pump coil (wet) (Healthcare facilities can select twice.)	0.066	0.056	0.052	0.069	0.059	0.053
Desiccant system—solid or liquid	0.077	0.065	0.061	0.080	0.068	0.062
Hot gas reheat coil	0.022	0.019	0.017	0.023	0.020	0.018
Series energy recovery	0.066	0.056	0.052	0.069	0.059	0.053
Evaporative humidifier/cooler in series with a cooling coil. Value shown is allowed W/L/s per 250 Pa. Determine pressure loss (Pa) at 2 m/s or maximum velocity allowed by the manufacturer, whichever is less. (Calculation required; see footnote [b].)	0.110	0.092	0.087	0.114	0.097	0.088
Energy Recovery						
Enthalpy recovery ratio ≥0.50 and <0.55	0.066	0.056	0.052	0.069	0.059	0.053
Enthalpy recovery ratio ≥0.55 and <0.60	0.078	0.066	0.061	0.081	0.069	0.063
Enthalpy recovery ratio ≥0.60 and <0.65	0.090	0.076	0.071	0.094	0.080	0.072
Enthalpy recovery ratio ≥0.65 and <0.70	0.102	0.086	0.081	0.106	0.090	0.082
Enthalpy recovery ratio ≥0.70 and <0.75	0.114	0.096	0.090	0.118	0.101	0.091
Enthalpy recovery ratio ≥0.75 and <0.80	0.126	0.106	0.100	0.130	0.111	0.101
Enthalpy recovery ratio ≥0.8	0.138	0.116	0.110	0.142	0.121	0.110
Run-around liquid or refrigerant coils	0.066	0.056	0.052	0.069	0.059	0.053
Gas-Phase Filtration						
Gas-phase filtration	0.110	0.092	0.087	0.114	0.097	0.088

a. See section 6.5.3.1.1.(a) for requirements a for a multizone VAV system

b. Power allowances require further calculation. Multiply the actual pressure drop of the device or component by the fan power allowance in Table 6.5.3.1-1.

c. The 100% outdoor air system must serve three or more HVAC zones.

d. A low-turndown single-zone VAV fan system must be capable of and configured to reduce airflow to 50% of design airflow and use no more than 30% of the design wattage at that airflow. No more than 10% of the design load served by the equipment shall have fixed loads.

e. The deduction of 0.236 L/s is a default value for multizone VAV fan systems. If the terminal unit or fan-coil manufacturer can demonstrate that the share of the unit's fan power required to move the fan system's air is less than 0.236 L/s, that value may be used. The L/s shall be calculated by dividing the power required to operate the terminal unit's fan at fan system design conditions by the airflow of the terminal unit at those conditions.

f. Substitute sensible recovery ratio for enthalpy recovery ratio when a sensible energy recovery device meets the requirements of Section 6.5.6.1.1(b) or Section 6.5.6.1.2.1(b).

Table 6.5.3.1-1 Fan Power Allowances for Supply Fan Systems (SI) (Continued)

Air System Component	Multi-Zone VAV Fan System ^a Airflow,			All Other Fan Systems Airflow,		
	L/s			L/s		
	<u><2360</u>	<u>2360 to <4720</u>	<u>>4720</u>	<u><2360</u>	<u>2360 to <4720</u>	<u>>4720</u>
	W/L/s					
Other						
Economizer return damper	<u>0.023</u>	<u>0.020</u>	<u>0.018</u>	<u>0.023</u>	<u>0.020</u>	<u>0.018</u>
100% outdoor air system meeting the requirements of footnote [c]	<u>0.000</u>	<u>0.000</u>	<u>0.000</u>	<u>0.034</u>	<u>0.049</u>	<u>0.053</u>
Low-turndown single-zone VAV fan systems meeting the requirements in footnote [d]	<u>0.000</u>	<u>0.000</u>	<u>0.000</u>	<u>0.034</u>	<u>0.049</u>	<u>0.044</u>
Economizer return damper	<u>0.022</u>	<u>0.019</u>	<u>0.017</u>	<u>0.023</u>	<u>0.020</u>	<u>0.018</u>
Air blender	<u>0.022</u>	<u>0.019</u>	<u>0.017</u>	<u>0.023</u>	<u>0.020</u>	<u>0.018</u>
Project is an alteration where the duct system is not replaced	<u>0.169</u>	<u>0.182</u>	<u>0.176</u>	<u>0.217</u>	<u>0.221</u>	<u>0.205</u>
Sound attenuation section (fans serving spaces with design background noise goals below NC35)	<u>0.017</u>	<u>0.014</u>	<u>0.013</u>	<u>0.017</u>	<u>0.015</u>	<u>0.013</u>
Deduction for systems that feed a terminal unit or fan coil with a fan with electrical input power <1 kW ^e	<u>-0.236</u>	<u>-0.236</u>	<u>-0.236</u>	<u>-0.047</u>	<u>-0.047</u>	<u>-0.047</u>

a. See section 6.5.3.1.1(a) for requirements a for a multizone VAV system

b. Power allowances require further calculation. Multiply the actual pressure drop of the device or component by the fan power allowance in Table 6.5.3.1-1.

c. The 100% outdoor air system must serve three or more HVAC zones.

d. A low-turndown single-zone VAV fan system must be capable of and configured to reduce airflow to 50% of design airflow and use no more than 30% of the design wattage at that airflow. No more than 10% of the design load served by the equipment shall have fixed loads.

e. The deduction of 0.236 L/s is a default value for multizone VAV fan systems. If the terminal unit or fan-coil manufacturer can demonstrate that the share of the unit's fan power required to move the fan system's air is less than 0.236 L/s, that value may be used. The L/s shall be calculated by dividing the power required to operate the terminal unit's fan at fan system design conditions by the airflow of the terminal unit at those conditions.

f. Substitute sensible recovery ratio for enthalpy recovery ratio when a sensible energy recovery device meets the requirements of Section 6.5.6.1.1(b) or Section 6.5.6.1.2.1(b).

Table 6.5.3.1-2 Fan Power Allowances for Exhaust, Return, Relief, Transfer Fan systems

Air System Component	Multi-Zone VAV Fan System ^a Airflow, L/s			All Other Fan Systems Airflow, L/s		
	<2360	>2360 to	>4720	<2360	>2360 to	>4720
		<4720			<4720	
W/L/s						
Exhaust, return, and transfer <i>system</i> base allowance for each <i>fan system</i>	0.109	0.121	0.117	0.092	0.091	0.094
Particle Filtration						
Filter (any MERV value)	0.023	0.020	0.018	0.023	0.020	0.018
Energy recovery ^d						
Enthalpy recovery ratio ≥0.50 and <0.55	0.069	0.059	0.053	0.069	0.060	0.054
Enthalpy recovery ratio ≥0.55 and <0.60	0.081	0.070	0.063	0.081	0.071	0.064
Enthalpy recovery ratio ≥0.60 and <0.65	0.094	0.080	0.072	0.094	0.082	0.073
Enthalpy recovery ratio ≥0.65 and <0.70	0.106	0.091	0.082	0.106	0.092	0.083
Enthalpy recovery ratio ≥0.70 and <0.75	0.118	0.101	0.091	0.119	0.103	0.092
Enthalpy recovery ratio ≥0.75 and <0.80	0.130	0.111	0.101	0.131	0.113	0.102
Enthalpy recovery ratio ≥0.8	0.142	0.122	0.110	0.143	0.124	0.111
Run-around liquid or refrigerant coils	0.069	0.059	0.053	0.069	0.060	0.054
Special Exhaust and Return System Requirements (select all that apply)						
Return or exhaust <i>systems</i> required to be fully ducted by code or accreditation standards	0.057	0.049	0.044	0.057	0.050	0.045
Return and/or exhaust airflow <i>control devices</i> required by code or accreditation standards to maintain pressure relationships between <i>spaces</i>	0.057	0.049	0.044	0.057	0.050	0.045
Laboratory and vivarium exhaust <i>systems</i> in high-rise <i>buildings</i> for vertical duct exceeding 25 m. Value shown is allowed W/L/s per 60 Pa for each 30 m exceeding 25 m. (Calculation required; see note [c].)	0.029	0.025	0.022	0.029	0.025	0.023
Exhaust systems serving fume hoods	0.040	0.035	0.031	0.040	0.035	0.032
Biosafety cabinet. Value shown is allowed W/L/s per 250 Pa air pressure drop. [Calculation required, see footnote [c].]	0.114	0.097	0.088	0.114	0.099	0.089
Exhaust filters, scrubbers, or other exhaust treatment required by code or standard. Value shown is allowed W/L/s per 250 Pa air pressure drop. [Calculation required; see footnote [c].]	0.114	0.097	0.088	0.114	0.099	0.089
Other						
Project is an alteration where the duct <i>system</i> is not replaced.	0.119	0.121	0.109	0.136	0.137	0.124
Sound attenuation section (fans serving spaces with design background noise goals below NC35)	0.017	0.015	0.013	0.017	0.015	0.014

a. See Section 6.5.3.1.1(a) for requirements for a multizone VAV system.

b. Particle filter pressure loss can only be counted once per fan system.

c. Power allowances require further calculation. Multiply the actual pressure drop of the device or component by the fan power allowance in Table 6.5.3.1-2.

d. Substitute sensible recovery ratio for enthalpy recovery ratio when a sensible energy recovery device meets the requirements of Section 6.5.6.1.1(b) or Section 6.5.6.1.2.1(b).

Table 6.5.3.1-3 Fan Power Limit Altitude Correction Factor

<u>Altitude,</u> <u>m</u>	<u>Correction</u> <u>Factor</u>
<900	1.000
≥900 and <1200	0.896
≥1200 and <1500	0.864
≥1500 and <1800	0.832
≥1800	0.801

Table 6.5.3.1-4 Default Values for Fan Electrical Input Power Based on Motor Nameplate Horsepower

<u>Motor Nameplate,</u> <u>kW</u>	<u>Variable-Speed Drive,</u> <u>kW</u>	<u>Without Variable-Speed Drive,</u> <u>kW</u>
≤0.75	0.96	0.89
>0.75 and ≤1.1	1.38	1.29
>1.1 and ≤1.5	1.84	1.72
>1.5 and ≤2.2	2.73	2.57
>2.2 and ≤3.7	4.38	4.17
>3.7 and ≤5.5	6.43	6.15
>5.5 and ≤7.5	8.46	8.13
>7.5 and ≤11	12.47	12.03
>11 and ≤15	16.55	16.04
>15 and ≤18.5	20.58	19.92
>18.5 and ≤22	24.59	23.77
>22 and ≤30	32.74	31.7
>30 and ≤37	40.71	39.46
>37 and ≤45	48.5	47.1
>45 and ≤55	60.45	58.87
>55 and ≤75	80.4	78.17

a. This table cannot be used for motor nameplate kilowatt values greater than 75.

b. This table is to be used only with motors with a service factor <1.15. If the service factor is not provided, this table may not be used.

Modify Section 13 as shown (I-P and SI).

<u>Reference</u>	<u>Section</u>
Air Conditioning, Heating and Refrigeration Institute (AHRI) 2311 Wilson Blvd., Arlington, VA 22201	
AHRI 430 (I-P/2020) AHRI 431 (SI/2020)	Performance Rating of Central Station Air-handling Unit Supply Fans 6.5.3.1.1.2
AHRI 440 (I-P/2019) AHRI 441 (SI/2019)	Performance Rating of Fan-coil Units 6.5.3.1.1.2
Air Movement and Control Association International (AMCA) 30 West University Drive, Arlington Heights, IL 60004-1806	
ANSI/AMCA 210-16	Laboratory Methods of Testing Fans for Certified Aerodynamic Performance Rating 6.5.3.1.1.2
International Organization for Standardization (ISO) ISO Central Secretariat BIBC II Chemin de Blandonnet 8, CP 401, 1214 Vernier, Geneva, Switzerland	
ISO 5801:2017	Fans—Performance Testing Using Standardized Airways 6.5.3.1.1.2

POLICY STATEMENT DEFINING ASHRAE'S CONCERN FOR THE ENVIRONMENTAL IMPACT OF ITS ACTIVITIES

ASHRAE is concerned with the impact of its members' activities on both the indoor and outdoor environment. ASHRAE's members will strive to minimize any possible deleterious effect on the indoor and outdoor environment of the systems and components in their responsibility while maximizing the beneficial effects these systems provide, consistent with accepted Standards and the practical state of the art.

ASHRAE's short-range goal is to ensure that the systems and components within its scope do not impact the indoor and outdoor environment to a greater extent than specified by the Standards and Guidelines as established by itself and other responsible bodies.

As an ongoing goal, ASHRAE will, through its Standards Committee and extensive Technical Committee structure, continue to generate up-to-date Standards and Guidelines where appropriate and adopt, recommend, and promote those new and revised Standards developed by other responsible organizations.

Through its *Handbook*, appropriate chapters will contain up-to-date Standards and design considerations as the material is systematically revised.

ASHRAE will take the lead with respect to dissemination of environmental information of its primary interest and will seek out and disseminate information from other responsible organizations that is pertinent, as guides to updating Standards and Guidelines.

The effects of the design and selection of equipment and systems will be considered within the scope of the system's intended use and expected misuse. The disposal of hazardous materials, if any, will also be considered.

ASHRAE's primary concern for environmental impact will be at the site where equipment within ASHRAE's scope operates. However, energy source selection and the possible environmental impact due to the energy source and energy transportation will be considered where possible. Recommendations concerning energy source selection should be made by its members.

ASHRAE · 180 Technology Parkway · Peachtree Corners, GA 30092 · www.ashrae.org

About ASHRAE

Founded in 1894, ASHRAE is a global professional society committed to serve humanity by advancing the arts and sciences of heating, ventilation, air conditioning, refrigeration, and their allied fields.

As an industry leader in research, standards writing, publishing, certification, and continuing education, ASHRAE and its members are dedicated to promoting a healthy and sustainable built environment for all, through strategic partnerships with organizations in the HVAC&R community and across related industries.

To stay current with this and other ASHRAE Standards and Guidelines, visit www.ashrae.org/standards, and connect on LinkedIn, Facebook, Twitter, and YouTube.

Visit the ASHRAE Bookstore

ASHRAE offers its Standards and Guidelines in print, as immediately downloadable PDFs, and via ASHRAE Digital Collections, which provides online access with automatic updates as well as historical versions of publications. Selected Standards and Guidelines are also offered in redline versions that indicate the changes made between the active Standard or Guideline and its previous edition. For more information, visit the Standards and Guidelines section of the ASHRAE Bookstore at www.ashrae.org/bookstore.

IMPORTANT NOTICES ABOUT THIS STANDARD

To ensure that you have all of the approved addenda, errata, and interpretations for this Standard, visit www.ashrae.org/standards to download them free of charge.

Addenda, errata, and interpretations for ASHRAE Standards and Guidelines are no longer distributed with copies of the Standards and Guidelines. ASHRAE provides these addenda, errata, and interpretations only in electronic form to promote more sustainable use of resources.