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ADDENDA

ASHRAE Addendum p to ASHRAE Guideline 36-2021

High-Performance Sequences of Operation for HVAC Systems

Approved by ASHRAE and the American National Standards Institute on February 29, 2024.

This addendum was approved by a Standing Standard Project Committee (SSPC) for which the Standards Committee has established a documented program for regular publication of addenda or revisions, including procedures for timely, documented, consensus action on requests for change to any part of the standard. Instructions for how to submit a change can be found on the ASHRAE® website (www.ashrae.org/continuous-maintenance).

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ASHRAE Standing Guideline Project Committee 36 Cognizant TC: 1.4, Control Theory and Application SPLS Liaison: Jennifer A. Isenbeck

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FOREWORD

This addendum addresses the following:

- 1. Removes redundant text in the AHU Automatic Fault Detection and Diagnostics sections.
- 2. Clarifies how to calculate %OA when an airflow monitoring station is used for Multiple Zone VAV Air Handling Units.
- 3. Adds an option to evaluate FC#6 using an airflow monitoring station for Single Zone VAV Air Handling Units.
- 4. Fixes errors in the Single Zone VAV Air Handling Unit AFDD for fault conditions FC#3 and FC#9.

Note: In this addendum, changes to the current guideline are indicated in the text by underlining (for additions) and strikethrough (for deletions) unless the instructions specifically mention some other means of indicating the changes.

Addendum p to Guideline 36-2021

(IP and SI Units)

Revise Section 5.16.13.5 as follows:

5.16.13.5. Low building pressure (less than 0 Pa [0.0 in. of water], i.e., negative) for 5 minutes: Level 4.

Automatic fault detection and diagnostics (AFDD) is a sophisticated system for detecting and diagnosing airhandler faults.

To function correctly, AFDD requires specific sensors and data be available, as detailed in the sequences below. If this information is not available, AFDD tests that do not apply should be deleted.

Revise Section 5.16.14 as follows:

5.16.14. Automatic Fault Detection and Diagnostics

<u>Automatic fault detection and diagnostics (AFDD) is a sophisticated system for detecting and diagnosing airhandler faults.</u>

<u>To function correctly, AFDD requires specific sensors and data be available, as detailed in the sequences below. If</u> this information is not available, AFDD tests that do not apply should be deleted.

The AFDD routines for AHUs continually assess AHU performance by comparing the values of BAS inputs and outputs to a subset of potential fault conditions. The subset of potential fault conditions that is assessed at any point depends on the operating state (OS) of the AHU, as determined by the position of the cooling and heating valves and the economizer damper. Time delays are applied to the evaluation and reporting of fault conditions to suppress false alarms. Fault conditions that pass these filters are reported to the building operator along with a series of possible causes.

These equations assume that the air handler is equipped with hydronic heating and cooling coils, as well as a fully integrated economizer. If any of these components are not present, the associated tests and variables should be omitted from the programming.

5.16.14.1. Note that tThese alarms rely on reasonably accurate measurement of mixed air temperatures, so the use of averaging temperature sensors is. An MAT sensor is required for many of these alarms to work, and an averaging sensor is strongly recommended for best accuracy as mixing box conditions are often highly non-uniform. AFDD conditions are evaluated continuously and separately for each operating AHU.

The engineer must specify whether the unit has a return fan, relief dampers or relief fans and a separate minimum outdoor air damper or relief dampers or relief fans and a single common damper for minimum outdoor air and economizer functions.

If there is a return fan, keep Section 5.16.14.2 and delete Sections 5.16.14.3 and 5.16.14.4.

If there are relief dampers or relief fans and a separate minimum outdoor air damper, keep Section 5.16.14.3 and delete Sections 5.16.14.2 and 5.16.14.4.

If there are relief dampers or relief fans and a single common damper for minimum outdoor air and economizer functions, keep Section 5.16.14.4 and delete Sections 5.16.14.2 and 5.16.14.3.

Delete this flag note after selections have been made.

5.16.14.2. For units with return fans:

a. The OS of each Ahu shall be defined by the commanded positions of the heating coil control valve, cooling coil control valve and the return air damper in accordance with Table 5.16.14.2.

Informative Table 5.1.14.4 Table 5.16.14.2 VAV AHU Operating States

Operating State	Heating Valve Position	Cooling Valve Position	Return Air Damper Position
#1: Heating	> 0	= 0	= MaxRA-P
#2: Free cooling, modulating OA	= 0	= 0	MaxRA-P > x > 0%
#3: Mechanical + economizer cooling	= 0	> 0	= 0%
#4: Mechanical cooling, minimum OA	= 0	> 0	= MaxRA-P
#5: Unknown or dehumidification	No other OS applie	es	

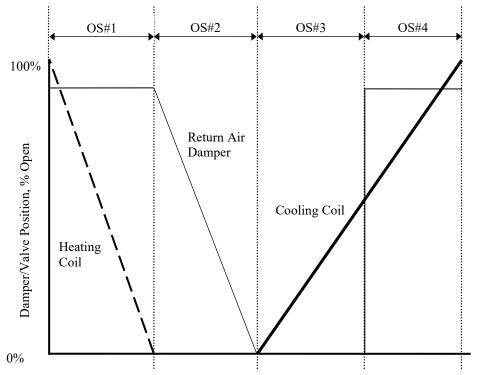


Figure 5.16.14.2 VAV AHU operating states.

5.16.14.3. For units with relief dampers or relief fans and a separate minimum outdoor air damper:

a. The OS of each AHU shall be defined by the commanded positions of the heating-coil control valve, cooling-coil control valve, and economizer damper in accordance with Table 5.16.14.3 and Figure 5.16.14.3.

Informative Table 5.1.14.4 Table 5.16.14.3 VAV AHU Operating States

Operating State	Heating Valve Position	Cooling Valve Position	Economizer Outdoor Air Damper Position
#1: Heating	> 0	= 0	= 0%
#2: Free cooling, modulating OA	= 0	= 0	0% < x < 100%
#3: Mechanical + economizer cooling	= 0	> 0	= 100%
#4: Mechanical cooling, minimum OA	= 0	> 0	= 0%
#5: Unknown or dehumidification	No other OS appl	ies	

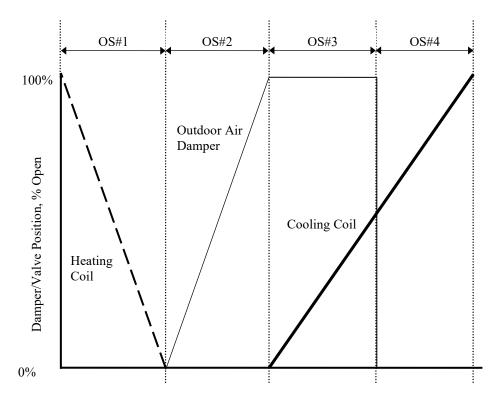


Figure 5.16.14.3 VAV AHU operating states.

- 5.16.14.4. For units with relief dampers or relief fans and a single common damper of minimum outdoor air and economizer functions.
 - a. The OS of each AHU shall be defined by the commanded positions of the heating-coil control valve, cooling-coil control valve, and economizer damper in accordance with Table 5.16.14.4 and Figure 5.16.14.4.

Informative Table 5.1.14.4 Table 5.16.14.4 VAV AHU Operating States

Operating State	Heating Valve Position	Cooling Valve Position	Outdoor Air Damper Position
#1: Heating	> 0	= 0	= MinOA-P
#2: Free cooling, modulating OA	= 0	= 0	MinOA-P < x < 100%
#3: Mechanical + economizer cooling	= 0	> 0	= 100%
#4: Mechanical cooling, minimum OA	= 0	> 0	= MinOA-P
#5: Unknown or dehumidification	No other OS applie	S	

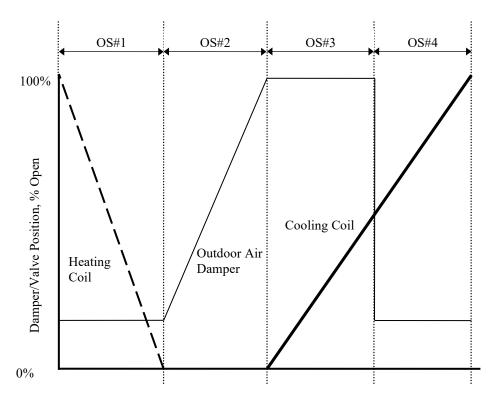


Figure 5.16.14.4 VAV AHU operating states.

The OS is distinct from, and should not be confused with, the zone status (cooling, heating, deadband) or Zone Group mode (occupied, warmup, etc.).

OS#1 through OS#4 (see Tables 5.16.14.2 through 5.16.14.4) represent normal operation during which a fault may nevertheless occur if so determined by the fault condition tests in Section 5.16.14.8. By contrast, OS#5 may represent an abnormal or incorrect condition (such as simultaneous heating and cooling) arising from a controller failure or programming error, but it may also occur normally, e.g., when dehumidification is active or during warmup.

5.16.14.5. The following points must be available to the AFDD routines for each AHU:

For the AFDD routines to be effective, an averaging sensor is recommended for SAT. An averaging sensor is essential for MAT, as the environment of the mixing box will be subject to nonuniform and fluctuating air temperatures. It is recommended that the OAT sensor be located at the AHU so that it accurately represents the temperature of the incoming air.

- a. SAT = supply air temperature
- b. MAT = mixed air temperature
- c. RAT = return air temperature
- d. OAT = outdoor air temperature
- e. DSP = duct static pressure
- f. SATSP = supply air temperature setpoint
- g. DSPSP = duct static pressure setpoint

- h. HC = heating coil valve position command; 0% ≤ HC ≤ 100%
- i. CC = cooling-coil valve position command; 0% ≤ CC ≤ 100%
- j. FS = fan speed command; $0\% \le FS \le 100\%$
- k. CCET = cooling coil entering temperature (Depending on the AHU configuration, this could be the MAT or a separate sensor for this specific purpose.)
- l. CCLT = cooling coil leaving temperature (Depending on the AHU configuration, this could be the SAT or a separate sensor for this specific purpose.)
- m. HCET = heating coil entering temperature (Depending on the AHU configuration, this could be the MAT or a separate sensor for this specific purpose.)
- n. HCLT = heating coil leaving temperature (Depending on the AHU configuration, this could be the SAT or a separate sensor for this specific purpose.)
- 5.16.14.6. The following values must be continuously calculated by the AFDD routines for each AHU:
 - a. Five minute rolling averages with 1 minute sampling time of the following point values; operator shall have the ability to adjust the averaging window and sampling period for each point independently.
- 5.16.14.5. For each AHU, the following values must be continuously monitored or determined by the AFDD routines and mapped to the indicated variables, which are used in the fault detection equations that follow.
 - a. <u>Continuously measure the following points:</u>
 - 1. SATSP = supply air temperature setpoint
 - 2. HC = heating-coil valve position command; $0\% \le HC \le 100\%$
 - 3. $CC = cooling-coil valve position command; <math>0\% \le CC \le 100\%$
 - 4. FS = fan speed command; $0\% \le FS \le 100\%$
 - 5. <u>DSPSP = duct static pressure setpoint</u>
 - b. Calculate five-minute rolling averages with one-minute sampling time of the following point values; operator shall have the ability to adjust the averaging window and sampling period for each point independently.
 - 1. $SAT_{avg} = rolling$ average of supply air temperature
 - 2. MAT_{avg} = rolling average of mixed air temperature
 - 3. $RAT_{avg} = rolling$ average of return air temperature
 - 4. $OAT_{avg} = rolling$ average of outdoor air temperature
 - 5. $DSP_{avg} = rolling$ average of duct static pressure

- 6. CCET_{avg} = rolling average of cooling-coil entering temperature (depending on the AHU configuration, this could be the MAT or a separate sensor for this specific purpose).
- 7. CCLT_{avg} = rolling average of cooling-coil leaving temperature (depending on the AHU configuration, this could be the SAT or a separate sensor for this specific purpose).
- 8. HCET_{avg} = rolling average of heating-coil entering temperature (depending on the AHU configuration, this could be the MAT or a separate sensor for this specific purpose).
- 9. HCLT_{avg} = rolling average of heating-coil leaving temperature (depending on the AHU configuration, this could be the SAT or a separate sensor for this specific purpose).
- c. %OA = actual outdoor air fraction as a percentage = (MAT RAT)/(OAT RAT), or <u>active</u> outdoor airflow divided by total airflow rate, Vps, perif airflow measurement station isif available.
- d. %OAmin = active minimum OA setpoint (MinOAsp) divided by actual total airflow (from sum of VAV box flows or by airflow measurement station) as a percentage.
- e. OS = number of changes in operating state during the previous 60 minutes (moving window)
- 5.16.14.6. The internal variables shown in Table 5.16.14.65.16.14.5 shall be defined for each AHU. All parameters are adjustable by the operator, with initial values as shown.

Default values are derived from NISTIR 7365 and have been validated in field trials. They are expected to be appropriate for most circumstances, but individual installations may benefit from tuning to improve sensitivity and reduce false alarms.

The default values have been intentionally biased toward minimizing false alarms—if necessary, at the expense of missing real alarms. This avoids excessive false alarms that will erode user confidence and responsiveness. However, if the goal is to achieve the best possible energy performance and system operation, these values should be adjusted based on field measurement and operational experience.

Values for physical factors, such as fan heat, duct heat gain, and sensor error, can be measured in the field or derived from trend logs. Likewise, the occupancy delay and switch delays can be refined by observing in trend data the time required to achieve quasi steady-state operation.

Other factors can be tuned by observing false positives and false negatives (i.e., unreported faults). If transient conditions or noise cause false errors, increase the alarm delay. Likewise, failure to report real faults can be addressed by adjusting the heating coil, cooling coil, temperature, or flow thresholds.

Table 5.16.14.65.16.14.7 VAV AHU AFDD Internal Variables

Variable Name	Description	Default Value
ΔT_{SF}	Temperature rise across supply fan	1°C (2°F)
ΔT_{MIN}	Minimum difference between OAT and RAT to evaluate economizer error conditions (FC#6)	6°C (10° F)
\mathcal{E}_{SAT}	Temperature error threshold for SAT sensor	1°C (2°F)
$\mathcal{E}_{\mathrm{RAT}}$	Temperature error threshold for RAT sensor	1°C (2°F)
$\mathcal{E}_{ ext{MAT}}$	Temperature error threshold for MAT sensor	3°C (5°F)

Variable Name	Description	Default Value
$\mathcal{E}_{\mathrm{OAT}}$	Temperature error threshold for OAT sensor	1°C (2°F) if local sensor @ unit.
		3°C (5°F) if global sensor.
$\epsilon_{\scriptscriptstyle F}$	Airflow error threshold	30%
$\epsilon_{ ext{vfdspd}}$	VFD speed error threshold	5%
\mathcal{E}_{DSP}	Duct static pressure error threshold	25 Pa (0.1")
$\mathcal{E}_{\text{CCET}}$	Cooling coil entering temperature sensor error. Equal to ϵ_{MAT} or dedicated sensor error	E _{MAT} or error of dedicated sensor Varies, see Description
$\mathcal{E}_{ ext{CCLT}}$	Cooling coil leaving temperature sensor error. Equal to ϵ_{SAT} or dedicated sensor error	E _{SAT} or error of dedicated sensor
$\mathcal{E}_{ ext{HCET}}$	Heating coil entering temperature sensor error; equal to \mathcal{E}_{MAT} or dedicated sensor error	E _{MAT} or error of dedicated sensor
$\epsilon_{ ext{HCLT}}$	Heating coil leaving temperature sensor error. Equal to ϵ_{SAT} or dedicated sensor error	E _{SAT} or error of dedicated sensor
ΔOS_{MAX}	Maximum number of changes in Operating State during the previous 60 minutes (moving window)	7
ModeDelay	Time in minutes to suspend Fault Condition evaluation after a change in Mode	30
AlarmDelay	Time in minutes to that a Fault Condition must persist before triggering an alarm	30
TestModeDelay	Time in minutes that Test Mode is enabled	120

The purpose of ΔT min is to ensure that the mixing box/economizer damper tests are meaningful. These tests are based on the relationship between supply, return, and outdoor air. If $RAT \sim MAT$, these tests will not be accurate and will produce false alarms.

The purpose of TestModeDelay is to ensure that normal fault reporting occurs after the testing and commissioning process is completed as prescribed in Section 5.16.14.14.

- 5.16.14.7. Table 5.16.14.8 shows potential fault conditions that can be evaluated by the AFDD routines. If the equation statement is TRUE, then the specified fault condition exists. The fault conditions to be evaluated at any given time will depend on the OS of the AHU. Table 5.16.14.7 shows fault conditions that can be evaluated by the AFDD routines.
 - a. If the equation statement is TRUE, then the specified fault condition exists.
 - b. Only those fault condition equations that apply to the current OS of the AHU shall be evaluated.

The equations in Table <u>5.16.14.7</u>5.16.14.8 assume that the SAT sensor is located downstream of the supply fan and the RAT sensor is located downstream of the return fan. If actual sensor locations differ from these assumptions, it may be necessary to add or delete fan heat correction factors.

To detect the required economizer faults in California Title 24 section 120.2(i)7, use FC#2, #3, and #5 through #13 at a minimum. Other Title 24 AFDD requirements, including acceptance tests, are not met through these fault conditions.

Table 5.16.14.75.16.14.8 VAV AHU Fault Conditions

Table <u>5.10.14.7</u> 5.10.14.8 VAV ATO Faun Conditions				
	Equation	$DSP_{AVG} < DSPSP - \mathcal{E}_{DSP}$ and $VFDSPD \geq 99\% - \mathcal{E}_{VFDSPD}$ Ap		
FC#1	Description	Duct static pressure is too low with fan at full speed	to OS	
	Possible Diagnosis	Problem with VFD Mechanical problem with fan Fan undersized SAT Setpoint too high (too much zone demand)	#1 – #5	
ECHA	Equation	$MAT_{AVG} + \varepsilon_{MAT} < min[(RAT_{AVG} - \varepsilon_{RAT}), (OAT_{AVG} - \varepsilon_{OAT})]$		
FC#2 (omit if	Description	MAT too low; should be between OAT and RAT	Applies	
no MAT sensor)	Possible Diagnosis	RAT sensor error MAT sensor error OAT sensor error	to OS #1 – #5	
FC#3	Equation	$MAT_{AVG} - \mathcal{E}_{MAT} > max[(RAT_{AVG} + \mathcal{E}_{RAT}), (OAT_{AVG} + \mathcal{E}_{OAT})]$		
(omit if	Description	MAT too high; should be between OAT and RAT	Applies	
no MAT sensor)	Possible Diagnosis	RAT sensor error MAT sensor error OAT sensor error	to OS #1 – #5	
	Equation	$\Delta OS > \Delta OS_{MAX}$	Ammliag	
FC#4	Description	Too many changes in Operating State	Applies to OS	
	Possible Diagnosis	Unstable control due to poorly tuned loop or mechanical problem	#1 – #5	
	Equation	$SAT_{AVG} + \epsilon_{SAT} \le MAT_{AVG} - \epsilon_{MAT} + \Delta T_{SF}$		
-	Description	SAT too low; should be higher than MAT		
FC#5 (omit if no MAT sensor)	Possible Diagnosis	SAT sensor error MAT sensor error Cooling coil valve leaking or stuck open Heating coil valve stuck closed or actuator failure Fouled or undersized heating coil HW temperature too low or HW unavailable Gas or electric heat unavailable DX cooling stuck on	Applies to OS #1	

	Equation	$ \ RAT_{AVG} - OAT_{AVG}\ \geq \Delta T_{MIN}$ and $ \ \%OA - \%OA_{MIN}\ > \epsilon_F$	Applies
FC#6	Description	OA fraction is too low or too high; should equal %OA _{MIN}	to OS
	Possible Diagnosis	RAT sensor error MAT sensor error OAT sensor error Leaking or stuck economizer damper or actuator	#1, #4
	Equation	$SAT_{AVG} < SATSP - \mathcal{E}_{SAT}$ and $HC \geq 99\%$	
FC#7	Description	SAT too low in full heating	Annling
(omit if no no heating coil)	Possible Diagnosis	SAT sensor error Cooling coil valve leaking or stuck open Heating coil valve stuck closed or actuator failure Fouled or undersized heating coil HW temperature too low or HW unavailable Gas or electric heat unavailable DX cooling stuck on Leaking or stuck economizer damper or actuator	Applies to OS #1
EC#0	Equation	$ SAT_{AVG} - \Delta T_{SF} - MAT_{AVG} > \sqrt{\epsilon_{SAT}^2 + \epsilon_{MAT}^2}$	
FC#8 (omit if	Description	SAT and MAT should be approximately equal	Applies to OS
no MAT sensor)	Possible Diagnosis	SAT sensor error MAT sensor error Cooling coil valve leaking or stuck open Heating coil valve leaking or stuck open	#2
	Equation	OAT_{AVG} - \mathcal{E}_{OAT} > $SATSP$ - ΔT_{SF} + \mathcal{E}_{SAT}	
FC#9	Description	OAT is too high for free cooling without additional mechanical cooling	Applies to OS
	Possible Diagnosis	SAT sensor error OAT sensor error Cooling coil valve leaking or stuck open	#2
FC#10	Equation	$ MAT_{AVG} - OAT_{AVG} > \sqrt{{\epsilon_{MAT}}^2 + {\epsilon_{OAT}}^2}$	Annling
(omit if	Description	OAT and MAT should be approximately equal	Applies to OS
no MAT sensor)	Possible Diagnosis	MAT sensor error OAT sensor error Leaking or stuck economizer damper or actuator	#3

	Equation	$OAT_{AVG} + \epsilon_{OAT} < SATSP - \Delta T_{SF} - \epsilon_{SAT}$	
	Description	OAT is too low for mechanical cooling	Applies
FC#11	Possible Diagnosis	SAT sensor error OAT sensor error Heating coil valve leaking or stuck open Leaking or stuck economizer damper or actuator	to OS #3
	Equation	$SAT_{AVG} - \epsilon_{SAT} - \Delta T_{SF} \ge MAT_{AVG} + \epsilon_{MAT}$	
	Description	SAT too high; should be less than MAT	
FC#12 (omit if no MAT sensor)	Possible Diagnosis	SAT sensor error MAT sensor error Cooling coil valve stuck closed or actuator failure Fouled or undersized cooling coil CHW temperature too high or CHW unavailable DX cooling unavailable Gas or electric heat stuck on Heating coil valve leaking or stuck open	Applies to OS #2 – #4
	Equation	$SAT_{AVG} > SATSP + \varepsilon_{SAT}$ and $CC \ge 99\%$	
	Description	SAT too high in full cooling	Annlies
FC#13	Possible Diagnosis	SAT sensor error Cooling coil valve stuck closed or actuator failure Fouled or undersized cooling coil CHW temperature too high or CHW unavailable DX cooling unavailable Gas or electric heat stuck on Heating coil valve leaking or stuck open	Applies to OS #3, #4
FC#14	Equation Description	CCET _{AVG} - CCLT _{AVG} $\geq \sqrt{\epsilon_{CCET}^2 + \epsilon_{CCLT}^2} + \Delta T_{SF}^*$ *Fan heat factor included or not depending on location of sensors used for CCET and CCLT Temperature drop across inactive cooling coil	Applies to OS #1, #2
Possible Diagnosis		CCET sensor error CCLT sensor error Cooling coil valve stuck open or leaking DX cooling stuck on	
FC#15	Equation $ \begin{aligned} & + CLT_{AVG} - HCET_{AVG} \geq \sqrt{\epsilon_{HCET}}^2 + \epsilon_{HCLT}^2 + \Delta T_{SF}^* \\ & *Fan \ heat \ factor \ included \ or \ not \ depending \ on \ location \ of \\ & sensors \ used \ for \ HCET \ and \ HCLT \end{aligned} $		Applies to OS #2 – #4
	Description Temperature rise across inactive heating coil Possible Diagnosis HCET sensor error HCLT sensor error Heating coil valve stuck open or leaking.		

5.16.14.10. A subset of all potential fault conditions is evaluated by the AFDD routines. The set of applicable fault conditions depends on the OS of the AHU:

- a. In OS#1 (heating), the following fault conditions shall be evaluated:
 - 1. FC#1: DSP too low with fan at full speed
 - 2. FC#2: MAT too low; should be between RAT and OAT
 - 3. FC#3: MAT too high; should be between RAT and OAT
 - 4. FC#4: Too many changes in OS
 - 5. FC#5: SAT too low; should be higher than MAT
 - 6. FC#6: OA fraction too low or too high; should equal %OAmin
 - 7. FC#7: SAT too low in full heating
 - 8. FC#14: Temperature drop across inactive cooling coil
- b. In OS#2 (modulating economizer), the following fault conditions shall be evaluated:
 - 1. FC#1: DSP too low with fan at full speed
 - 2. FC#2: MAT too low; should be between RAT and OAT
 - 3. FC#3: MAT too high; should be between RAT and OAT
 - 4. FC#4: Too many changes in OS
 - 5. FC#8: SAT and MAT should be approximately equal
 - 6. FC#9: OAT too high for free cooling without mechanical cooling
 - 7. FC#12: SAT too high; should be less than MAT
 - 8. FC#14: Temperature drop across inactive cooling coil
 - 9. FC#15: Temperature rise across inactive heating coil
- c. In OS#3 (mechanical + 100% economizer cooling), the following fault conditions shall be evaluated:
 - 1. FC#1: DSP too low with fan at full speed
 - 2. FC#2: MAT too low; should be between RAT and OAT
 - 3. FC#3: MAT too high; should be between RAT and OAT
 - 4. FC#4: Too many changes in OS
 - 5. FC#10: OAT and MAT should be approximately equal
 - 6. FC#11: OAT too low for mechanical cooling
 - 7. FC#12: SAT too high; should be less than MAT

- 8. FC#13: SAT too high in full cooling
- 9. FC#15: Temperature rise across inactive heating coil
- d. In OS#4 (mechanical Cooling, minimum OA), the following fault conditions shall be evaluated:
 - 1. FC#1: DSP too low with fan at full speed
 - 2. FC#2: MAT too low; should be between RAT and OAT
 - 3. FC#3: MAT too high; should be between RAT and OAT
 - 4. FC#4: Too many changes in OS
 - 5. FC#6: OA fraction too low or too high; should equal %OAmin
 - 6. FC#12: SAT too high; should be less than MAT
 - 7. FC#13: SAT too high in full cooling
 - 8. FC#15: Temperature rise across inactive heating coil
- e. In OS#5 (other), the following fault conditions shall be evaluated:
 - 1. FC#1: DSP too low with fan at full speed
 - 2. FC#2: MAT too low; should be between RAT and OAT
 - 3. FC#3: MAT too high; should be between RAT and OAT
 - 4. FC#4: Too many changes in OS
- 5.16.14.9. For each air handler, the operator shall be able to suppress the alarm for any fault condition.
- 5.16.14.10. Evaluation of fault conditions shall be suspended under the following conditions:
 - a. When AHU is not operating
 - b. For a period of ModeDelay minutes following a change in mode (e.g., from Warmup Mode to Occupied Mode) of any Zone Group served by the AHU
- 5.16.14.11. Fault conditions that are not applicable to the current OS shall not be evaluated.
- 5.16.14.12. A fault condition that evaluates as TRUE must do so continuously for AlarmDelay minutes before it is reported to the operator.
- 5.16.14.13. Test mode shall temporarily set ModeDelay and AlarmDelay to 0 minutes for a period of TestModeDelay minutes to allow instant testing of the AFDD system, and ensure normal fault detection occurs after testing is complete.
- 5.16.14.14. When a fault condition is reported to the operator, it shall be a Level 3 alarm and shall include the description of the fault and the list of possible diagnoses from the table in Section 5.16.14.7.

Revise Section 5.17.4 as follows:

- 5.17.4. Automatic Fault Detection and Diagnostics
 - 5.17.4.1. The AFDD routines for AHUs continually assess AHU performance by comparing the values of BAS inputs and outputs to a subset of potential fault conditions. Time delays are applied to the evaluation and reporting of fault conditions to suppress false alarms. Fault conditions that pass these filters are reported to the building operator along with a series of possible causes. The AFDD routines listed in this section are intended for heating ducts only; AFDD routines for cooling ducts are listed in Section 5.16.14.AFDD conditions are evaluated continuously and separately for each operating AHU.
 - 5.17.4.2. The following points must be available to the AFDD routines for each AHU:

For the AFDD routines to be effective, an averaging sensor is recommended for supply air temperature.

- a. SAT supply air temperature
- b. RAT = return air temperature
- c. DSP = duct static pressure
- d. SATSP = supply air temperature setpoint
- e. DSPSP = duct static pressure setpoint
- f. HC = heating coil valve position command; 0% ≤ HC ≤ 100%
- g. $FS = fan speed command; 0\% \le FS \le 100\%$
- 5.17.4.3. The following values must be continuously calculated by the AFDD routines for each AHU:
 - a. Five minute rolling averages with 1 minute sampling time of the following point values; operator shall have the ability to adjust the averaging window and sampling period for each point independently
- 5.17.4.2. For each AHU, the following values must be continuously monitored or determined by the AFDD routines and mapped to the indicated variables, which are used in the fault detection equations that follow.
 - a. <u>Continuously measure the following points:</u>
 - 1. <u>SATSP = supply air temperature setpoint</u>
 - 2. DSPSP = duct static pressure setpoint
 - 3. HC = heating-coil valve position command; $0\% \le HC \le 100\%$
 - 4. FS = fan speed command; $0\% \le FS \le 100\%$
 - b. Calculate five-minute rolling averages with 1-minute sampling time of the following point values; operator shall have the ability to adjust the averaging window and sampling period for each point independently.
 - 1. $SAT_{avg} = rolling$ average of supply air temperature

- 2. $RAT_{avg} = rolling$ average of return air temperature
- 3. $DSP_{avg} = rolling$ average of duct static pressure
- 5.17.4.3. The internal variables shown in Table 5.17.4.35.17.4.4 shall be defined for each AHU. All parameters are adjustable by the operator, with initial values as given below:

Default values are derived from NISTIR 7365 and have been validated in field trials. They are expected to be appropriate for most circumstances, but individual installations may benefit from tuning to improve sensitivity and reduce false alarms.

The default values have been intentionally biased toward minimizing false alarms—if necessary, at the expense of missing real alarms. This avoids excessive false alarms that will erode user confidence and responsiveness. However, if the goal is to achieve the best possible energy performance and system operation, these values should be adjusted based on field measurement and operational experience.

Values for physical factors, such as fan heat, duct heat gain, and sensor error, can be measured in the field or derived from trend logs. Likewise, the occupancy delay and switch delays can be refined by observing in trend data the time required to achieve quasi steady-state operation.

Other factors can be tuned by observing false positives and false negatives (i.e., unreported faults). If transient conditions or noise cause false errors, increase the alarm delay. Likewise, failure to report real faults can be addressed by adjusting the heating coil, cooling coil, temperature, or flow thresholds.

Table 5 17 4 25 17 4 4	DEDD Haadlas	ATITI AEDD	Takana al Manialalas
Table 5.17.4.3 5.17.4.4	DEDD Heating	AHU AFDD	internal variables

Variable Name	Description	Default Value
ΔT_{SF}	Temperature rise across supply fan	1°C (2° F)
\mathcal{E}_{SAT}	Temperature error threshold for SAT sensor	1°C (2° F)
\mathcal{E}_{RAT}	Temperature error threshold for RAT sensor	1°C (2° F)
$\mathcal{E}_{ ext{VFDSPD}}$	VFD speed error threshold	5%
\mathcal{E}_{DSP}	Duct static pressure error threshold	25 Pa (0.1")
ModeDelay	Time in minutes to suspend Fault Condition evaluation after a change in Mode	30
AlarmDelay	Time in minutes that a Fault Condition must persist before triggering an alarm	30
TestModeDelay	Time in minutes that Test Mode is enabled	120

- 5.17.4.4. Table 5.17.4.5 shows potential fault conditions that can be evaluated by the AFDD routines. If the equation statement is TRUE, then the specified fault condition exists. Table 5.17.4.4 shows fault conditions that can be evaluated by the AFDD routines.
 - a. If the equation statement is TRUE, then the specified fault condition exists.

Table 5.17.4.45.17.4.5 DFDD Heating AHU Fault Conditions

<u> </u>			
		$DSP < DSPSP - \mathcal{E}_{DSP}$	
FC#1	Equation	and	
	Equation		
		VFDSPD ≥ 99% - E _{VFDSPD}	
	Description	Duct static pressure is too low with fan at full speed	
		Problem with VFD	
	Possible	Mechanical problem with fan	
	Diagnosis	Fan undersized	
	9	SAT Setpoint too high (too much zone demand)	
		$SAT_{AVG} < SATSP - \mathcal{E}_{SAT}$	
	Equation	and	
	•	HC ≥ 99%	
		110 = 7770	
FC#2	Description	SAT too low in full heating	
		SAT sensor error	
	Possible Diagnosis	Heating coil valve stuck closed or actuator failure	
		Fouled or undersized heating coil	
		HW temperature too low or HW unavailable	
		Gas or electric heat unavailable	
	Equation	$RAT_{AVG} - SAT_{AVG} \ge \sqrt{\epsilon_{SAT}^2 + \epsilon_{RAT}^2 + \Delta T_{SF}}$	
		and	
FC#3		HC = 0%	
rc#3	Description	Temperature rise across inactive heating coil	
	•	HCET sensor error	
	Possible	HCLT sensor error	
	Diagnosis	Heating coil valve stuck open or leaking	
		Gas or electric heat stuck on	

- 5.17.4.5. For each air handler, the operator shall be able to suppress the alarm for any fault condition.
- 5.17.4.6. Evaluation of fault conditions shall be suspended under the following conditions:
 - a. When AHU is not operating
 - b. For a period of ModeDelay minutes following a change in mode (e.g., from Warmup Mode to Occupied Mode) of any Zone Group served by the AHU
- 5.17.4.7. A fault condition that evaluates as TRUE must do so continuously for AlarmDelay minutes before it is reported to the operator.
- 5.17.4.8. Test mode shall temporarily set ModeDelay and AlarmDelay to 0 minutes for a period of TestModeDelay minutes to allow instant testing of the AFDD system and ensure normal fault detection occurs after testing is complete.
- 5.17.4.9. When a fault condition is reported to the operator, it shall be a Level 3 alarm and shall include the description of the fault and the list of possible diagnoses from Table <u>5.17.4.45.17.4.5</u>.

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Revise Section 5.18.13 as follows:

Automatic Fault Detection and Diagnostics (AFDD) is a sophisticated system for detecting and diagnosing air-handler faults.

To function correctly, AFDD requires specific sensors and data be available, as detailed in the sequences below. If this information is not available, AFDD tests that do not apply should be deleted.

5.18.13. Automatic Fault Detection and Diagnostics

The AFDD routines for AHUs continually assess AHU performance by comparing the values of BAS inputs and outputs to a subset of potential fault conditions. The subset of potential fault conditions that is assessed at any point depends on the OS of the AHU, as determined by the position of the cooling and heating valves and the economizer damper. Time delays are applied to the evaluation and reporting of fault conditions to suppress false alarms. Fault conditions that pass these filters are reported to the building operator along with a series of possible causes.

These equations assume that the air handler is equipped with hydronic heating and cooling coils, as well as a fully integrated economizer. If any of these components are not present, the associated tests and variables should be omitted from the programming.

- 5.18.13.1. Note that tThese alarms rely on reasonably accurate measurement of mixed air temperature, so the use of averaging sensors. An MAT sensor is required for many of these alarms to work, and an averaging sensor is strongly recommended for best accuracy as mixing box conditions are often highly non-uniform. If an MAT sensor is not installed, omit Fault Conditions #2, #3, #5, #8, #10, and #12. If a heating coil is not installed, omit Fault Condition #7.AFDD conditions are evaluated continuously and separately for each operating AHU.
- 5.18.13.2. The OS of each AHU shall be defined by the commanded positions of the heating-coil control valve, cooling-coil control valve, and economizer damper in accordance with Table 5.18.13.2 and Figure 5.18.13.2.

Table 5.18.13.2	SZVAV AHI	Operating States
1 4010 3.10.13.2	DELITA INTE	Operaning States

Operating State	Heating Valve Position	Cooling Valve Position	Outdoor Air Damper Position
#1: Heating	> 0	= 0	= MinOA-P
#2: Free cooling, modulating OA	= 0	= 0	MinOA-P $< x < 100\%$
#3: Mechanical + economizer cooling	= 0	> 0	= 100%
#4: Mechanical cooling, minimum OA	= 0	> 0	= MinOA-P
#5: Unknown or dehumidification	No other OS applies		

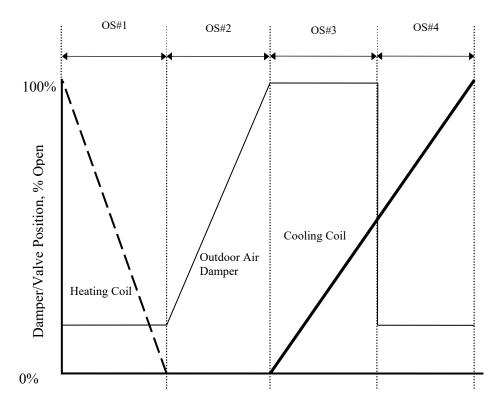


Figure 5.18.13.2 SZVAV AHU operating states.

The OS is distinct from, and should not be confused with, the zone status (cooling, heating, deadband) or Zone Group mode (occupied, warmup, etc.).

OS#1 through OS#4 (see Table 5.18.13.2) represent normal operation during which a fault may nevertheless occur if so determined by the fault condition tests in Section 5.18.13.5. By contrast, OS#5 may represent an abnormal or incorrect condition (such as simultaneous heating and cooling) arising from a controller failure or programming error, but it may also occur normally, e.g., when dehumidification is active or during warmup.

5.18.13.3. The following points must be available to the AFDD routines for each AHU:

For the AFDD routines to be effective, an averaging sensor is recommended for supply air temperature. An averaging sensor is essential for mixed air temperature, as the environment of the mixing box will be subject to nonuniform and fluctuating air temperatures. It is recommended that the OAT sensor be located at the AHU so that it accurately represents the temperature of the incoming air.

- a. SAT = supply air temperature
- b. MAT = mixed air temperature
- c. RAT = return air temperature
- d. OAT = outdoor air temperature
- e. DSP = duct static pressure
- f. SATsp = supply air temperature setpoint for heating coil and economizer control
- g. SATsp C = supply air temperature setpoint for cooling coil control
- h. HC = heating coil valve position command; $0\% \le HC \le 100\%$
- i. CC = cooling coil valve position command; 0% ≤ CC ≤ 100%
- i. FS = fan speed command; $0\% \le FS \le 100\%$
- k. CCET = cooling coil entering temperature (Depending on the AHU configuration, this could be the MAT or a separate sensor for this specific purpose).
- l. CCLT = cooling coil leaving temperature (Depending on the AHU configuration, this could be the SAT or a separate sensor for this specific purpose.)
- m. HCET = heating coil entering temperature (Depending on the AHU configuration, this could be the MAT or a separate sensor for this specific purpose.)
- n. HCLT = heating coil leaving temperature (Depending on the AHU configuration, this could be the SAT or a separate sensor for this specific purpose.)
- 5.18.13.4. The following values must be continuously calculated by the AFDD routines for each AHU:
- 5.18.13.3. Five minute rolling averages with 1 minute sampling of the following point values; operator shall have the ability to adjust the averaging window and sampling period for each point independently. For each AHU, the following values must be continuously monitored or determined by the AFDD routines and mapped to the indicated variables, which are used in the fault detection equations that follow.
 - a. Continuously measure the following points;
 - 1. SATsp = supply air temperature setpoint for heating coil and economizer control

- 2. <u>SATsp-C</u> = supply air temperature setpoint for cooling coil control
- 3. HC = heating-coil valve position command; $0\% \le HC \le 100\%$
- 4. CC = cooling-coil valve position command; $0\% \le CC \le 100\%$
- 5. FS = fan-speed command; $0\% \le FS \le 100\%$
- b. Calculate five-minute rolling averages with 1-minute sampling time of the following point values; operator shall have the ability to adjust the averaging window and sampling period for each point independently.
 - 1. SAT_{avg} = rolling average of supply air temperature
 - 2. MAT_{avg} = rolling average of mixed air temperature
 - 3. $RAT_{avg} = rolling$ average of return air temperature
 - 4. $OAT_{avg} = rolling$ average of outdoor air temperature
 - 5. $CCET_{avg}$ = rolling average of cooling-coil entering temperature (Depending on the AHU configuration, this could be the MAT or a separate sensor for this specific purpose).
 - 6. CCLT_{avg} = rolling average of cooling-coil leaving temperature (Depending on the AHU configuration, this could be the SAT or a separate sensor for this specific purpose).
 - 7. HCET_{avg} = rolling average of heating-coil entering temperature (<u>Depending on the AHU</u> configuration, this could be the MAT or a separate sensor for this specific purpose).
 - 8. HCLT_{avg} = rolling average of heating-coil leaving temperature (Depending on the AHU configuration, this could be the SAT or a separate sensor for this specific purpose).
- c. <u>Vps = current fan airflow, current fan speed multiplied by design cooling airflow scheduled on plans divided by MaxCoolSpeed.</u>
- d. <u>%OA</u> = actual outdoor air fraction as a percentage = (MAT RAT)/(OAT RAT), or active outdoor airflow divided by total airflow rate, Vps, if airflow measurement station is available.
- e. %OAmin = active minimum OA setpoint (MinOAsp) divided by current fan airflow, Vps) as a percentage.
- f. $\Delta OS =$ number of changes in OS during the previous 60 minutes (moving window)
- 5.18.13.4. The internal variables shown in Table 5.18.13.45.18.13.5 shall be defined for each AHU. All parameters are adjustable by the operator, with initial values as given below.

Default values are derived from NISTIR 7365 and have been validated in field trials. They are expected to be appropriate for most circumstances, but individual installations may benefit from tuning to improve sensitivity and reduce false alarms.

The default values have been intentionally biased toward minimizing false alarms, if necessary at the expense of missing real alarms. This avoids excessive false alarms that will erode user confidence and responsiveness. However, if the goal is to achieve the best possible energy performance and system operation, these values should be adjusted based on field measurement and operational experience.

Values for physical factors such as fan heat, duct heat gain, and sensor error can be measured in the field or derived from trend logs. Likewise, the occupancy delay and switch delays can be refined by observing in trend data the time required to achieve quasi steady state operation.

Other factors can be tuned by observing false positives and false negatives (i.e., unreported faults). If transient conditions or noise cause false errors, increase the alarm delay. Likewise, failure to report real faults can be addressed by adjusting the heating coil, cooling coil, temperature, or flow thresholds.

Table <u>5.18.13.4</u>5.18.13.5 SZVAV AHU Internal Variables

Variable Name	Description	Default Value
ΔT_{SF}	Temperature rise across supply fan	0.5°C (1°F)
ΔT_{MIN}	Minimum difference between OAT and RAT to evaluate economizer error conditions (FC#6)	6°C (10°F)
ϵ_{SAT}	Temperature error threshold for SAT sensor	1°C (2°F)
ϵ_{RAT}	Temperature error threshold for RAT sensor	1°C (2°F)
$\epsilon_{ ext{MAT}}$	Temperature error threshold for MAT sensor	3°C (5°F)
EOAT	Temperature error threshold for OAT sensor	1°C (2°F) if local sensor @ unit. 3°C (5°F) if global sensor.
<u>E</u> _F	Airflow error threshold	30%
€ CCET	Cooling coil entering temperature sensor error. Equal to ϵ_{MAT} or dedicated sensor error	E _{MAT} or error of dedicated sensor Varies; see description.
€ _{CCLT}	Cooling coil leaving temperature sensor error. Equal to ϵ_{SAT} or dedicated sensor error	E _{SAT} or error of dedicated sensor
Е НСЕТ	Heating coil entering temperature sensor error; equal to ε_{MAT} or dedicated sensor error	E _{MAT} or error of dedicated sensor
EHCLT	Heating coil leaving temperature sensor error. Equal to ϵ_{SAT} or dedicated sensor error	E _{SAT} or error of dedicated sensor
ΔOSmax	Maximum number of changes in Operating State during the previous 60 minutes (moving window)	7
ModeDelay	Time in minutes to suspend Fault Condition evaluation after a change in mode	30
AlarmDelay	Time in minutes that a Fault Condition must persist before triggering an alarm	30
TestModeDelay	Time in minutes that Test Mode is enabled	120

The purpose of ΔT min is to ensure that the mixing box/economizer damper tests are meaningful. These tests are based on the relationship between supply, return, and outdoor air. If RAT \approx MAT, these tests will not be accurate and will produce false alarms.

The purpose of TestModeDelay is to ensure that normal fault reporting occurs after the testing and commissioning process is completed as described in Section 5.18.13.115.18.13.12.

- 5.18.13.5. Table 5.18.13.5.18.13.6 shows potential fault conditions that can be evaluated by the AFDD routines. (At most, 14 of the 15 fault conditions are actively evaluated, but numbering was carried over from multiple-zone AHUs for consistency.) If the equation statement is TRUE, then the specified fault condition exists. The fault conditions to be evaluated at any given time will depend on the OS of the AHU.
- 5.18.13.6. Table 5.18.13.5 shows fault conditions that can be evaluated by the AFDD routines.
 - a. If the equation statement is TRUE, then the specified fault condition exists.
 - b. Only those fault condition equations that apply to the current OS of the AHU shall be evaluated.

The equations in Table <u>5.18.13.5</u>5.18.13.6 assume that the SAT sensor is located downstream of the supply fan and the RAT sensor is located downstream of the return fan. If actual sensor locations differ from these assumptions, it may be necessary to add or delete fan heat correction factors.

To detect the required economizer faults in California Title 24 section 120.2(i)7, use FC#2, #3, and #5 through #13 at a minimum. Other Title 24 AFDD requirements, including acceptance tests, are not met through these fault conditions.

Table 5.18.13.55.18.13.6 SZVAV AHU Fault Conditions

FC #1	This fault condition is not used in single zone units, as it requires a static pressure setpoint.		Applies to OS #1 – #5
FC #2 (omit if no MAT sensor)	Equation	$\begin{aligned} MAT_{AVG} + \epsilon_{MAT} &< min[(RAT_{AVG} - \epsilon_{RAT}), \\ & (OAT_{AVG} - \epsilon_{OAT})] \end{aligned}$	
	Description	MAT too low; should be between OAT and RAT	Applies to OS #1 – #5
	Possible Diagnosis	RAT sensor error MAT sensor error OAT sensor error	
FC #3 (omit if no MAT sensor)	Equation	$\begin{aligned} MAT_{AVG} - & \epsilon_{MAT} > max[(RAT_{AVG} + \epsilon_{RAT}), \\ & (OAT_{AVG} + \epsilon_{OAT})] \end{aligned}$	
	Description	MAT too high; should be between OAT and RAT	Applies to OS #1 – #5
	Possible Diagnosis	RAT sensor error MAT sensor error OAT sensor error	#1 #B
FC #4	Equation	$\Delta OS > \Delta OS_{MAX}$	
	Description	Too many changes in Operating State	Applies to OS
	Possible Diagnosis	Unstable control due to poorly tuned loop or mechanical problem	#1 – #5

	Equation	$SAT_{AVG} + \epsilon_{SAT} \leq MAT_{AVG} - \epsilon_{MAT} + \Delta T_{SF}$	
FC #5 (omit if no MAT sensor)	Description	SAT too low; should be higher than MAT	
	Possible Diagnosis	SAT sensor error MAT sensor error Cooling coil valve leaking or stuck open Heating coil valve stuck closed or actuator failure Fouled or undersized heating coil HW temperature too low or HW unavailable Gas or electric heat unavailable	Applies to OS #1
	Equation	$ RAT_{AVG} - OAT_{AVG} \ge \Delta T_{MIN} $ and $ [RAT_{AVG} - MAT_{AVG} > OAT_{AVG} - MAT_{AVG} $ $ \frac{or}{ \%OA - \%OA_{MIN} > \mathcal{E}_F]} $	Applies to OS #1, #4
FC #6	Description	OA fraction is too high; MAT should be closer to RAT than to OAT	
	Possible Diagnosis	RAT sensor error MAT sensor error OAT sensor error Leaking or stuck economizer damper or actuator	
	Equation	$SAT_{AVG} < SATSP - \mathcal{E}_{SAT}$ and $HC \ge 99\%$	
	Description	SAT too low in full heating	
FC #7 (omit if no heating coil)	Possible Diagnosis	SAT sensor error Cooling coil valve leaking or stuck open Heating coil valve stuck closed or actuator failure Fouled or undersized heating coil HW temperature too low or HW unavailable Gas or electric heat is unavailable DX cooling is stuck on Leaking or stuck economizer damper or actuator	Applies to OS #1

	Equation	$ SAT_{AVG} - \Delta T_{SF} - MAT_{AVG} >$	
FC #8 (omit if no MAT sensor)	_	$\sqrt{{\epsilon_{SAT}}^2 + {\epsilon_{MAT}}^2}$ SAT and MAT should be approximately	
	Description	equal	Applies to OS
	Possible Diagnosis	SAT sensor error MAT sensor error Cooling coil valve leaking or stuck open DX cooling stuck on Heating coil valve leaking or stuck open Gas or electric heat stuck on	#2
	Equation	OAT_{AVG} - ε_{OAT} > $SATSP$ - ΔT_{SF} + ε_{SAT}	
77. VA	Description	OAT is too high for free cooling without additional mechanical cooling	Applies to OS
FC #9	Possible Diagnosis	SAT sensor error OAT sensor error Cooling coil valve leaking or stuck open DX cooling stuck on	#2
	Equation	$ MAT_{AVG} - OAT_{AVG} > $ $\sqrt{{\epsilon_{MAT}}^2 + {\epsilon_{OAT}}^2}$	
FC #10 (omit if no MAT	Description	OAT and MAT should be approximately equal	Applies to OS #3
sensor)	Possible Diagnosis	MAT sensor error OAT sensor error Leaking or stuck economizer damper or actuator	•
	Equation	$OAT_{AVG} + \varepsilon_{OAT} < SAT_{SP} - \Delta T_{SF} - \varepsilon_{SAT}$	
	Description	OAT is too low for mechanical cooling	
FC #11	Possible Diagnosis	SAT sensor error OAT sensor error Heating coil valve leaking or stuck open Gas or electric heat stuck on Leaking or stuck economizer damper or actuator	Applies to OS #3
	Equation	$SAT_{AVG} - \epsilon_{SAT} - \Delta T_{SF} \ge MAT_{AVG} + \epsilon_{MAT}$	
FC #12 (omit if no MAT sensor)	Description	SAT too high; should be less than MAT	
	Possible Diagnosis	SAT sensor error MAT sensor error Cooling coil valve stuck closed or actuator failure Fouled or undersized cooling coil CHW temperature too high or CHW unavailable DX cooling unavailable Gas or electric heat stuck on Heating coil valve leaking or stuck open	Applies to OS #2 – #4

	Equation	$SAT_{AVG} > SAT_{SP}\text{-}C + \mathcal{E}_{SAT}$ and $CC \ge 99\%$	
	Description	SAT too high in full cooling	
FC #13	Possible Diagnosis	SAT sensor error Cooling coil valve stuck closed or actuator failure Fouled or undersized cooling coil CHW temperature too low or CHW unavailable DX cooling unavailable Gas or electric heat stuck on Heating coil valve leaking or stuck open	Applies to OS #3, #4
FC#14	Equation	$CCET_{AVG} - CCLT_{AVG} \ge$	Applies to OS #1, #2
		$\sqrt{\epsilon_{\text{CCET}}^2 + \epsilon_{\text{CCLT}}^2 + \Delta T_{\text{SF}}^*}$	
		*Fan heat factor included or not depending on location of sensors used for CCET and CCLT	
	Description	Temperature drop across inactive cooling coil	
	Possible Diagnosis	CCET sensor error CCLT sensor error Cooling coil valve stuck open or leaking DX cooling stuck on	
FC#15	Equation	HCLT _{AVG} - HCET _{AVG} ≥	Applies to OS #2 – #4
		$\sqrt{\epsilon_{\text{HCET}}^2 + \epsilon_{\text{HCLT}}^2 + \Delta T_{\text{SF}}^*}$	# -
		*Fan heat factor included or not depending on location of sensors used for HCET and HCLT	
	Description	Temperature rise across inactive heating coil	
	Possible Diagnosis	HCET sensor error HCLT sensor error Heating coil valve stuck open or leaking Gas or electric heat stuck on	

Informative Table 5.1.14.4

5.18.13.9. A subset of all potential fault conditions is evaluated by the AFDD routines. The set of applicable fault conditions depends on the OS of the AHU. If an MAT sensor is not installed, omit FCs #2, #3, #5, #8, #10, and #12. If there is no heating coil, omit FC#7:

- a. In OS#1 (Heating), the following fault conditions shall be evaluated:
 - 1. FC#2: MAT too low; should be between RAT and OAT
 - 2. FC#3: MAT too high; should be between RAT and OAT
 - 3. FC#4: Too many changes in OS

- 4. FC#5: SAT too low; should be higher than MAT
- 5. FC#6: OA fraction too high; MAT should be closer to RAT than to OAT
- 6. FC#7: SAT too low in full heating
- 7. FC#14: Temperature drop across inactive cooling coil
- b. In OS#2 (modulating economizer), the following fault conditions shall be evaluated:
 - 1. FC#2: MAT too low; should be between RAT and OAT
 - 2. FC#3: MAT too high; should be between RAT and OAT
 - 3. FC#4: Too many changes in OS
 - 4. FC#8: SAT and MAT should be approximately equal
 - 5. FC#9: OAT too high for free cooling without mechanical cooling
 - 6. FC#12: SAT too high; should be less than MAT
 - 7. FC#14: Temperature drop across inactive cooling coil
 - 8. FC#15: Temperature rise across inactive heating coil
- e. In OS#3 (mechanical + 100% economizer cooling), the following fault conditions shall be evaluated:
 - 1. FC#2: MAT too low; should be between RAT and OAT
 - 2. FC#3: MAT too high; should be between RAT and OAT
 - 3. FC#4: Too many changes in OS
 - 4. FC#10: OAT and MAT should be approximately equal
 - 5. FC#11: OAT too low for mechanical cooling
 - 6. FC#12: SAT too high; should be less than MAT
 - 7. FC#13: SAT too high in full cooling
 - 8. FC#15: Temperature rise across inactive heating coil
- d. In OS#4 (mechanical cooling, minimum OA), the following fault conditions shall be evaluated:
 - 1. FC#2: MAT too low; should be between RAT and OAT
 - 2. FC#3: MAT too high; should be between RAT and OAT
 - 3. FC#4: Too many changes in OS
 - 4. FC#6: OA fraction too high; MAT should be closer to RAT than to OAT

- 5. FC#12: SAT too high; should be less than MAT
- 6. FC#13: SAT too high in full cooling
- 7. FC#15: Temperature rise across inactive heating coil
- e. In OS#5 (other), the following fault conditions shall be evaluated:
 - 1. FC#2: MAT too low; should be between RAT and OAT
 - 2. FC#3: MAT too high; should be between RAT and OAT
 - 3. FC#4: Too many changes in OS
- 5.18.13.7. For each air handler, the operator shall be able to suppress the alarm for any fault condition.
- 5.18.13.8. Evaluation of fault conditions shall be suspended under the following conditions:
 - a. When AHU is not operating
 - b. For a period of ModeDelay minutes following a change in mode (e.g., from Warmup Mode to Occupied Mode) of any Zone Group served by the AHU
- 5.18.13.9. Fault conditions that are not applicable to the current OS shall not be evaluated.
- 5.18.13.10. A fault condition that evaluates as TRUE must do so continuously for AlarmDelay minutes before it is reported to the operator.
- 5.18.13.11. Test mode shall temporarily set ModeDelay and AlarmDelay to 0 minutes for a period of TestModeDelay minutes to allow instant testing of the AFDD system and ensure normal fault detection occurs after testing is complete.
- 5.18.13.12. When a fault condition is reported to the operator, it shall be a Level 3 alarm and shall include the description of the fault and the list of possible diagnoses from Table 5.18.13.65.18.13.5.

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POLICY STATEMENT DEFINING ASHRAE'S CONCERN FOR THE ENVIRONMENTAL IMPACT OF ITS ACTIVITIES

ASHRAE is concerned with the impact of its members' activities on both the indoor and outdoor environment. ASHRAE's members will strive to minimize any possible deleterious effect on the indoor and outdoor environment of the systems and components in their responsibility while maximizing the beneficial effects these systems provide, consistent with accepted Standards and the practical state of the art.

ASHRAE's short-range goal is to ensure that the systems and components within its scope do not impact the indoor and outdoor environment to a greater extent than specified by the Standards and Guidelines as established by itself and other responsible bodies.

As an ongoing goal, ASHRAE will, through its Standards Committee and extensive Technical Committee structure, continue to generate up-to-date Standards and Guidelines where appropriate and adopt, recommend, and promote those new and revised Standards developed by other responsible organizations.

Through its *Handbook*, appropriate chapters will contain up-to-date Standards and design considerations as the material is systematically revised.

ASHRAE will take the lead with respect to dissemination of environmental information of its primary interest and will seek out and disseminate information from other responsible organizations that is pertinent, as guides to updating Standards and Guidelines.

The effects of the design and selection of equipment and systems will be considered within the scope of the system's intended use and expected misuse. The disposal of hazardous materials, if any, will also be considered.

ASHRAE's primary concern for environmental impact will be at the site where equipment within ASHRAE's scope operates. However, energy source selection and the possible environmental impact due to the energy source and energy transportation will be considered where possible. Recommendations concerning energy source selection should be made by its members.

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About ASHRAE

Founded in 1894, ASHRAE is a global professional society committed to serve humanity by advancing the arts and sciences of heating, ventilation, air conditioning, refrigeration, and their allied fields.

As an industry leader in research, standards writing, publishing, certification, and continuing education, ASHRAE and its members are dedicated to promoting a healthy and sustainable built environment for all, through strategic partnerships with organizations in the HVAC&R community and across related industries.

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