## ERRATA SHEET FOR ANSI/ASHRAE STANDARD 103-2017 Methods of Testing for Annual Fuel Utilization Efficiency of Residential Central Furnaces and Boilers

## May 10, 2022

The corrections listed in this errata sheet apply to ANSI/ASHRAE Standard 103-2017. The first printing is identified on the outside back cover as "Product code: 86316 7/17". Shaded items have been added since the previously published errata sheet dated April 25, 2019 was distributed.

## <u>Page</u> <u>Erratum</u>

31 Table 8 Fuel Characteristics and Parameters for Calculating Steady-State Sensible Heat Loss (L<sub>s,ss</sub>) and Steady-State Efficiency (Effy<sub>ss</sub>). The parenthesis ")" currently located between "(CA(i))" and the square bracket "]" in the equation for L<sub>s,ss</sub> should be moved after "(CF(i)" as shown below.

TABLE 8 Fuel Characteristics and Parameters for Calculating Steady-State Sensible Heat Loss ( $L_{S,SS}$ ) and Steady-State Efficiency ( $Effy_{SS}$ )

$$L_{S,SS} = \frac{100}{\text{HHV}_{A} \times K_{6}} \sum_{i=1}^{5} \left\{ \left[ \left(1 + \frac{A}{F}\right) \left(\text{CF}(i) + \left(\frac{A}{F}\right) (\text{CA}(i))\right) \times \left\langle \left[(T_{a,SS,X} + T_{abs}) \times K_{7}\right]^{i} - \left[(T_{RA} + T_{abs}) \times K_{7}\right]^{i} \right\} \right\}$$

The corrected equation *Ls,ss* is shown below.

$$L_{S,SS} = \frac{100}{HHV_A \times K_6} \sum_{i=1}^{5} \left\{ \left[ \left( 1 + \frac{A}{F} \right) (CF(i)) + \left( \frac{A}{F} \right) (R_{T,a} - 1) (CA(i)) \right] \times \left\langle \left[ \left( T_{a,SS,X} + T_{abs} \right) \times K_7 \right]^i - \left[ \left( T_{RA} + T_{abs} \right) \times K_7 \right]^i \right\rangle \right\}$$

**39 11.2.10.6 Off-Cycle Sensible Heat Loss.** In Section 11.2.10.6 the nomenclature for  $M_{F,P}$  should be replaced as follows:

 $M_{F,P}$  = rate of flue gas mass flow during the off-period during the post-purge after the burner is shut off as defined in Section 11.6.3

40 11.2.10.8 OFF-Cycle Infiltration Heat Loss. In Section 11.2.10.8 for systems numbered 2, 3, and 4 for cases where  $t_p$  is intended to be less than or equal to 3 minutes, the equation for  $L_{I,OFFI}$  should be:

$$\begin{split} L_{I,OFF1} &= 100 * C_p * M_{F,P} * t_P * \left(T_{F,SS} + T_{abs}\right) * \left[\frac{1}{t_{oN}\frac{Q_{IN}}{60}}\right] \\ & * \left[\frac{T_{IA} - T_{OA}}{C_{TS}(T_{F,SS} - T_{F,OFF}(t_P))}\right] * \ln \left[\frac{T_{RA} + T_{abs} + C_{TS}(T_{F,OFF}(t_P) - T_{RA})}{T_{RA} + T_{abs} + C_{TS}(T_{F,OFF}(t_P) - T_{RA})}\right] \end{split}$$

The nomenclature for  $M_{F,P}$  should be replaced as follows:

 $M_{F,P}$  = rate of flue gas mass flow during the off-period during the post-purge after the ©2022 ASHRAE. All rights reserved.

- 42 **11.3.11.1 Latent Heat Gain under Part-Load Conditions.** In the equation for  $L_G$  change " $h_g$ " to " $h_{fg}$ ".
- 44 **11.4.8.3 Average Outdoor Temperature.** In the two equations for  $T_{OA,H}$  in Section 11.4.8.3 delete the square bracket "[" from each of the equations identified below in red text.

$$T_{OA,H}(T_C \text{ in } ^\circ\text{F}) = 6.86 \times 10^{-7} (T_C)^4 - 1.96 \times 10^{-4} (T_C)^3 + [1.08 \times 10^{-2} (T_C)^2 + 5.50 \times 10^{-1} (T_C) + 2.33]$$

Or for temperature in °C use the following:

$$T_{OA,H}(T_C \text{ in } ^{\circ}\text{C}) = 4.00 \times 10^{-6} (T_C)^4 - 3.51 \times 10^{-4} (T_C)^3 - 6.84 \times 10^{-3} (T_C)^2 + 7.29 \times 10^{-1} (T_C) - 3.73$$

**69-75** Figures E-9 through E-15. Replace Figures E-9 through E-15 on pages 69 through 75 with the corrected figures shown on the attached pages.











FIGURE E-11 Steady-state sensible heat loss versus ratio of total combustion to stoichiometric air (for No. 2 oil).















Figure E-15 Steady-state sensible heat loss versus ratio of total combustion to stoichiometric air (for butane).